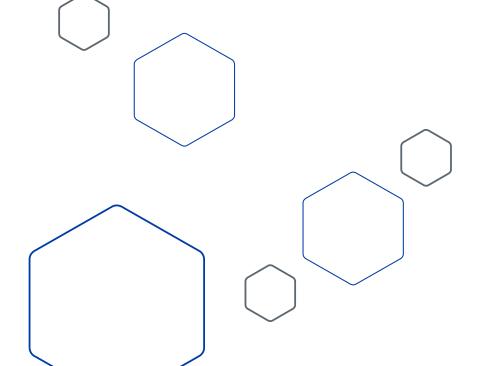






STANDARD OF PRACTICE



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Alberta Private Sewage Systems Standard of Practice 2015

Established by the **Plumbing Technical Council, Safety Codes Council December 1, 2015**

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Safety Codes Council - Plumbing Technical Council

The Safety Codes Council is a statutory corporation that formulates and oversees the development and administration of safety codes and standards in Alberta. The Plumbing Technical Council is one of ten technical councils forming the Safety Codes Council and deals with all matters related to plumbing and private sewage systems. Based upon public review, the Plumbing Technical Council establishes the content of the Private Sewage Systems Standard of Practice and proposes its adoption to the Minister of Municipal Affairs by an Alberta Regulation, the Private Sewage Disposal Regulation.

Technical Task Group

This Standard of Practice is developed by a Task Group of experts established by the Safety Codes Plumbing Technical Council and reviewed by the Council members. The Task Group is made up of industry, municipal, academic, and provincial and federal government stakeholders. Task Group Members represent the following stakeholder groups:

- Alberta Association of Municipal Districts & Counties
- Alberta Onsite Wastewater Management Association
- Private Sewage System Contractors
- Academia and Research
- Work Camp Industry
- Government of British Columbia

- Private Sewage Safety Codes Officer Inspectors
- Manufacturers of onsite wastewater equipment
- and Inuit Health Branch
- Alberta Health
- Public
- Alberta Summer Villages Association

- Alberta Urban Municipalities Association
- Safety Codes Plumbing **Technical Council**
- Health Canada, First Nations
 Association of Professional Engineers, Geologists, and Geophysicists of Alberta
 - Alberta Municipal Affairs
 - Alberta Environment and Parks
 - Alberta Trade Schools

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Part 1 Scope and Definitions

Section 1.1. General

1.1.1. Intent

1.1.1.1. Intent

- 1) The intent of this Standard is to set out performance objectives, design standards, prescriptive-based solutions, and requirements for materials and equipment related to on-site wastewater treatment system designs regarding the
 - a) initial treatment of wastewater,
 - **b)** final treatment of wastewater in soil.
 - c) containment of wastewater and treated effluent,
 - **d)** risk of contact with wastewater or treated effluent,
 - e) operational control of a system, and
 - f) structural adequacy of a system,

that will result in an *on-site wastewater treatment system* that reduces the risk to public health and the natural environment to a level that is deemed acceptable.

1.1.2. Scope

Application 1.1.2.1.

- 1) This Standard establishes requirements for the design, installation, and site selection of onsite wastewater treatment systems that are defined further as¹
 - a) including all components making up the treatment system starting at a point 1.8 m (6 ft.) upstream of the first component in the wastewater management and treatment system to the point where the effluent reaches the treatment boundary limit established for the system and includes any wastewater tanks or lift stations outside the buildings, but not including the building drain leaving the building,
 - b) including any portion of the on-site soils or imported soils used to achieve the required treatment performance,
 - c) including systems where water re-use for irrigation is included as a method to achieve the final treatment and return of the wastewater to the environment,2
 - d) including systems designed to contain wastewater in a safe manner until the wastewater can be removed and transported to another location for treatment and final disposition,
 - including earthen pit privies and vault privies as they relate to the management of the waste received but does not include
 - i) self-contained, portable privies, and
 - ii) any related structural components not required for the management of the wastewater,
 - f) not including systems used for the management of wastewater resulting from industrial processes or otherwise considered an industrial wastewater, and
 - g) not including systems that discharge into a natural body of water or manmade body of water, other than a *wastewater* or *effluent lagoon* described in this Standard.

¹ Note: Sentence (1) — Regulations adopting this Standard may set limits on the application of this Standard under that regulation as it applies to the volume of wastewater generated by the development or limitations regarding the use of systems following this Standard based on larger scale cumulative loading impacts. Reference to the applicable legislation is required for the proper application of this Standard

Alberta Private Sewage Systems Standard of Practice

- ² Note: Clause (c) Such systems would include irrigation where the effluent is utilized for a beneficial purpose but is ultimately returned to the environment through the soil to achieve final treatment.
- 2) This Standard includes specific requirements for on-site wastewater treatment systems that fall within the following broad categories:
 - a) systems serving residential and commercial developments that generate
 - i) up to 5.7 m³ (1,250 lmp. gal.) per day of wastewater volume, and
 - wastewater of a strength equal to or less than typical wastewater,
 - b) systems serving small residential and commercial developments that generate up to 5.7 m³ (1,250 lmp. gal.) per day of wastewater volume and
 - i) the wastewater is of a strength greater than typical wastewater, or
 - ii) where treatment objectives require a disinfection or nutrient reduction component in the treatment train.
 - c) systems serving developments that generate more than 5.7 m³ (1,250 lmp. gal.) of wastewater per day,
 - d) systems that employ effluent water re-use for irrigation as a method of returning it to the environment, and
 - e) pit privies and vault privies.
- This Standard sets out specific requirements for
 - a) holding tanks and septic tanks,
 - **b)** packaged sewage treatment plants,
 - c) treatment fields.
 - **d)** treatment mounds,
 - e) LFH At-grade systems
 - **f)** open discharge systems,
 - wastewater or effluent lagoons,
 - **h)** sand filters,
 - gravel filters, and
 - privies.
- 4) This Standard does not include or establish requirements related to administrative programs needed for the effective overall management of on-site wastewater treatment systems.
- 5) This Standard sets out acceptable system designs and effluent treatment standards suitable for general use in Alberta.
- 6) This Standard sets requirements suitable for the design of private sewage systems in Alberta but does not set out the additional requirements for, or provide direction on, the selection of the type of on-site wastewater treatment system and required effluent quality that may be needed to manage *cumulative impacts* from nitrogen or phosphorus loading present in the wastewater
 - a) on a multi-lot/subdivision scale or water shed scale caused by multiple or large onsite wastewater treatment systems, or
 - b) where systems are located in a sensitive receiving environment.¹
 - Note: Clause (b) The determination of treatment objectives, effluent quality and system types required for a development may need to consider any cumulative impact or loading limits established under other legislation. Loading limits required to prevent unacceptable impacts on groundwater or surface water, caused by the total wastewater generated from multi-lot subdivisions or where needed to protect a sensitive receiving environment, need to be considered in the selection and use of on-site wastewater treatment systems.

1.1.3. Objectives

1.1.3.1. General

- 1) The objective of an on-site wastewater treatment system is to treat wastewater and return it to the environment so that
 - a) risks to health are not created.
 - b) the impact on ground and surface waters is minimized, and
 - c) the environment is not harmed.

1.1.4. Interpretations

1.1.4.1. Supplementary Information

1) Intent statements, notes, and warning statements are included to provide additional information regarding specific requirements.

1.1.4.2. Liability

1) This Standard does not provide or imply any assurance or guarantee about the life expectancy, durability, operating performance, or workmanship of the equipment, materials, or undertaking.

1.1.4.3. Units of Measurement

1) Metric units of measure are the official measurement used in this Standard with approximate imperial equivalents provided in brackets for user convenience.

1.1.4.4. Numbering

1) The numbering system in this Standard uses the following format:

2	Part,
2.5.	Section,
2.5.1.	Subsection,
2.5.1.1.	Article,
2.5.1.1.(1)	Sentence,
2.5.1.1.(1)(c)	Clause,
2.5.1.1.(1)(c)(i)	Subclause.

1.1.5. Definitions

Interpretation of Words and Phrases 1.1.5.1.

- 1) Words and phrases used in this Standard that are not included in the list of definitions shall have the meanings that are commonly assigned to them in the context in which they are used in this Standard, taking into account the specialized use of terms by the trades and professions to which the terminology applies.
- 2) Words and phrases regarding soils and soil characteristics used in this Standard, including defined terms, shall be interpreted and used in a manner consistent with definitions established under the Canadian System of Soil Classification. 1

¹ Note: Sentence (2) — Canadian System of Soil Classification definitions can be used to gain more description of the terms and direction on how to identify and classify soils. Additional and more detailed definitions can also be found in the Canadian Soil Information System (CanSIS) Manual for Describing Soils in the Field.

1.1.5.2. **Defined Terms**

1) Italicized words and terms in this Standard shall have the following meanings:

Administrator - an Administrator appointed pursuant to Section 14 of the Safety Codes Act.

Aguifer - any porous water-bearing geologic formation capable of yielding a supply of water.

Aquifer, Domestic Use - (DUA) a geologic unit (either of a single lithology or inter-bedded units) that is above the Base of Groundwater Protection and has one or more of the following properties:

- a) a bulk hydraulic conductivity of 1 x 10⁻⁶ m/s or greater and sufficient thickness to support a sustained yield of 0.76 L/min or greater,
- b) is currently being used for domestic purposes, or
- c) is any aquifer determined by Alberta Environment to be a DUA.¹

Berm - the raised area around a treatment mound, sand filter, lagoon, or privy.

Biochemical oxygen demand (BOD₅) - the amount of oxygen (expressed as mg/L) utilized by micro-organisms in the oxidation of organic matter during a 5-day period at a temperature of 20°C (68°F). This measure is typically used for raw wastewater samples.

Building - any structure used or intended for supporting or sheltering any use or occupancy that is subject to the Alberta Building Code requirements.

Building drain - the lowest horizontal piping, including any vertical offset, that conducts sewage, clear-water waste, or storm water by gravity to a building sewer.

Building sewer - a pipe connected to a building drain starting 1 m (3.25 ft.) outside a wall of a building and that connects to a public sewer or on-site wastewater treatment system.

Carbonaceous biochemical oxygen demand (cBOD₅) - the amount of oxygen (expressed as mg/L) utilized by micro-organisms in the non-nitrogenous oxidation of organic matter in wastewater during a 5-day period at a temperature of 20°C (68°F). This measure is typically used for effluent samples.

Certified - investigated and identified by a designated testing organization as conforming to recognized standards, requirements, or test reports as set out in this standard or acceptable to the Administrator.

Clearwater waste - wastewater with impurity levels that will not likely be harmful to a person's health but is not considered *potable*.

Coarse-fragment - mineral particles in the soil that exceed 2.00 mm in diameter.

COLE (Coefficient Of Linear Extensibility) - the percentage decrease in the length of a bar of soil formed from a disturbed soil sample at its liquid limit (saturation limit) after being dried in an oven.

¹ Note: While it is possible that peat deposits and muskeg may meet the definition of a DUA, based on hydraulic conductivity and unit thickness, Alberta Environment generally does not consider peat deposits or muskeg to be a DUA because groundwater in them is unlikely to be used as a domestic source.

¹ Note: as the building sewer starts 1m (3.25 ft.) outside the building, the building drain then ends at a point 1m (3.25 ft.) outside the building.

Consistence - an attribute of soil expressed in degree of cohesion and adhesion, or in resistance to deformation or rupture. Consistence includes: the resistance of soil material to rupture; resistance to penetration; the plasticity, toughness, or stickiness of puddled soil material; and the manner in which the *soil* material behaves when subjected to compression. Classifications of moist soil consistence include loose, very friable, friable, firm, very firm, and extremely firm.

Cumulative impact - the total impact attributable to numerous individual influences.

Development - buildings or other constructed facilities.

Diameter unless otherwise indicated, the nominal *diameter* by which a pipe, fitting, trap, or other item is commercially designated.

Distribution header - a non-perforated pipe, receiving effluent from the effluent sewer or effluent line, which distributes effluent by pressure or gravity to more than one effluent distribution lateral pipe, weeping lateral pipe, or weeping lateral trench.

Distribution lateral pipe - a perforated pressurized pipe used to evenly distribute effluent throughout the entire length of a weeping lateral trench or over a surface area in a sand filter or treatment mound.

Drain media - clean washed *gravel*, clean crushed rock, or other media into which *effluent* is distributed or used to collect effluent below treatment filter media and meets the specific material requirements set out in this Standard for its specific purpose.

Dwelling or **Dwelling unit** - a suite operated as a housekeeping unit that is used or intended to be used as a domicile by one or more persons and usually contains cooking, eating, living, sleeping, and sanitary facilities.

DWV pipe - a class of piping certified for use in a plumbing system for use as drain, waste, and venting piping.

Effective particle size (D_{10}) - the size of opening of an ideal sieve that would retain 90% of a sample, while passing 10% of the sample.

Effluent - the liquid discharged from any *on-site wastewater treatment system* component.

Effluent chamber or Effluent tank - a chamber within a tank or any tank that receives and stores effluent (from which effluent is periodically discharged into other components of the treatment system).

Effluent hydraulic linear loading - the cumulative total of effluent applied to the soil profile below a soil-based treatment area, expressed as volume per unit length per unit time, e.g., litres per day per lineal metre, along the axis of the soil-based treatment area that is oriented at 90 degrees to the assumed direction of subsurface flow (typically this is consistent with surface slope direction).

Effluent hydraulic loading rate - the quantity of effluent applied to a given treatment component, usually expressed as volume per unit of infiltrative surface area per unit time, e.g., liters per day per square metre (Lpd/m²) or imperial gallons per day per square foot (gpd/ft²).

Effluent line - piping for the flow of *effluent* under pressure and supplied by a pump.

Effluent sewer - piping for the flow of *effluent* through the action of gravity.

Equalization tank - a tank that provides storage of wastewater or effluent to enable timed-dosing by pumps to manage flow variations, resulting in a more uniform delivery of wastewater or effluent to a subsequent component over time, usually a day or more; also known as a surge tank.

Field capacity - the maximum amount of water that can be held by a soil without draining by gravity.

Field header - a main gravity weeping lateral pipe that also distributes effluent to other weeping lateral pipes in a treatment field where all weeping lateral trenches and the distribution header are at the same elevation and level.

Filter fabric - a synthetic woven or spun-bonded sheet material used to impede or prevent the movement of sand, silt, and clay into the spaces between larger media but does not impede the movement of air or water.

Fines - particles that can pass through a 0.15mm (0.0059 in.) No. 100 sieve.

Gleyed - a characteristic of a soil that has undergone gleysation, a soil-forming process that occurs under poor drainage conditions and results in redoximorphic features (the reduction of iron and other elements and in bluish, greenish or gray soil colours, and/or rust or gray coloured mottles). It is indicative of soils that are saturated or waterlogged for significant periods of time, which limits the suitability of soil for an effluent treatment system. See the Canadian Soil Information System for a more definitive definition and further information on identifying *gleyed* soils.

Grade -

- a) in relation to soil characteristics, the degree of visual distinctness and cohesion of soil aggregates into peds expressed as grade: single grained structureless or massive (0), weak (1), moderate (2), or strong (3), or
- b) in relation to an elevation on the landscape, the upper surface of the ground.

Gravel - see Drain Media

Greywater - wastewater that does not include waste from toilets or urinals, and that must be effectively managed and treated in accordance with this Standard.

Groundwater mounding - the rise in elevation of the seasonally saturated soil, regional water table or the creation of a perched water table below the soil-based treatment area resulting from the addition of effluent to the soil.

Groundwater Under the Direct Influence of Surface Water (GWUDI) - groundwater having incomplete/undependable subsurface filtration of surface water and infiltrating precipitation. 1

Note: Refer to the Alberta Environment document entitled "Assessment Guideline for Groundwater Under the Direct Influence of Surface Water (GWUDI)" for determining whether a groundwater source is GWUDI.

Holding tank - a tank designed to retain wastewater or effluent until transferred into mobile equipment for treatment offsite.

Infiltration -

- entry of water or effluent into the soil;
- undesirable inflow or seepage of water into a system component, for example, infiltration of surface water into a tank through a leaking pipe or through an access riser/tank seam that is not water-tight.

Lagoon - an man-made pond for the storage, treatment, and stabilization of wastewater or effluent.

LFH At-grade system - a system for the dispersal and final treatment of effluent that

- is located in a well-established forested area having a substantial LFH (litter, fermented, humic) layer,
- b) has a pressurized effluent distribution lateral pipe system that is placed on the surface of the undisturbed forest floor inside a chamber, and
- has wood chips, or other material that is suited to the ecology of the forest, covering the chambers.

Lift Station - a tank-and-pump assembly used for the prime purpose of lifting sewage to a higher elevation and discharging it into other parts of the on-site wastewater treatment system.

Limiting condition - soil or site characteristic that reduces the efficiency of *effluent* treatment in the soil or reduces hydraulic conductivity and thus restricts design options for a system.

Linear loading - (See Effluent hydraulic linear loading).

Mobile soil water content - the amount of water held in a soil between the soil's field capacity and the hydroscopic water holding ability of the soil, that is displaced as additional water is added to the soil volume.

Mottling - a soil zone of chemical oxidation and reduction activity, appearing as splotchy patches of red, brown, orange, or gray in the soil, that may indicate the presence of a water table.

Nominally level - level, so as to not affect the performance of the system.

On-site wastewater treatment system - a system for the management and/or treatment of wastewater at or near the development that generates the wastewater, including that portion of the building sewer 1.8 m (6 ft.) upstream of any on-site lift station, equalization tank, settling tank, septic tank, packaged sewage treatment plant, holding tank, or berm of a sewage lagoon, and includes the final soil-based effluent dispersal and treatment system but does not include the plumbing building drain from the development, which ends 1 m (3.25 ft.) outside a building.

Open discharge system - a system designed to discharge *effluent* to the ground surface to accomplish evaporation and absorption of the effluent into the soil as a method of treatment.

Organic loading - the total mass loading per unit of area per unit of time based on the cBOD₅ concentration in the effluent, multiplied by the volume of effluent applied over a given time, e.g., grams of *cBOD*₅/m²/day.

Packaged sewage treatment plant - a manufactured unit that is used to substantially improve the effluent quality beyond the quality of effluent expected of a septic tank.

Packed bed filter - a container(s) packed with a filter media that receives effluent from an effluent distribution system to achieve the aerobic, biological, and physical treatment of wastewater as it passes through and comes in contact with the filter media.

Parcel - has the same meaning as *property*, as defined in this standard, which is also the same meaning as set out in Section 616 of the Municipal Government Act

Particle size analysis - establishing the percentage of sand, silt, or clay particles in a soil sample by of a standard hydrometer method and sieve analysis, as set out in the Canadian Soil Information System (CanSIS Analytical Methods Manual 1984 or other more recent and equivalent method recognized in the soil sciences).

Percolation test - a procedure to estimate the rate the soil can accept and move clean water in saturated flow conditions.

Potable - suitable for human consumption.

Pressure head - the pressure existing in a fluid expressed as the height of a column of water that would exert an equal pressure.

Primary treatment - physical treatment processes involving removal of particles, typically by settling and flotation with or without the use of coagulants; (e.g. a septic tank provides primary treatment).

Private sewage system - (See On-site wastewater treatment system).

Primary treated effluent or primary treated effluent Level 1 - effluent that

- a) 80% of the time has
 - cBOD₅ of less than 150 mg/L,
 - TSS of less than 100 mg/L, and
 - oil and grease content of less than 15 mg/L, and iii)
- b) does not exceed
 - $cBOD_5$ of 230 mg/L, i)
 - TSS of 150 mg/L, and ii)
 - oil and grease content of 30 mg/L.

Privy - a small building having a toilet pedestal, or bench with a hole or holes, through which human excretion falls into an excavated pit or waterproof vault.

Property - the land described in the Certificate of Title issued under the Land Titles Act.

Re-circulating gravel filter - a system where effluent is re-circulated through filter media a number of times on an intermittent basis before being discharged for additional treatment or into a final treatment and dispersal system. (This design is often used to treat higher strength wastewater. It is sometimes referred to as a "re-circulating sand filter" in the industry).

Restricting layer or restrictive layer - a soil horizon, soil layer, or other condition in the soil profile, or underlying strata, that restricts the downward movement of fluids that could cause a perched water table or saturated soil under the soil infiltration surface of the system. Examples include but are not limited to: a fragipan or spodic horizon, fine textured soil with massive structure, certain bedrock, seasonally saturated soils, water table, etc.

Sand filter - a single-pass sand filter that is intermittently dosed and that uses specifically graded sand or other media as the media for filtration and treatment of effluent.

Sand filter media - the granular filter media used in a sand filter for the treatment of the effluent.

Sand filter surface area - the area of the level plane section of the sand filter media receiving the effluent immediately below the drain media or chambers containing the pressurized effluent distribution piping.

Sand layer - (when referring to a *treatment mound*) the required depth and area of specifically graded sand that will receive the effluent distributed through a gravel bed or chambers located immediately above the sand layer.

Seasonally saturated soil - a soil that is seasonally saturated by a periodic high water table and is identified by the presence of mottling or gleying in the soil.

Secondary treated effluent - effluent that at least 80% of the time meets the effluent quality parameters set out in Table 5.1.1.1 for secondary treated effluent Levels 2, 3, or 4.

Septic tank - a tank or chamber(s) within a tank used to provide primary treatment of wastewater through the process of settling and floating of solids and in which digestion of the accumulated sludge occurs.

Serial distribution - a treatment field design where discharged effluent is forced to travel through one weeping lateral trench to get to another weeping lateral trench.

Settling tank - a tank, or chamber within a tank, that typically has a limited retention time and is installed upstream of a packaged sewage treatment plant or other initial treatment system and is intended for the removal of larger items or inorganic material in the wastewater stream and may also provide some level of treatment and anaerobic digestion (sometimes referred to as a "trash tank").

Sewage - (see Wastewater).

Shore - the edge of a body of water; includes the land adjacent to a body of water that has been covered so long by water as to wrest it from vegetation, or as to mark a distinct character on the vegetation where it extends into the water or on the soil itself.

Single-pass sand filter - a system in which the effluent is applied on an intermittent basis and flows through the filter only once before being discharged for additional treatment or final dispersal.

Size - unless indicated otherwise, the nominal size by which a pipe, fitting, trap, or other item is commercially designated.

Slope of land - a landscape form or feature demonstrating a change in elevation; typically described as a percentage (amount of rise divided by amount of run multiplied by 100).

Smectitic or Smectitic soil - a soil that has characteristics significantly influenced by smectite clays, which are a group of 2:1 layer silicates with a high cation exchange capacity, about 110 cmol/kg soil smectites, and variable interlayer spacing; formerly called the montmorillonite group. The group includes dioctahedral members (montmorillonite, beidellite, and nontronite) and trioctahedral members (saponite, hectorite, and sauconite). These soils can increase the risk of failure when effluent having a high SAR is applied. For test methods that can assist in identifying these soils and the soil's susceptibility to dispersion when applying effluent with a high SAR, see the Private Sewage Treatment Systems Standard of Practice handbook. Information on the Emerson modified soil dispersion test is also helpful.

Sodium Adsorption Ratio (SAR) - a ratio of sodium, calcium, and magnesium that is used to express the relative activity of sodium ions in exchange reactions with soil. Effluent having a high SAR leads to a breakdown in the physical structure of the soil in smectitic soils.

Soil - a naturally occurring, unconsolidated mineral or organic material at the earth's surface that is capable of supporting plant growth. Its properties usually vary with depth and are determined by climatic factors and organisms, as conditioned by relief and hence water regime, acting on geologic materials and producing genetic horizons that differ from the parent material.

Soil colour - colour features of a soil that indicate soil formation processes and conditions. The colours are indicators of the level of aerobic conditions of the soil, which is important to wastewater treatment in the soil. The Munsell Colour System is the method used to define and communicate the colours of the soil.

Soil horizon - a layer of *soil* or *soil* material approximately parallel to the land surface; it differs from adjacent genetically related layers in properties such as colour, structure, texture, consistence, and chemical, biological, and mineralogical composition.

Soil infiltration surface - the surface of *soil* receiving *effluent* for final treatment but does not include the infiltration surface of an engineered media or soil intended to improve the quality of the effluent prior to infiltration in to the soil for final treatment, such as the sand layer in a treatment mound.

Soil separates - has the following 3 categories:

- a) **Sand** soil particles of a size between 0.05–2 mm.
- **b)** Silt soil particles of a size between 0.002– <0.05 mm.
- c) Clay soil particles of a size smaller than 0.002 mm.

Soil structure or **Structure** - the combination or arrangement of primary soil particles into secondary units or peds; secondary units are characterized on the basis of shape, size class, and grade (degree of visual distinctness and cohesion of soil aggregates into peds expressed as: single grained structureless or massive (0), weak (1), moderate (2), or strong (3)).

Soil texture classification or **Texture -** the relative proportions of the various soil separates in a soil (sand, silt, clay) and is described with the following soil textural classes and sub-classes:

- Sand soil material that contains 85% or more sand; the percentage of silt plus 1.5 times the percentage of clay does not exceed 15; sand has the following sub-classes:
 - i) Coarse sand 25% or more very coarse and coarse sand, and less than 50% any other one grade of sand. Coarse sand has a size limit that ranges between 1.0 to 0.5 mm. Very coarse sand has a size limit that ranges between 1.0 to 2.0 mm.
 - ii) **Medium sand -** 25% or more very coarse, coarse, and medium sand, and less than 50% fine or very fine sand. Medium Sand has a size limit that ranges between 0.5 and 0.25 mm.
 - iii) Fine sand 50% or more fine sand or less than 25% very coarse, coarse, and medium sand and less than 50% very fine sand. Fine sand has a size limit that ranges between 0.25 and 0.10 mm.
 - iv) Very fine sand 50% or more very fine sand. Very fine sand has a size limit that ranges between 0.10 to 0.05 mm.
- b) **Loamy sand -** soil material that contains at the upper limit 85 to 90% sand, and the percentage of silt plus 1.5 times the percentage of clay is not less than 15; at the lower limit it contains not less than 70 to 85% sand, and the percentage of silt plus twice the percentage of *clay* does not exceed 30; *loamy sand* has the following sub-classes:
 - i) Loamy coarse sand 25% or more very coarse and coarse sand and less than 50% any other one grade of sand.
 - ii) Loamy medium sand 25% or more very coarse, coarse, and medium sand and less than 50% fine or very fine sand.
 - iii) Loamy fine sand 50% or more fine sand or less than 25% very coarse, coarse, and medium sand and less than 50% very fine sand.
 - iv) Loamy very fine sand 50% or more is very fine sand.
- **Sandy loam -** soil material that contains either 20% or less *clay*, with a percentage of silt plus twice the percentage of clay that exceeds 30, and 52% or more sand; or less than 7% clay, less than 50% silt, and between 43% and 52% sand; sandy loam has the following sub-classes:
 - i) Coarse sandy loam 25% or more very coarse and coarse sand and less than 50% any other one grade of sand.

- **Medium sandy loam -** 30% or more very coarse, coarse, and *medium sand*, but less than 25% very coarse sand, and less than 30% very fine sand or fine sand.
- iii) Fine sandy loam 30% or more fine sand and less than 30% very fine sand or between 15 and 30% very coarse, coarse sand, and medium sand.
- iv) Very fine sandy loam 30% or more very fine sand or more than 40% fine sand and very fine sand, at least half of which is very fine sand, and less than 15% very coarse, coarse sand, and medium sand.
- Loam soil material that contains 7 to 27% clay, 28 to 50% silt, and less than 52% d) sand.
- **Silt loam** soil material that contains 50% or more silt and 12 to 27% clay, or 50 to 80% silt and less than 12% clay.
- Silt soil material that contains 80% or more silt and less than 12% clay. Silt has a size f) limit that ranges from 0.05 to 0.002 mm.
- Sandy clay loam soil material that contains 20 to 35% clay, less than 28% silt, and g) 45% or more sand.
- Clay loam soil material that contains 27 to 40% clay and 20 to 45% sand. h)
- i) **Silty clay loam -** soil material that contains 27 to 40% *clay* and less than 20% *sand*.
- Sandy clay soil material that contains 35% or more clay and 45% or more sand. i)
- k) Silty clay - soil material that contains 40% or more clay and 40% or more silt.
- Clay soil material that contains 40% or more clay, less than 45% sand, and less than I) 40% silt. Clay has a size limit that is less than 0.002 mm.
- m) **Heavy clay -** soil material that contains more than 60% clay.

Soil-based treatment area or system - the physical location and area where the dispersal of effluent into the soil and final treatment of the effluent in the soil occurs.

Storm water - water discharged from a surface as a result of rainfall or melting snowfall.

Subsoil foundation drainage pipe - a piping system that is installed underground to intercept and convey subsurface water away from a foundation.

Total Suspended Solids (TSS) - the dispersed particulate matter in a wastewater sample that may be retained by a filter medium. Suspended solids may include both settleable and unsettleable solids of both inorganic and organic origin. This parameter is widely used to monitor the performance of the various stages of wastewater treatment, and is often used in conjunction with BOD₅ and cBOD₅ to describe wastewater strength.

Treatment boundary limits - the limits of the treatment zone in the soil as defined by this Standard and as used in a design, such as the *vertical separation* depth required below an infiltrative surface that *effluent* is applied over and at the point the design requires or expects treatment to be achieved.

Treatment field - a system of *effluent* dispersal and treatment by distributing *effluent* within trenches containing void spaces that are covered with soil and includes the following types:

conventional treatment field - a system of effluent dispersal and treatment utilizing a) perforated piping laid in a bed of *gravel* in trenches for distributing *effluent* within the trenches.

- b) chamber system treatment field - a system of effluent dispersal and treatment using preformed structures to provide a void space for storage and movement of effluent, and an interface with the exposed infiltrative surface of the soil.
- c) gravel substitute treatment field - a conventional treatment field, in which the gravel is replaced with an alternate media having characteristics that will provide void space and performance similar to gravel, and
- raised treatment field any of the above variations of treatment fields where soil is d) imported to enable all or a portion of the treatment field trench to be located above the in situ soil surface.

Treatment mound or **Mound** - a system where the *effluent* is distributed onto a sand layer and is built above grade to overcome limits imposed by depth to seasonally saturated soil or bedrock, or by highly permeable or impermeable soils.

Typical wastewater - wastewater that1

- a) 80% of the time has
 - i) BOD_5 of less than 220 mg/L,
 - ii) TSS of less than 220 mg/L, and
 - iii) oil and grease content of less than 50 mg/L, and
- b) does not exceed
 - i) BOD_5 of 300 mg/L,
 - ii) TSS of 350 mg/L, and
 - iii) oil and grease content of 70 mg/L.

Underdrain media - (as used in a sand filter) material that is placed under the sand filter media in a sand filter and is of a size to support the sand.

Underdrain piping - piping placed under the sand filter surface area in the underdrain media or drain media to collect the effluent that has travelled through the sand filter.

Uniformity coefficient (CU) - a numeric quantity that is calculated by dividing the size of the opening which will pass 60% of a sample by the size of the opening which will pass 10% of the sample ($D_{60}/D_{10}=CU$).

Vadose zone - the depth of soil from the top of the ground surface, in which soil water has a pressure head less than atmospheric pressure and is retained by a combination of adhesion and capillary action, to the depth at which soil water is at atmospheric pressure.

Vertical separation - the depth of unsaturated soil between the soil infiltration surface and a restricting layer.

Wastewater - the composite of liquid and water-carried wastes associated with the use of water for drinking, cooking, cleaning, washing, hygiene, sanitation, or other domestic purposes; includes *greywater* but does not include liquid waste from industrial processes.

Water course;

- a) a river, stream, creek, or lake,
- b) swamp, marsh, or other natural body of water,
- c) a canal, reservoir, or other man-made surface feature intended to contain water for a specified use, whether it contains or conveys water continuously or intermittently, but

¹ Note: These concentrations assume a design peak daily flow of 340 L per person per day.

- does not include surface water run-off drainage ditches, such as those found at the side of roads, or
- an area that water flows through or stands in long enough to establish a definable d) change in or absence of vegetation (See definition of shore).

Water re-use - a beneficial use of the treated wastewater directed to a specific purpose other than the general release to surface or subsurface environments.

Water source - a man-made or natural source of potable water.

¹ Note: A cistern is also considered to be a water source when buried in the earth. An above ground tank or a freestanding tank within a basement of a building would not have to meet minimum distance requirements from treatment components.

Water table - the highest elevation in the soil at any given point in time where all voids are filled with water, as evidenced by the presence of water, soil mottling, or other soil characteristics that indicate intermittent saturated soil conditions.

Water well - an opening in the ground, whether drilled, bored, dug or otherwise altered from its natural state, which is used, or intended to be used, for the withdrawal of groundwater.

Weeping lateral pipe - the perforated pipe used to distribute effluent by gravity within a treatment field trench.

Weeping lateral trench - a trench in a treatment field that receives effluent and provides a soil infiltration surface.

Working capacity - the liquid volume of wastewater held in the septic chamber when the tank is properly installed and is in normal use, and does not include the air space, siphon chamber, pumping chamber, or effluent chamber of a tank.

1.1.6. **Abbreviations**

1.1.6.1. General

1) Abbreviations in this Standard have the following meanings:

ABS acrylonitrile-butadiene- Styrene				
BOD5 Biochemical Oxygen Demand cBOD5 Carbonaceous Biochemical Oxygen Demand cm² square centimetre(s) degree(s) CSA Canadian Standards Association dia. diameter DWV drain, waste, and vent EC electrical conductivity ft. foot (feet) gpm gallons per minute gal. gallons limp. lmperial (gallons) in. inch(es) kPa kilopascal(s) L/min litres per minute mL millilitre kilogram(s) lmp. light of the first severage in the carbonaceous Biochemical Oxygen Demand mg/L millilitre light of the carbonaceous Biochemical mg/L millilitre millililitre millilililitre millilililitre millililitre millililililililililililililililililili	ABS	acrylonitrile-butadiene-		
Carbonaceous Biochemical Oxygen Demand Cm2		Styrene		
CBOD ₅ Carbonaceous Biochemical Oxygen Demand Cm ² square centimetre(s) square temp. Implification square temp.	BOD₅	Biochemical Oxygen Demand		
Oxygen Demand cm² square centimetre(s) degree(s) C degree(s) Celsius CSA Canadian Standards	U		-	
cm² square centimetre(s) degree(s) Combo degree(s) Nombo degree(s) Nom	02025			` ,
degree(s) CC degree(s) Celsius CSA Canadian Standards Association dia. diameter DWV drain, waste, and vent EC electrical conductivity ft. foot (feet) gpm gallons per minute gal. gallons Imp. Imperial (gallons) in. inch(es) kPa kilopascal(s) L litre(s) L/min litres per minute mL millilitre water Resources Capacity NSF National Sanitation Foundation NPS nominal pipe size P phosphorus PE polyethylene PO4 ortho phosphate PVC poly (vinyl chloride) psi pounds per sq. inch (pressure) SAR sodium adsorption ratio sq. square temp. temperature	cm²			` ,
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ft. foot (feet) gpm gallons per minute gal. gallons Imp. Imperial (gallons) in. inch(es) kPa kilopascal(s) L litre(s) L/min litres per minute mL millilitre kg kilogram(s) NPS nominal pipe size P phosphorus PE polyethylene PO ₄ ortho phosphate PVC poly (vinyl chloride) psi pounds per sq. inch (pressure) SAR sodium adsorption ratio sq. square temp. temperature	DWV	drain, waste, and vent	NSF	
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mL millilitre square temp temperature	L		CVD	,,
kg kilogram(s) temp temperature		•		·
	mL			
	kg	• ,		total kjeldahl nitrogen
TOC total kjeldali filtiogen	lb	pound(s)		
m metre(s) TSS total suspended solids	m	metre(s)		
mm millimetre(s) US United States				·
μm micrometre(s) or microns (liquid gallon measure)	μm	` ,		

Part 2 General Requirements

Section 2.1. General System Requirements

2.1.1. General System Requirements — Objectives and Design Requirements

2.1.1.1. General

- 1) An on-site wastewater treatment system designed and installed to meet the objectives and requirements of this Standard shall
 - a) be capable of treating the volume and strength of wastewater generated by the development served,
 - **b)** be suitable for the location and soil conditions at the site,
 - c) achieve the performance objectives required by this Standard and anticipated for the design, and
 - **d)** accommodate maintenance and/or operational functions required by the system.

2.1.1.2. Objectives and Design Requirements Based on Peak Flow

1) Subsection 2.2.2. shall be referenced to determine the applicability of objectives or requirements based on flow volumes and class of treatment system.

2.1.1.3. Objectives Achieved Within Treatment Boundary Limits

- 1) Wastewater quality treatment objectives set out in this Standard shall be achieved before the wastewater meets the intended treatment boundary limits applicable to the design and required by site conditions whether the wastewater is on the surface where intended by the design, or moving through the soil and subsoil.
- 2) A treatment boundary limit set for all systems, except for lagoons and open discharge systems, is established at the surface of the ground and to a depth of 75 mm (3 in.) below ground surface in which the following limits will not be exceeded:
 - a) fecal coliform < 10 cfu/100 mL above background levels, or
 - fecal coliform < 2 MPN/gram of dry soil above background levels.

2.1.1.4. **Design Considerations**

- 1) An on-site wastewater treatment system design shall consider¹
 - a) the soil conditions determined by a complete site evaluation as required in Part 7.
 - the projected volume of wastewater, flow variation, and wastewater strength determined by an evaluation
 - i) as required in Section 2.2. of this Standard, and
 - ii) that considers any pertinent characteristics of the development not specifically set out in this Standard.
 - the impact of potential groundwater mounding resulting from the addition of the effluent,
 - separation distances required by this Standard, d)
 - cold-weather operation and other climatic conditions recorded by Environment Canada or another recognized source for the specific location where the system is installed,² and

other objectives and prescriptive requirements of this Standard that may impact system design and performance.

¹ Note: Sentence (1) — The design may need to include consideration of cumulative impacts or loading limits established under other legislation. Also see Article 1.1.2.1.sentence (6)

2.1.1.5. Dosing of Effluent Required

1) An *on-site wastewater treatment system* that includes a *soil infiltration surface* shall be capable of delivering *effluent* to the *soil infiltration surface* in a volume dose adequate to achieve effective distribution of the *effluent* and minimize the risk of system freezing.¹

¹ Intent: Sentence (1) — The system should discharge effluent intermittently with sufficient volume to encourage distribution of effluent throughout the system and to reduce the incidence of freezing problems common with "Trickle Type" systems. Trickle type systems are not allowed by this Standard. A dose tank must be included in the system. The dose tank does not have to be integral to the septic tank. A separate tank is often better as it allows the designer to select a tank that has adequate volume to accomplish the desired dosing pattern.

2.1.1.6. Effluent Filters

- 1) All systems shall include an *effluent* filter that removes particles 3.2 mm (1/8 in.) in *diameter* and larger from the *effluent* being discharged to the *soil*-based *effluent* treatment component.
- 2) Effluent filters shall be selected to accommodate the flow rate through the filter required by the system design over the period of time intended for system service intervals set out in the operations manual developed for the system.¹

¹ Note: Sentence (2) — The filter should be selected to provide an intended service interval appropriate for the system while considering other required service intervals for the system. It should be inspected yearly and serviced as required. To provide clarity this requirement applies to both pressure distribution lateral systems and to gravity systems that rely on the infiltration of effluent into the soil. As such it includes an open discharge system that relies on infiltration into the soil.

2.1.1.7. Groundwater Infiltration

1) An *on-site wastewater treatment system* shall be designed and installed to prevent the *infiltration* of groundwater into any component of the system.

2.1.1.8. Surface Storm Water Run-off

 The design and location of the on-site wastewater treatment system and finished landscaping shall minimize the impact of surface storm water run-off water on the performance and operation of the system.

2.1.1.9. Service Access

- Components of an on-site wastewater treatment system that require regular maintenance shall be readily accessible such that servicing or required maintenance can be performed from the ground surface.
- 2) The location of tanks that need servicing by vacuum trucks shall be located such that reasonable access can be provided to the tank, considering distance and vacuum lift limitations.

2.1.1.10. High-Strength Wastewater Considerations

- If the development served by the on-site wastewater treatment system is expected to generate wastewater that includes constituents normally not found in typical wastewater, or if the concentrations exceed the values anticipated in typical wastewater, the system design shall¹
 - a) include specific features that effectively treat the wastewater, or

² Note: Clause (1)(e) — Appendix A provides climatic data for various locations in Alberta and may be used to satisfy design criteria.

b) have the *wastewater* directed to a *holding tank* for treatment at an appropriate facility. Note: Sentence (1) — If the wastewater source only includes an increased organic load, it may be treated by an on-site treatment system with appropriate design considerations; however, in some cases the wastewater may include hydrocarbons, metals, or other chemicals that require specialized treatment offsite.

2.1.1.11. Bypassing Treatment Phase Prohibited

1) Wastewater shall not bypass any treatment phase of the on-site wastewater treatment svstem.1

Intent: Sentence (1) — To ensure system effectiveness is not reduced due to ineffective flow management or treatment resulting from wastewater bypassing a component of the treatment system.

2.1.2. General System Requirements — Prescriptive Requirements and Installation Standards

2.1.2.1. Site Suitability and Use of Holding Tanks

- 1) An on-site wastewater treatment system shall not be installed where there is
 - a) insufficient area to meet all minimum distance requirements of this Standard for the intended system, or
 - b) no available location that has the soil and site characteristics, as determined by an evaluation required by Part 7 and set out in Part 8, required to develop a sustainable onsite wastewater treatment system that can accept and treat the wastewater load generated by the *development*.
- 2) Notwithstanding Clause (1)(b) and subject to Sentence (3), a holding tank system may be installed.
- 3) The suitability of using a holding tank system for a development, or a requirement that only a holding tank system be used, is subject to determination by the local municipal government, and if a holding tank system is used it shall conform with this Standard. ¹

Intent: Sentence (3) — Holding tanks are not a self-sustaining method of private wastewater management. The system relies on the availability of an approved offsite wastewater treatment facility creating a load on municipal infrastructure. Owners of holding tanks also incur ongoing costs for the removal and hauling of wastewater to approved treatment facilities. Municipalities have discretion regarding the acceptance of holding tanks as the wastewater management solution for a development.

2.1.2.2. Owner's Responsibility

- 1) The owner of an *on-site wastewater treatment system* shall ensure that the system
 - a) is maintained.
 - b) is operated within the design parameters of the system, and
 - effectively treats the wastewater.

2.1.2.3. Designer and Installer Responsibility

- 1) The system designer and system installer are responsible for ensuring that
 - a) the site has been sufficiently investigated and the design has considered and addressed all pertinent factors to achieve a functional system, and
 - **b)** testing and commissioning of the system is undertaken to confirm that it operates safely, as intended by the design and meets the objectives of this Standard.

2.1.2.4. Separation from Specific Surface Waters

1) The soil-based treatment component of an on-site wastewater treatment system shall be located not less than 90 m (300 ft.) from the shore of a¹

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- a) lake,
- b) river,
- c) stream, or
- **d)** creek.

¹ Intent: Sentence (1) — The terms lake, river, stream, or creek are used specifically to separate them from other types of water courses to which this article does not apply. The purpose is to cause the location of the soil-based treatment component to be far enough from the body of water that upon a failure of surfacing effluent the effluent will not quickly and directly flow into the body of water. Alternatively, as set out in Sentence (2), the soil-based treatment component can be positioned on the lot, away from the body of water and in a location that will make a failure more easily noticed and upon failure will create an immediate inconvenience for the owner. This should result in a faster repair of the system. To achieve the intent of Sentence (2), the building does not have to be directly between the system and body of water. A water-tight septic tank or similar water tight initial treatment component does not need to meet the requirements of this Article.

2) Notwithstanding the requirements of Sentence (1), where a principal building or other development feature is situated between the soil-based treatment component and a lake, river, stream, or creek, such that a failure of the system causing effluent on the ground surface will be obvious and create an undesirable impact on the owner, the distance may be reduced to the minimum distance requirements set out in this Standard for the particular type of treatment system being used.

2.1.2.5. Prohibited Discharge Locations

- 1) Wastewater or effluent shall not be discharged
 - a) into a well, abandoned well, aquifer, or water supply,
 - b) into any surface body of water such as, but not limited to, a lake, river creek, stream, natural wetland, or constructed agua-scape/water feature.
 - c) onto any vegetable garden, or
 - d) into any other system or location not consistent with the designs provided under this Standard.

2.1.2.6. **Prohibited Wastes and Substances**

- 1) On-site wastewater treatment systems designed under the prescriptive requirements of this Standard shall not receive substances and wastewater that could adversely affect the operation of the system, which include, but are not limited to, the following:
 - a) storm water.
 - b) surface water,
 - c) abattoir waste.
 - d) sub-surface seepage water from weeping tile systems, foundation drains, or subsoil foundation drainage pipes,
 - e) clearwater waste from a hot tub, spa, or hydro massage bath that is not of the fill-anddrain design, unless the design of the system specifically includes capacity for the additional wastewater flow and instantaneous flow conditions the fixture will cause along with the potential disinfectants in the water,
 - f) clearwater waste from a swimming pool, except that the waste from the area drains around the pool area may discharge into a system,
 - commercial or industrial process wastes,
 - h) waste from a water filter or other water treatment device, if the on-site wastewater treatment system has not been designed to receive and treat the discharge from the filter or treatment device, 2,3,4
 - i) wastes from an iron filter, and
 - j) other wastes not considered in the design of the system.

Intent: Sentence (1) — The wastewater treatment systems identified in this Standard are intended for treating wastewater. Substances, contaminants, and wastewater constituents not typically expected in domestic wastewater require special consideration.

2.1.2.7. Construction Wastes Removed Prior to Commissioning a System

1) The installer of a system shall ensure that during construction of the *development*, substances that may harm or reduce the effectiveness of the system do not enter the system or are removed before the system is put into operation.

2.1.2.8. Owner's Manual

- 1) Prior to putting an on-site wastewater treatment system into operation, an operations and maintenance manual shall be made available to the owner detailing
 - a) the capacity of system design,
 - b) the principles of operation,
 - c) the construction details, including a site plan showing the specific as-built location and area occupied by treatment components,
 - d) pump capacity requirements, control settings, float elevations, and dosing volumes as applicable,
 - e) all operating and maintenance requirements, and
 - f) instructions on managing an alarm condition.
- An operations and maintenance manual shall be affixed in close proximity to the electrical service panel or another clearly visible, accessible location of the development.

2.1.3. General System Requirements — Requirements for Materials

2.1.3.1. General

1) All materials, systems, and equipment used in an on-site wastewater treatment system shall be designed for and possess the necessary characteristics to perform their intended functions.

² Warning: Clause (1)(h) — The use of water softeners and the discharge of regeneration wastes are not specifically prohibited from discharging to an on-site wastewater treatment system. The use of sodium salts in a water softener is generally more harmful to the soil-based treatment component of a treatment system than the use of potassium based salts. Increased sodium levels will be present in the domestic water used daily in the house, and may be further increased by the inefficient backwash functioning of a water softener that does not control the regeneration by flow volume. High levels of sodium can reduce the effectiveness of the on-site wastewater treatment system and reduce its life expectancy, particularly when it is located in fine-textured clay soils. Sodium occurring naturally in the groundwater or introduced to the water supply by a water softener using sodium salts may affect the ability of the soil to absorb the effluent. High sodium adsorption ratio effluent and the presence of expansive clays, such as montmorillonite clay (Refer to Appendix A.3.B. and Appendix A.3.C. for mapping of montmorillonite clays) in the soil may cause a soil-based treatment component to fail. Additional considerations from those set out in this Standard may be required.

³ Note: Clause (1)(h) — The use of potassium salts as a regeneration agent in a water softener is not expected to have the same negative effect on expansive clays as the use of sodium salts.

⁴ Warning: Clause (1)(h) — The discharge of waste from water treatment devices can generate large volumes of water that are not included in flow estimates set out in this Standard. They may generate volumes that cannot be accurately predicted or include substances that are difficult to treat or can harm the system and cause a failure.

Section 2.2. Wastewater Flow and Strength

2.2.1. Wastewater Flow and Strength — Objectives and Design Requirements

2.2.1.1. General

1) The on-site wastewater treatment system shall achieve treatment of the wastewater within the range of volume and strength of wastewater generated by the development.

2.2.1.2. Wastewater Strength Projected in Design

1) A system design shall include a projection of wastewater strength.

2.2.1.3. Methods of Projecting Wastewater Strength

- 1) The mass or concentration of constituents of concern in the wastewater shall be estimated using
 - a) values set out in this Standard,
 - **b)** published guidelines acceptable to the *Administrator*,
 - c) analytical results of wastewater samples taken following appropriate sampling and analytical protocols, or
 - **d)** wastewater quality data collected from similar establishments.

2.2.1.4. Peak Wastewater Flow for Design

- 1) The system design flow shall be based on the daily peak flow expected from the development.
- 2) The daily peak flow referred to in Sentence (1) shall be estimated using
 - a) the prescriptive requirements of this Standard,
 - b) metered flow to establish a daily peak flow design value based on applying
 - i) a safety factor of 1.5 to the mean metered flow in order to provide the required safety in design, or
 - ii) a larger factor to accommodate any potential increases in flow anticipated due to changes in use of the development over time and uncertainties in the metered flow
 - c) data collected from similar developments if an appropriate safety factor is included to accommodate peak flow, or
 - published guidelines or standards acceptable to the Administrator.
- 3) The meter referred to in Clause (2)(b) must be recorded daily for at least 30 consecutive days during a typical peak flow period or as otherwise acceptable to the Administrator.
- 4) If the daily water use of a development is expected to vary substantially between days of the week and a flow equalization and management method that effectively distributes the flow to the treatment components over a 7-day period is used, the system design may be based on the averaged 7-day peak flow calculated using the expected use frequency of the development.1

Note: Sentence (4) — Examples of a development that can expect to see variations include churches, community halls, schools, and office buildings. Flow equalization and management can increase the effectiveness of the treatment system and reduce costs.

Consideration of High Flow Plumbing Fixtures 2.2.1.5.

- 1) The system design shall include a method for managing additional volume and high instantaneous flow rates, or have the capacity to treat the wastewater at the high flow rate, where the *development* includes plumbing fixtures that
 - a) will generate high instantaneous flows, or
 - b) are likely to increase flow volumes above levels normally expected of that type of development.

2.2.1.6. Consideration of Water Conservation Plumbing Fixtures

1) Where the *development* includes low-flow or water conservation plumbing fixtures that will generate lower flow volumes, the system shall be designed to treat the increased wastewater strength that will result.

2.2.1.7. Highly Variable Flow Volumes During the Day

1) A system serving a *development*, such as, but not limited to, a motel or other facility that will generate the majority of daily flow during a short period of the day or is subject to high instantaneous flow, shall include flow equalization to attenuate the high-flow periods.

2.2.2. Wastewater Flow and Strength — Prescriptive Requirements and Installation Standards

2.2.2.1. Influent Wastewater Quality

- 1) Unless otherwise specified, the requirements of this Standard anticipate an influent raw wastewater strength that1
 - 80% of the time does not exceed
 - i) BOD_5 of 220 mg/L.
 - ii) TSS of 220 mg/L, and
 - iii) oil and grease content of 50 mg/L, and
 - b) does not exceed maximum values of
 - i) BOD_5 of 300 mg/L,
 - ii) TSS of 350 mg/L, and
 - iii) oil and grease content of 70 mg/L.

- 2) If the wastewater strength is projected to exceed the values set out in Sentence (1), the system shall
 - include additional treatment capacity to achieve the effluent quality required for the downstream component.
 - have the downstream component include additional treatment capacity appropriate for the higher wastewater strength, or
 - have a combination of the requirements referred to in Clauses (a) and (b).
- 3) If the development is non-residential, the projection of wastewater strength shall not be less than the highest strength determined by
 - the values estimated in Table 2.2.2.1. for the type of *development* listed.
 - wastewater strength projections set out in published information acceptable to the Administrator that is more specific to the development, or
 - the measured wastewater strength from similar developments.

¹ Note: Sentence (1) — At daily flow volumes assumed in this Standard.

Table 2.2.2.1. Non-Residential Projected Wastewater Strength

Note: —These values are minimums. The designer must determine and substantiate the correct wastewater strength to use in the design for the particular application. Actual values are often substantially higher than the values set out below.

Non-Residential Development	Minimum Projected Wastewater Strength, mg/L
Restaurant	600 BOD ₅ ; 400 TSS; 200 Oil & Grease
Work Camp	600 BOD ₅ ; 400 TSS; 200 Oil & Grease
Camp ground with RV dump station	600 BOD ₅ ; 400 TSS; 70 Oil & Grease

- 4) All systems, except a *lagoon*, shall include an *effluent* testing port or a readily accessible location that enables sampling of the effluent at a point downstream of any manufactured effluent treatment component and prior to discharge to the soil-based treatment component.¹ Note: Sentence (4) — Sampling from the effluent chamber may be acceptable if there is no filter required downstream of the pump.
- 5) For a system where the anticipated *wastewater* strength exceeds that of *typical wastewater*, the effluent discharged to the soil infiltration surface area shall be tested once the system is commissioned to confirm that the design has achieved the effluent quality intended by the initial treatment components.

Peak Daily Wastewater Volume 2.2.2.2.

- 1) The expected peak daily volume of wastewater used for system design shall not be less than the values provided in¹
 - Table 2.2.2.2.A. for residential developments,
 - b) Table 2.2.2.2.B. for non-residential developments, or

accordance with Article 2.2.1.4.

Intent: Sentence (1) — The expected volumes of wastewater listed in Tables 2.2.2.2.A. and 2.2.2.2.B. are for uses typically expected applications, additional fixtures, high capacity fixtures, or home designs that support entertaining events are expected to increase the load substantially. The designer and or installer must consider additional load factors when determining the expected sewage per day. The expected volume of sewage set out in these tables includes a volume that allows for a reasonable number of operational personnel.

	Table 2.2.2.A.					
Facility R	Peak expected daily wastewater volume	n Volumes of Wastewater Per D Additional capacity required based on plumbing F.U. total	Mean daily wastewater volume			
Single-family dwelling and duplex	 2 bedrooms or less: 2 people per bedroom X 340L (75 Imp. gal.) per person 3 bedrooms or more: 1.5 persons per bedroom X 340L (75 Imp. gal.) per person 	Add 50 L (11 Imp. gal.) for each fixture unit ¹ exceeding: - 25 in a 2- or 3-bedroom residence or occupancy unit - 28 in a 4-bedroom residence or occupancy unit - 31 in a 5-bedroom residence	228 L (50 Imp. gal.) per person			
Residential Occupancy other than single-family dwelling or duplex	• 340 L (75 Imp. gal.) X 2 persons per bedroom	or occupancy unit - 33 in a 6-bedroom residence or occupancy unit - the sum of 33 plus 3 F.U. per each bedroom over 6 bedrooms to determine F.U. load when there are more than 6 bedrooms	228 L (50 Imp. gal.) per person			

¹ Note: Table 2.2.2.2.A. — Fixture units are a value assigned to plumbing fixtures related to their frequency of use, rate of discharge, and anticipated volume. The following table lists fixture unit values for common fixtures. For a complete fixture unit loading list, refer to the National Plumbing Code.

Fixture	FU value	Fixture	FU value
Basin	1	Kitchen sink	1.5
Bathtub	1.5	Laundry stand pipe	2
Single head shower 2 or 3 heads	1.5 3	Laundry tray (one or two compartment)	1.5
Water Closet (toilet)flush tank	4	Floor drain 4 inch 3 inch 2 inch	3 3 2
Bathroom group	6	Bidet	1

^{*}A bathroom group (the combined load from a tub/shower, toilet and basin) is rated at 6 fixture units.

A floor drain does not need to be counted in the fixture unit load from a building unless it receives waste from a plumbing fixture or water-using device.

Table 2.2.2.B. Peak Volumes of Wastewater Per Day			
Facility	Peak daily <i>wastewater</i> volume in litres (Imp. gallons) per day		
Assembly Hall	32 (7) per seat		
Campground (full service)	80 (18) per campsite		
Church without kitchen	23 (5) per seat		
Church with kitchen	32 (7) per seat		
Construction Camp	225 (50) per person		
Day Care Centre	113 (25) per child		
Golf Club Golf Club with bar and restaurant add	45 (10) per member 113 (25) per seat		
Hospital (no resident personnel)	900 (200) per bed		
Industrial and Commercial <i>Building</i> (does not include process water, showers or a cafeteria)	45 (10) per employee		
Industrial and Commercial Building (with showers)	90 (18) per employee		
Institution (residential)	450 (100) per resident		
Laundry (coin operated)	1800 (400) per machine		
Liquor License Establishment	113 (25) per seat		
Mobile Home Park	1350 (300) per space		
Motel/Hotel	90 (18) per single bed		
Nursing and Rest Homes	450 (100) per resident		
Office Building	90 (18) per employee		
Recreational Vehicle Park (special considerations are required for systems receiving waste from RV's as the waste may contain formaldehyde, which could cause the system to fail)	180 (40) per space		
Restaurant (24-hour) Restaurant (not 24-hour)	225 (50) per seat 160 (35) per seat		
School: Elementary Junior High High School Boarding	70 (15) per student 70 (15) per student 90 (18) per student 290 (64) per student		
Service Station (not including café or restaurant)	560 (125) per fuel outlet		
Swimming Pool (public) based on design bathing load	23 (5) per person		

Additional or High Capacity Fixtures 2.2.2.3.

1) Where additional fixtures or high capacity fixtures are installed, the system shall have the capacity to manage the additional load, determined in accordance with Table 2.2.2.3. or by the application of Articles 2.2.1.4. and 2.2.1.5.1

¹ Intent: Sentence (1) — This table provides a minimum estimate of the additional volume needed to accommodate both increased overall peak flow and instantaneous loading generated by the fixture.

Table 2.2.2.3. Fixtures that Require Additional Design Capacity		
Fixture	Add to expected peak daily wastewater volume in litres (Imp. gallons) per day	
Hydro-massage and soaker tubs (fill and drain style) The design Peak Flow needs to increase to adequately handle the instantaneous flow from these fixtures. Flow equalization should be included in the system if these types of fixtures are present in the development as required by Article 2.2.1.5.	(Volume of tub in litres minus 340 liters) x 2 (Volume of tub in Imp. gallons minus 75 gal.) x 2	
Water Softener Discharge	15% increase in peak daily wastewater volume	
Other High Capacity Fixture	A volume reasonably anticipated from the specific fixture shall be added to peak daily wastewater volume and will consider the impact on peak instantaneous flow.	
High Flow Volume Showers (discharging in excess of 13 L (3 Imp. gal.) per minute)	Add 50 L (11 gallons) for every 6 L (1.5 gallons) per minute or portion thereof that exceeds a 13 L (3 Imp. gal.) per minute discharge (normal shower discharge).	

2.2.2.4. Flow Estimates with Water-Saving Fixtures

1) Where a design is based on the prescriptive requirements of this Standard, the peak daily flow estimates shall not be reduced from the values set out in Subsection 2.2.2. when water-saving fixtures or devices are used, unless adequate consideration of the increased wastewater strength is made.1

Note: Sentence (1) — Reduced water usage resulting from the use of water conservation measures or fixtures will increase wastewater strength a corresponding amount so no reduction in soil infiltration surface area should be applied.

2.2.2.5. Flow Equalization

- 1) In systems that require flow equalization
 - a) the capacity of the tank providing flow equalization shall be not less than the peak daily flow or 1.5 times the average daily flow volume, and
 - b) a pump control system shall be provided that will spread small doses of the daily wastewater volume over a 24-hour period.

2.2.2.6. Garbage Grinders

- 1) Where a garbage grinder is installed in a residential development, there shall be a
 - a) 5-percent increase to the expected peak daily *wastewater* volume projection,
 - **b)** 30-percent increase to the *wastewater* strength projection, and

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- **c)** 50-percent increase in the projected volume of sludge storage required in a *septic tank*.
- 2) In all other developments, the specific increase in loading due to the garbage grinder shall be calculated in the design.

Section 2.3. System Controls: System Flow Less than 5.7 Cubic Metres per Day

2.3.1. System Controls: System Flow Less than 5.7 Cubic Metres per Day — Objectives and Design Requirements

2.3.1.1. **Application**

1) Subsection 2.3.1. applies to all on-site wastewater treatment systems where the estimated peak wastewater flow from the development is less than 5.7 m³ (1,250 lmp. gal.) per day.

2.3.1.2. Alarms Required

- 1) All on-site wastewater treatment systems, including holding tank systems but excluding lagoons, shall include a mechanism or process capable of visually and audibly warning the user of the system when high liquid level conditions above the normal operating specifications exist.
- 2) A control system for a timed dosing system shall include an alarm that visually or audibly indicates to the user that the *wastewater* flow is exceeding the design settings of the system.
- 3) The visual and auditory alarm signals shall continue to function in the event of an electrical, mechanical, or hydraulic malfunction of the system.

2.3.1.3. Control Systems Required

1) All treatment systems shall include the necessary system controls to achieve the level of functionality, operation, and monitoring of the system required to meet the objectives and requirements of this Standard.1

Intent: Sentence (1) — Depending on the system design and treatment demands of the site, various control systems will be required. For example, if a sand filter design requires small volume time spaced dosing of effluent to achieve the expected level of treatment, the control required to achieve that must be provided.

2.3.1.4. Mounting of Water Level Control Devices

- 1) Water level indicating devices shall be mounted in a manner that allows for the
 - a) removal or adjustment of the devices without requiring the disconnection of other system components, and
 - **b)** re-installation of devices at a consistent reference elevation.
 - Note: Sentence (1) To achieve this, water level control floats are mounted on a float mast that is independent of other piping and components. This enables the removal and replacement of the water control floats or other system components in a manner that ensures float settings remain at the level intended for the design. Mounting or securing these water level control devices to the effluent piping does not achieve the intent of this Article.

2.3.1.5. Detection and Data Recording for Secondary Treatment Systems

- 1) Treatment systems where a secondary treatment level is achieved prior to distribution of the effluent to a final soil-based treatment must include a component capable of
 - a) detecting electrical or mechanical failures that are critical to the treatment process,
 - b) detecting high liquid level conditions above the normal operating specifications,
 - c) determining daily flow volumes, and

- d) collecting and recording the operational data history as defined in Clauses (a), (b), and (c) for a minimum of the previous 30 days.
- 2) The collection of operational data history shall cover a sufficient period to provide information that can be used to develop a report on the system's operational performance that can be reviewed to
 - a) evaluate operational problems,
 - b) optimize system performance, and
 - c) evaluate the achievement of treatment objectives.

System Controls: System Flow Less than 5.7 2.3.2. Cubic Metres per Day — Prescriptive Requirements and Installation Standards

2.3.2.1. Application

1) Subsection 2.3.2. applies to all on-site wastewater treatment systems where the estimated peak wastewater flow from the development is less than 5.7 m3 (1,250 lmp. gal.) per day.

2.3.2.2. Location of Alarm and Warning Devices

- 1) Alarm and warning devices shall be located where
 - a) the visual alarm signal is reasonably conspicuous to the user(s) of the system, and
 - b) the audible alarm location and signal strength are reasonably conspicuous to the user(s) of the system.

2.3.2.3. Alarm Back-up

1) The alarm shall be connected to a separate electrical circuit that is not associated with the wastewater treatment system, or shall have a battery back-up that provides a minimum of four hours' operation.

2.3.2.4. Silencing Alarm Caused by Malfunction

1) An alarm or warning device may include the ability to silence an audible alarm, provided the visual signal continues to function until the condition is corrected and the alarm includes an automatic re-setting feature.

2.3.2.5. Pump Control Redundant Off

1) When control systems for the on-site wastewater treatment system include a pump "on-offauto" switch, the control system shall be equipped with a redundant-off water level controller that prevents the pump from running in the event of inadvertent operation of the pump in the manual-on setting.

2.3.2.6. Controls and Wiring Protected From Corrosive **Environments**

1) System controls, alarm devices, and electrical connections shall not be located in any space that communicates directly with the wastewater, gases, or vapours generated from the

wastewater, unless the system control or alarm device is specifically designed for installation in the corrosive and high-moisture environment.

- 2.3.3. System Controls: System Flow Less than 5.7 Cubic Metres per Day — Requirements for Materials
- 2.3.3.1. Certification of System Controls and Alarm Devices
 - 1) System controls and alarm devices shall be specifically designed for the use in *on-site* wastewater treatment systems and certified to the applicable electrical equipment standards and comply with the Canadian Electrical Code Part 1 and provincial electrical regulations.

Section 2.4. System Controls and Monitoring: System Flow Greater than 5.7 Cubic Metres per Day

2.4.1. System Controls: System Flow Greater than 5.7 Cubic Metres per Day — Objectives and Design Requirements

2.4.1.1. Application

1) Subsection 2.4.1. applies to all *on-site wastewater treatment systems* where the estimated peak *wastewater* flow from the *development* is greater than 5.7 m³ (1,250 lmp. gal.) per day.

2.4.1.2. General

1) All treatment systems must include the necessary system controls to achieve the level of functionality, operation, and monitoring of the systems required to meet the objectives and requirements set out in this Standard.¹

¹ Note: Sentence (1) — Objectives and requirements related to a specific type of system and/or site conditions will vary and may be established in other sections of this Standard.

2.4.1.3. High Liquid Level Warning

1) All treatment systems shall include a mechanism or process capable of visually and audibly warning the user of the system when liquid levels exceed the maximum design capacity.

2.4.1.4. Holding Tank High Liquid Level Warning

1) All *holding tank* systems must include a mechanism or process capable of visually and audibly warning the user of the *holding tank* system when liquid levels exceed the normal operating specifications.

2.4.1.5. Alarm Back-Up

1) The visual and auditory alarm signals shall continue to function in the event of an electrical, mechanical, or hydraulic malfunction of the system.

2.4.1.6. Detection and Data Recording

- 1) All treatment systems must include a component capable of
 - a) detecting electrical or mechanical failures that are critical to the treatment process,
 - **b)** detecting high liquid level conditions above the normal operating specifications,
 - c) determining daily flow volumes, and
 - **d)** collecting and recording an operational data history as defined in Clauses (a), (b), and (c) for a minimum of the previous 30 days.
- 2) The collection of operational data history shall cover a sufficient period to provide information that can be used to develop a report on the system's operational performance that can be reviewed to
 - a) evaluate operational problems,
 - **b)** optimize system performance, and

evaluate the achievement of treatment objectives. c)

2.4.1.7. Mounting of Water Level Control Devices

- 1) Water level indicating devices shall be mounted in a manner that allows for the
 - a) removal or adjustment of the devices without requiring the disconnection of other system components, and
 - **b)** re-installation of devices at a consistent reference elevation. Note: Sentence (1) — Water level control floats should be mounted on a float mast that is independent of other piping and components. This enables the removal and replacement of the water control floats or other system components in a manner that ensures float settings remain at the level intended for the design. Controls cannot be mounted on wastewater piping and accomplish the intent of this Article.

2.4.1.8. Managing Flow Variation

1) The system design shall have features, including tanks and controls, that effectively manage daily or day-to-day flow variations to optimize system effectiveness and function.¹ Intent: Sentence (1) — This would typically be accomplished with adequate tank volume and timed dosing controls.

2.4.1.9. Monitoring Wells

1) The system design shall include *vertical separation* monitoring wells that extend to a depth below grade sufficient to confirm that the required vertical separation from the soil infiltration surface to saturated soil conditions is maintained during operation of the system; these monitoring wells shall be located within or immediately adjacent to the soil-based treatment area.1

¹Note: Sentence (1) — The purpose of the vertical separation well is to enable monitoring of soil water conditions within the soil depth below the infiltration surface of the wastewater system needed for effective treatment (the required vertical separation). These vertical separation wells are not used to measure depth to the water table. Vertical separation wells should not go to a depth that extends into a lower soil profile having a significantly higher hydraulic conductivity rate than the soil at the infiltration surface. If there are significant changes in the underlying profile, additional vertical separation wells should be provided; some to the depth of the required vertical separation and some to a lesser depth that can confirm overlying finer textured soils with a lower hydraulic conductivity have not become saturated creating a perched water table.

- 2) An on-site wastewater treatment system serving a development expected to generate more than 5.7 m³ (1,250 lmp. gal.) in peak daily wastewater flow shall include a minimum of 3 groundwater monitoring wells to a minimum depth of 15 m (50 ft.), at least one up gradient and two down gradient as measured by groundwater elevation, located to optimize the measurement of groundwater impact, if the system is located above GWUDI which meets the criteria of a domestic use aquifer.
- 3) An on-site wastewater treatment system serving a development that is expected to generate more than 9 m³ (1,980 lmp. gal.) in peak daily wastewater flow shall include a minimum of 3 groundwater monitoring wells to a minimum depth of 15m (50 ft.), at least one up gradient and two down gradient as measured by groundwater elevation, located to optimize the measurement of groundwater impact where a system is located within 2 km (1.25 miles) of a
 - a) lake,
 - b) river,
 - creek, or
 - stream.
- 4) Notwithstanding the requirements of Sentence (2) and (3) that set out a minimum depth of 15m (50 ft.), in no case shall a monitoring well required by this Standard be developed into a confined aquifer.
- 5) The design shall include monitoring ports that can be used to monitor effluent ponding on the soil infiltration surface of a soil-based treatment system or on the surface of the treatment

- medium used in a system to improve effluent quality such as, but not limited to, a treatment mound or sand filter.
- 6) Effluent sampling ports or access shall be provided in locations as required by the design to confirm that treatment and operational objectives are achieved prior to application of the wastewater effluent to the soil infiltration surface.
- 2.4.2. System Controls and Monitoring: System Flow Greater than 5.7 Cubic Metres per Day — Prescriptive Requirements and Installation Standards

2.4.2.1. Application

1) Subsection 2.4.2. applies to all *on-site wastewater treatment systems* where the estimated peak wastewater flow from the development is greater than 5.7 m³ (1,250 lmp. gal.) per day.

2.4.2.2. Installation

1) System controls and alarm devices shall be installed in compliance with the Canadian Electrical Code Part 1 and provincial electrical regulations.

2.4.2.3. Protection from Harmful Vapours

1) System controls, alarm devices, and electrical connections shall not be located in any space that communicates directly with the wastewater, gases, or vapours generated from the wastewater, unless the system control or alarm device is specifically designed for installation in the corrosive and high-moisture environment.

2.4.2.4. Pump Control Redundant Off

- 1) The on-site wastewater treatment system shall be equipped with a redundant-off water level controller for the pump that prevents the pump from running in the event of a failure of the main-off water level control or inadvertent operation of the pump in the manual-on setting.
- 2.4.3. System Controls and Monitoring: System Flow Greater than 5.7 Cubic Metres per Day — Requirements for Materials

2.4.3.1. Certification of System Controls and Alarm Devices

1) System controls and alarm devices shall be certified to the applicable electrical equipment standards and comply with the Canadian Electrical Code Part 1 and provincial electrical regulations.

Section 2.5. Piping

2.5.1. Piping — Objectives and Design Standards

2.5.1.1. Leaking

1) Piping shall not leak except where intended in the design.

2.5.1.2. Freezing

1) The system design shall prevent the freezing of liquids in the piping.

2.5.1.3. Grading and Sizing

1) Piping shall be sloped and sized to accommodate the designed flow of wastewater or effluent and the drainage of piping when required to prevent freezing.

Intent: Sentence (1) — Gravity piping must maintain a slope required for the flow volume and drain completely. Pressure piping must maintain sufficient slope to drain when required to prevent freezing. Pressure distribution piping shall be of sufficient size to deliver the required volume at the required pressure. Tables A.1.C.1., A.1.C.2., A.1.C.3., and A.1.C.4. in Appendix A may be used for sizing of pressure distribution piping, manifolds, and supply piping at the required pressure-head loss.

2.5.1.4. Supports

- 1) Piping shall be sufficiently supported to
 - a) prevent sagging,
 - withstand expected mechanical forces, and
 - withstand forces resulting from the movement of liquid in the system.

2.5.1.5. Design Pressure Rating

1) Piping shall be approved for a pressure rating of at least 1.5 times the maximum pressure it may be subjected to by the system design.

2.5.2. Piping — Prescriptive Requirements and Installation Standards

2.5.2.1. Sewer Line Support

1) Effluent sewers and distribution header piping shall be evenly and continuously supported.

2.5.2.2. Distribution Header Support

1) A distribution header serving weeping lateral trenches at different elevations shall be evenly and continuously supported on a bed of undisturbed or tightly compacted earth between trenches to adequately support the piping and prevent migration of effluent to a lower lateral.¹ Intent: Sentence (1) — To support the pipe and to prevent the migration of effluent through the ground from a weeping lateral trench

at a higher elevation into another weeping lateral trench at a lower elevation.

2.5.2.3. Protection from Freezing

1) A building sewer or effluent sewer having less than 1200 mm (4 ft.) of soil cover where it crosses under a ditch, driveway, or path shall be protected from freezing by a frost box, culvert, or other equivalent means.

2.5.2.4. Sizing

1) Effluent sewer piping shall not be smaller than 75 mm (3 in.) in pipe size.

2.5.2.5. Slope of Sewer Piping

- 1) A 100 mm (4 in.) building sewer or effluent sewer shall have a minimum slope of 1% ($\frac{1}{8}$ inch
- 2) A 75 mm (3 in.) building sewer or effluent sewer shall have a minimum slope of 2% ($\frac{1}{4}$ inch per foot).

2.5.2.6. Backfill

1) Backfill shall be carefully placed to prevent damage or dislocation of piping, and the backfill shall be free of stones, boulders, cinders, and frozen earth for a minimum depth of 150 mm (6 in.) above the piping.1

Intent: Sentence (1) — To prevent damage to the pipe during and after backfill.

2.5.2.7. Piping Connections to Tank

- 1) Piping connections to any tank or vessel used in the treatment systems shall be water-tight, flexible connections that will prevent *infiltration* and exfiltration and continue to provide a water-tight connection in the event the tank or piping shifts.
- 2) Piping connected to any tank or vessel shall be supported to within 300 mm (1 ft.) of the tank outlet or inlet on a solid soil base, or equivalent bridging provided.¹
- 3) Gravity drainage piping connected to a tank shall be DWV pipe or piping of equivalent structural strength for at least 1800 mm (6 ft.) from the tank.
 - 1 Intent: Sentence (2) The inlet and outlet piping connected to a tank must be protected from distortion caused by settling of the backfill material. The excavation for a tank should not be any longer than is necessary to install the tank. This provides undisturbed earth closer to the tank to support the inlet and outlet piping connected to the tank. A pipe with a greater wall thickness provides an added safety factor.
 - ² Intent: Sentence (3) The inlet and outlet piping connected to a tank are subject to distortion caused by settling of the tank and the excavation around the tank. Heavy wall pipe, and close excavation to minimize the distance to undisturbed earth, provides an added element of safety that is needed.

2.5.3. Piping — Requirements for Materials

2.5.3.1. Piping in Pressure Applications

- 1) The piping used in a pressure application shall be *certified* to one of the following standards:1
 - a) for pressure effluent line:
 - i) CAN/CSA-B137.1, "Polyethylene Pipe, Tubing and Fittings for Cold Water Pressure Services," (Series 160 with compression fittings or Series 75, 100 or 125 with insert fittings), or
 - ii) CAN/CSA-B137.3, "Rigid Polyvinyl Chloride (PVC) Pipe for Pressure Applications,"
 - **b)** for pressure effluent distribution lateral pipe:
 - i) CAN/CSA-B137.3, "Rigid Polyvinyl Chloride (PVC) Pipe for Pressure Applications,"
 - ii) CAN/CSA-B137.6, "CPVC Pipe, Tubing and Fittings for Hot and Cold Water Distribution Systems," or
 - c) pipe deemed acceptable to the Administrator for the intended application.

Note: Sentence (1) — Table A.5.A. lists piping and its acceptable applications.

2.5.3.2. Piping in Gravity Applications

- 1) The piping used for an effluent sewer, or gravity distribution header, shall be certified to one of the following standards:
 - a) CAN/CSA-B181.1, "ABS Drain, Waste, and Vent Pipe and Pipe Fittings,"
 - b) CAN/CSA-B181.2, "PVC Drain, Waste, and Vent Pipe and Pipe Fittings,"
 - c) CAN/CSA-B182.1, "Plastic Drain and Sewer Pipe and Pipe Fittings," or
 - d) CAN/CSA-B182.2, "PVC Sewer Pipe and Fittings, (PSM Type)."
- 2) Where there is no existing standard for the intended use of a piping material, piping use shall comply with Table A.5.A., "Piping Materials."

2.5.3.3. **Joints**

1) Every joint between pipes and fittings of dissimilar materials or sizes shall be made by adapters, connectors, or mechanical joints manufactured and certified for that purpose.

Section 2.6. Pressure Distribution of Effluent

2.6.1. Pressure Distribution — Objectives and Design Requirements

2.6.1.1. General

1) A pressure distribution lateral pipe system shall be designed to provide positive control of the volume of effluent delivered to the treatment component as determined by the design loading rate.

2.6.1.2. Orifice Discharge Volume

- 1) The volume of effluent discharged through any orifice in the distribution lateral pipe system as measured over the duration of a single dosing cycle shall not vary by more than 1
 - a) 10 percent along the length of a single distribution lateral pipe, and
 - b) 15 percent between all orifices in the system, unless specifically designed for in the system to accommodate variations in soil conditions.

¹ Note: Sentence (1) — When using pressure distribution laterals, the volume discharged from each orifice should not differ by more than the percentage set out in Clauses (a) and (b) except where varying soil conditions dictate that the loading rate needs to differ within the system. This may occur where soil conditions vary over the soil infiltration area. When determining the volume discharged from a single orifice, the differences in head pressure at the orifice and differences in the length of time effluent is discharged from each orifice requires consideration. In pressure delivery systems where the system supplies effluent to laterals of different lengths and relies on gravity to distribute effluent along the length of the trench, it may be necessary to vary the volume discharged at the outlet to each trench to match the desired loading rate.

2.6.1.3. Effluent Pressure Distribution Lateral Pipe Objective

- 1) When secondary treated effluent is applied to the soil interface, the design and/or spacing of the orifices shall be such that the effluent is spread over the soil interface in a manner that results in a soil moisture content that does not vary by more than 20% over the entire soil interface area, as measured at a depth of 75–175 mm (3–7 in.) below the soil interface.
- 2) The requirements of Sentence (1) do not apply when the pressure distribution system is designed as a pressure distribution header to supply gravity distribution weeping lateral trenches receiving primary treated effluent Level 1 doses.

2.6.1.4. Orifices Elevated Above Infiltration Surface

1) Distribution lateral piping shall be installed so that each orifice opening is an adequate distance above the soil infiltration surface to prevent drain back into the system should intermittent ponding occur.

2.6.1.5. Pressure Distribution Lateral System Design

- 1) The design of a pressure distribution lateral pipe system shall
 - a) determine the pressure head and flow rate the pump supplying the system must be capable of by considering
 - i) static lift measured from the minimum effluent level in the dosing tank to the elevation of the perforated distribution piping,
 - ii) pressure head required at the orifices,
 - iii) volume discharged from orifices, and
 - iv) head loss resulting from piping at the calculated design flows using a Hazen Williams coefficient of smoothness determined for the type of piping used in the system,¹

- b) maintain a flow velocity in the piping of not less than 0.6 m/s (2 ft/s) except that in an effluent distribution lateral pipe this minimum velocity is required only at the supply end of the effluent distribution lateral pipe,²
- c) maintain a flow velocity in the piping that does not exceed 1.5 m/s (5 ft/s) where the system includes any quick-closing valves,
- d) maintain a minimum pressure head of
 - i) 1.5 m (5 ft.) at all orifices that are 4.8 mm (³/₁₆ in.) or less in *diameter*, and
 - ii) 0.6 m (2 ft.) when orifices are larger than 4.8 mm (³/₁₆ in.) in *diameter*,
- e) use orifices in the lateral that are
 - i) not smaller than 3.2 mm (¹/₈ in.) in diameter, and
 - ii) spaced at a distance required to achieve the objectives of even distribution and in no case more than 1.5 m (5 ft.) apart when applying primary treated effluent Level 1, or more than 0.9 m (3 ft.) when applying secondary treated effluent,
- f) be capable of delivering a dose volume that is equal to or less than the volume per dose required by the downstream system design,³
- g) result in a distribution lateral pipe volume that is less than 20% of an individual dose volume.
- h) include an effluent filter that prevents particles 3.2 mm (¹/₈ in.) in diameter or larger from being discharged into the effluent distribution system, and
- i) include piping arrangements that result in components of the system being readily accessible from the ground surface to carry out the
 - i) flushing and cleaning of the individual laterals at the most downstream end of the lateral.
 - ii) checking of residual pressure head at both the supply end and most downstream end of the lateral, and
 - iii) regular maintenance and servicing of filters, pumps, and valves without requiring physical entry into a tank.

2.6.2. Pressure Distribution — Prescriptive Requirements and Installation Standards

2.6.2.1. Design

- 1) A pressurized distribution lateral pipe system shall have
 - a) distribution lateral piping not smaller than 19 mm (3/4 in.) in diameter,
 - b) distribution lateral pipe of a size determined by Table A.1.A. for the required size and number of orifices, or by using good engineering practice that achieves the objectives of a pressure distribution lateral pipe system design for achieving treatment goals, and
 - c) a distribution lateral pipe for each chamber assembly where chambers are used.

¹ Note: Subclause (1)(a)(iv) — Pipe friction loss tables can be found in Appendix A. These tables can be used to determine the size of main effluent supply piping and distribution headers. In large or complex systems where laterals are at different elevations, specific engineering of the system design may be required.

² Intent: Clause (1)(b) — the size of the effluent distribution pipe should be selected to maintain the required velocity while not exceeding pressure loss limits along the lateral.

³ Intent: Clause (1)(f) — Numerous light applications of effluent provide better treatment conditions. The individual doses should be evenly spaced over a 24-hour period to further improve treatment.

2.6.2.2. Orifices

- 1) Orifices in a distribution lateral pipe shall
 - a) point upwards and not form an angle greater than 45° with the vertical, except when 1
 - i) required for pipe drainage, the number of orifices required for effective drainage may point downward if equipped with suitable orifice shields, or
 - ii) the lateral is encased in *drain media* all orifices may point downward,
 - **b)** be equipped with orifice shields to prevent blocking of the orifice when encased in *drain* media.
 - be spaced at a distance of not greater than
 - i) 1.5 m (5 ft.) when distributing primary treated effluent Level 1,
 - ii) 900 mm (36 in.) when distributing secondary treated effluent, or
 - iii) the distance specified when using an approved distribution method that has been tested to meet the objectives of Article 2.6.1.3., and
 - d) not exceed the maximum number of orifices specified for the pipe size as set out in

2.6.2.3. Dose Volume 5 Times Pipe Volume

1) The volume of an individual dose to be distributed over the soil infiltration surface area using a pressure distribution lateral pipe system shall be at least 5 times the volume of the distribution lateral pipe but shall not exceed the maximum individual dose volume needed to deliver the required number of doses per day.

2.6.2.4. Lateral Length

1) An individual pressure distribution lateral pipe, as measured from the pressure distribution supply header to the last orifice, shall not exceed 20 m (65 ft.) in length.

2.6.2.5. Pressure Head at Orifices

- 1) The system design shall ensure a *pressure head* of not less than
 - a) 1.5 m (5 ft.) at orifices that are 4.8 mm (³/₁₆ in.) in *diameter* or smaller, and
 - **b)** 600 mm (2 ft.) at orifices larger than 4.8 mm (³/₁₆ in.) in *diameter*.

2.6.2.6. Orifices Flevated Above Infiltration Surface

1) Where the effluent distribution system is designed to enable drain back of the distribution lateral piping to the dosing tank, the piping shall be installed so that each orifice opening is a minimum of 100 mm (4 in.) above the soil infiltration surface.¹

Intent: Sentence (1) — The elevation above the infiltrative surface should be maximized. The orifices in the piping must be above the soil infiltration surface by an adequate distance to prevent drain back into the system if intermittent ponding were to occur on the soil infiltration surface.

2.6.2.7. Piping Supports

1) Distribution lateral piping that is not encased in media shall be supported at intervals of 1.2 m (4 ft.) or less, unless specified otherwise by the pipe manufacturer.

¹ Intent: Clause (1)(a) — Locating the orifice on the upper half of the pipe can help prevent clogging of the orifice from accumulated biological growths. Wherever the orifices are located, the orifices must be protected from rocks setting on the orifice and there must be room for the effluent to escape. The spraying effluent must not cause any erosion of the soil or sand around it.

2.6.3. Pressure Distribution — Requirements for Materials

Piping 2.6.3.1.

1) Piping used in a pressure distribution lateral pipe system shall meet the requirements of Section 2.5.

2.6.3.2. Effluent Filters and Service Access

- 1) Filters used in a pressure distribution lateral pipe system must
 - a) be suitable for wastewater applications,
 - b) provide filtration to smaller than 3.2 mm (1/8 in.) particle size,
 - c) be sized for the required flow rate of the system design and to provide a service interval frequency desired for the system, and
 - be located and installed so they are readily accessible from ground surface for servicing.

2.6.3.3. **Pumps**

1) Pumps used in a pressure distribution lateral pipe system must be suitable for wastewater applications and able to produce the volume of effluent at the pressure head required by the system design.

Part 3 Holding Tanks

Section 3.1. Holding Tanks

3.1.1. Holding Tanks — Objectives and Design Standards

3.1.1.1. Storage Capacity

1) A holding tank serving a detached single-family dwelling shall have a storage capacity of not less than 4,500 L (1,000 lmp. gal).¹

¹ Intent: Sentence (1) - It is not the intent of this Standard to exclude the use of a septic tank as a holding tank provided the requirements of the Standard are met regarding holding tanks. The capacity of the holding tank should be large enough to make effective use of trucking service and provide a reserve volume for the owner.

2) A *holding tank* for *developments* other than a detached single-family *dwelling* shall have a storage capacity suitable for the intended service.

3.1.1.2. Infiltration/Exfiltration Prevention

- 1) Holding tank access openings, manhole extensions, and piping connections shall prevent infiltration and exfiltration.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed, the design of the system shall address
 - a) anti-floatation measures required,
 - **b)** the ability of the tank to withstand structural stresses caused by the hydrostatic pressure and buoyancy, and
 - **c)** maintaining the elevation of piping connections above the projected *water table*, or include other specific additional measures to ensure *infiltration* does not occur through piping connections or manhole access risers.

3.1.2. Holding Tanks – Prescriptive Requirements and Installation Standards

3.1.2.1. Separation Distances

- 1) Holding tanks shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 1 m (3.25 ft.) of a property line, and
 - **d)** 1 m (3.25 ft.) of a *building*.

3.1.2.2. Service Access

1) Holding tank manhole access openings shall be brought above ground surface and have access openings for waste removal brought to a height above the surrounding landscape that ensures that surface water will drain away from the access openings.¹

¹ Intent: Sentence (1) — Access openings above the ground provide readily available access to the tank as compared to buried access openings, particularly when the ground is frozen. The manhole access may be buried if wastewater removal pipes are provided for aboveground access.

2) A holding tank shall be located and installed to accommodate the regular removal of wastewater by vacuum truck or other approved means.¹

Intent: Sentence (2) — Holding tanks are meant to hold a volume of wastewater and facilitate the removal of wastewater for treatment in a municipal lagoon or other suitable location.

3.1.2.3. Access Opening Lid/Cover

- 1) All access openings shall be equipped with a secure lid or cover.¹
 - Intent: Sentence (1) To increase safety by preventing unauthorized or accidental entry into the access opening of a septic tank or holding tank. Acceptable protective measures include, but are not limited to, a padlock, a cover that can only be removed with tools, or a cover having a minimum weight of 29.5 kg (65 lb).
- 2) The opening of a manhole access that extends above ground shall be insulated to an equivalent R-8 insulation value in order to protect the tank contents from freezing.

3.1.2.4. Base for Holding Tank

1) The bottom of an excavation for a holding tank shall provide a uniform base to support the tank in a level position and meet the manufacturer's installation instructions. 1

 1 Intent: Sentence (1) — A tank must have a stable base so it will not settle, shift, or crack after installation.

3.1.2.5. Insulation of Tank

1) A holding tank that has less than 1.2 m (4 ft.) of earth cover to protect it from freezing conditions shall be insulated to provide the equivalent of an R-8 insulation value at the top and sides of the tank to a minimum depth of 1.2 m (4 ft.) below grade or insulated in some other acceptable manner to achieve a level of protection from freezing that is equivalent to a tank that has a minimum 1.2 m (4 ft.) cover of the in situ soil.

3.1.3. Holding Tanks - Requirements for Materials

3.1.3.1. General

1) A holding tank shall be approved equipment that is certified by an accredited testing agency as meeting or exceeding the requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks."

Part 4 Initial Treatment Components Primary

Section 4.1. Primary Treatment

4.1.1. Primary Treatment — Objectives and Design Standards

Effluent Treatment Quality 4.1.1.1.

- 1) Except as permitted in Sentence (2), an initial treatment component intended to provide primary treatment of the wastewater prior to discharge to a soil-based final treatment component shall, at least 80% of the time, produce a primary treated effluent Level 1 having a strength that does not exceed any of the following concentrations:
 - a) $cBOD_5$: 150 mg/L,
 - TSS: 100 mg/L, and
 - oil and grease: 15 mg/L.
- 2) The effluent discharged from a primary treatment component to a downstream soil-based component may be of a stronger effluent strength than set out in Sentence (1) if the design of downstream treatment component has been based on receiving that higher strength effluent.

4.1.1.2. Sludge and Scum Accumulation

 A primary treatment tank (septic tank) shall include the capacity to store accumulating sludge and scum for a period of at least 3 years without reducing the hydraulic retention capacity to less than the design daily peak flow.

Note: Sentence (1) — This does not set the standard of tank pumping interval at three years. The tank must be regularly inspected (yearly is a good target) to determine sludge depth and pumped only when needed. Depending on actual use, the frequency may vary from one year to five. To minimize the amount of sludge trucked to outside treatment facilities the tank should only be pumped

Section 4.2. Septic Tanks

4.2.1. Septic Tanks — Objectives and Design Standards

4.2.1.1. Working Capacity

- 1) Except where a lesser volume is allowed in Article 4.2.2.2., a primary treatment (septic) tank
 - a) have a minimum working capacity of not less than the expected daily peak wastewater volume determined under Section 2.2., and
 - include an additional capacity of not less than
 - i) 400 L (88 Imp. gal.) per expected occupant in a residential development to accommodate sludge and scum accumulation, 1 or
 - an amount required for sludge accumulation following Table A.6.A. for other than residential occupancies.
 - The amount of storage provided for sludge and scum accumulation shall be increased by 1.5 times when a garbage grinder is used, unless that volume has already been included in the application of the requirements in Article 2.2.2.6.

Note: Subclause (1)(b)(i) — The additional capacity of 400 L (88 Imp. gal.) per person to accommodate sludge and scum accumulation is based on the anticipated sludge and scum accumulation rate of 135 L (30 Imp. gal.) per person per year at a 95% confidence level for residential applications and a 3-year targeted pump-out interval.

4.2.1.2. Service Access

1) The system design shall consider the location and depth below grade of the primary treatment component (septic tank) to facilitate accessibility for septage removal, service, and maintenance.1

Intent: Sentence (1) — The tank should be located where it is unlikely a deck or other structure may be built over the tank or where access may be otherwise limited for removal of septage by a vacuum truck. The depth of the tank should not exceed the practical suction elevation of vacuum trucks in order to enable septage removal.

4.2.1.3. Infiltration/Exfiltration Prevention

- 1) Tank access openings, manhole extensions, and piping connections shall prevent *infiltration* and exfiltration of wastewater and groundwater.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed, the design of the system shall
 - a) include the anti-floatation measures required,
 - b) ensure the tank can withstand the structural stresses caused by the hydrostatic pressure and buovancy, and
 - maintain the elevation of piping connections above the projected water table level, or include other specific additional measures to ensure that infiltration does not occur through piping connections or manhole access risers.

Insulation of Tank 4.2.1.4.

1) A septic tank shall have adequate earth cover or other means to protect it from freezing while in operation and during periods of non-use.

4.2.2. Septic Tanks — Prescriptive Requirements and Installation Standards

4.2.2.1. Separation Distances

- 1) Septic tanks shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 1 m (3.25 ft.) of a property line, and
 - **d)** 1 m (3.25 ft.) of a *building*.

4.2.2.2. Working Capacity

- 1) The working capacity of a septic tank shall not be less than
 - a) the volume set out in Table 4.2.2.2. for a single-family dwelling or duplex, or
 - **b)** the volume required by Article 4.2.1.1.

¹ Note: Clause 1) a) - Table 4.2.2.2. provides the working capacity volume required of the septic tank for residential applications where there are no conditions that require additional flow to be added to the peak daily volume.

Table 4.2.2.2. Working Capacity of Septic Tank				
Number of Bedrooms	Working Capacity Volume			
2 or 3 bedrooms	3,360 L (740 lmp. gal.)			
4 bedrooms	4,260 L (940 Imp. gal.)			
5 bedrooms	5,220 L (1,150 lmp. gal.)			
6 bedrooms	6,130 L (1,350 lmp. gal.)			

4.2.2.3. Septic Tank Manhole Access Not Buried

 Septic tank access openings shall not be buried and shall be located at a height above the surrounding landscape that ensures surface water will drain away from the access opening.¹

¹ Intent: Sentence (1) — Access openings above the ground provide readily available access to the tank as compared to buried access openings, particularly when the ground is frozen. An above-ground access also encourages regular maintenance and provides a permanent and visible marker of the location of the tank.

4.2.2.4. Access Opening Lid/Cover

1) All access openings shall be equipped with a secure, air-tight lid or cover.¹

¹ Intent: Sentence (1) — This requirement increases safety by preventing unauthorized or accidental entry into the access opening of a septic tank or holding tank. Acceptable protective measures include, but are not limited to, a padlock, a cover that can only be removed with tools, or a cover having a minimum weight of 29.5 kg (65 lb). The lid or cover is airtight in order to contain the odour.

2) All access openings shall be insulated to provide the equivalent of an R-8 insulation value.

4.2.2.5. Access Opening Extensions Water-tight

1) Access opening extensions shall be installed to ensure a water-tight connection to the *septic tank* and at the joints between all sections of the extensions.

4.2.2.6. Insulation of Tank

1) A septic tank that has less than 1.2 m (4 ft.) of earth cover to protect it from freezing conditions shall be insulated to provide the equivalent of an R-8 insulation value over the top and sides of the tank to a minimum depth of 1.2 m (4 ft.) below grade, or insulated in some other acceptable manner to achieve a level of protection from freezing that is equivalent to a tank that has a minimum 1.2 m (4 ft.) cover of the in situ soil.

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4.2.2.7. Base for Septic Tank

1) The bottom of an excavation for a septic tank shall provide a uniform base to support the tank in a level position and meet the manufacturer's installation instructions.¹

¹ Intent: Sentence (1) — A tank must have a stable base so it will not settle, shift, or crack after installation.

4.2.3. Septic Tanks — Requirements for Materials

4.2.3.1. General

1) A septic tank shall be approved equipment that has been certified by an accredited testing agency as meeting or exceeding the requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks."

Part 5 Initial Treatment Components — Secondary Treatment

Section 5.1. Secondary Treatment

5.1.1. Secondary Treatment — Objectives and Design Standards

Secondary Effluent Treatment Qualities 5.1.1.1.

1) Except as permitted in Sentence (2), an initial treatment component intended to produce secondary treated effluent shall, at least 80% of the time, produce an effluent quality that does not exceed the appropriate values set out in Table 5.1.1.1.

¹ Note: Sentence (1) — Level one treatment standard is equivalent to Primary Treatment. Thus, this table starts at Level 2.

Table 5.1.1.1. Secondary Treated Effluent						
	Maximum Concentration ¹ In Treated Effluent					
Treatment Type ²	Basic Treatment Level		Disinfection (D) ³	Phosphorus Reduction (P)	Nitrogen Reduction (N)	
	TSS,	CBOD ₅ ,	Fecal Coli,	Total	Total Nitrogen	
			or <i>E. coli,</i>	Phosphorus,	_	
	mg/l	mg/l	CFU/100 ml	mg/l		
Level 2	30	25				
Level 3	15	15				
Level 4	10	10				
D-I			50 000			
D-II			200			
D-III			ND⁴			
P-I				1		
P-II				0.3		
N-I					50% Reduction	
N-II					75% Reduction	

¹ No tolerances apply to these requirements, because the given values take into consideration the inaccuracy of the measurement.

² A system's overall treatment classification is denoted by the applicable treatment types written in sequence, i.e. Level 2-DII-NI.

Requirements for fecal coliform organisms or E. coli can be used for the purposes of Type D treatment. Reactivation after disinfection was not taken into consideration in establishing these requirements.

⁴ ND = non-detectable (median < 10 CFU/100 ml).

2) The effluent produced by a secondary treatment component used in an on-site wastewater treatment system design may vary from the quality referred to in Sentence (1) if the design of the downstream treatment component is based on receiving effluent of a quality that the secondary treatment component will achieve at least 90% of the time under the operating conditions.

5.1.1.2. Wastewater Sampling Access

1) A secondary treatment component shall include sampling ports or a suitable location to obtain wastewater and effluent samples to confirm treatment performance and assess operation of the component.¹

 1 Intent: Sentence (1) — The system should include at least a sampling port to determine effluent quality and a sampling port for influent wastewater to assess system operation and facilitate troubleshooting of the treatment component.

Section 5.2. Packaged Sewage Treatment Plants

5.2.1. Packaged Sewage Treatment Plants — Objectives and Design Standards

5.2.1.1. General

- 1) The effluent from a packaged sewage treatment plant used in an on-site wastewater treatment system shall discharge to a downstream soil-based treatment system as allowed in Part 8 or 9, and the effluent shall meet or exceed the effluent quality parameters required by the downstream final treatment components.
- 2) Except where the design of a certified packaged sewage treatment plant includes a pretreatment tank or chamber, a pre-treatment tank having a working capacity of not less than 0.75 of the peak daily volume of design wastewater flow shall be installed upstream of a packaged sewage treatment plant.

5.2.1.2. Treatment Capacity

- 1) The required treatment capacity of a packaged sewage treatment plant used in an on-site wastewater treatment system shall consider the
 - expected peak hydraulic load,
 - expected strength of the wastewater from the development, b)
 - extent of wastewater flow variation throughout a day, and
 - variations in wastewater flow from day to day.

5.2.1.3. Accessible Location

- The location of a packaged sewage treatment plant shall be selected with consideration to¹
 - accessibility for regular servicing,
 - accessibility for periodic removal of sludge, and
 - minimizing concerns with periodic odour problems that may occur.
 - 1 Intent: Sentence (1) The plant should be located where it is unlikely a deck or other structure may be built over the tank or where access may be otherwise limited for removal of sludge by a vacuum truck. The depth of the tank should not exceed the practical suction elevation of vacuum trucks at the truck access point.

5.2.1.4. Insulation of Tank

1) A packaged sewage treatment plant shall have adequate earth cover or other means to protect it from freezing while in operation and during periods of non-use.

5.2.1.5. Infiltration/Exfiltration Prevention

- 1) Tank access openings, manhole extensions, and piping connections shall prevent *infiltration* and exfiltration of wastewater and groundwater.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed, the design of the system shall
 - a) include any anti-floatation measures required,
 - b) ensure that the tank can withstand the structural stresses caused by the hydrostatic pressure and buoyancy, and

c) maintain the elevation of piping connections above the projected water table level, or include other specific additional measures to ensure that infiltration does not occur through piping connections or manhole access risers.

5.2.2. Packaged Sewage Treatment Plants — Prescriptive Requirements and Installation Standards

5.2.2.1. Separation Distances

- 1) A packaged sewage treatment plant shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 6 m (20 ft.) of a property line, and
 - **d)** 1 m (3.25 ft.) of a *building*.
- 2) Notwithstanding Sentence (1), a packaged sewage treatment plant may be located not less than 1 m (3.25 ft.) from a property line if
 - a) equipped with odour control mechanisms.¹
 - b) the plant serves a development where the peak daily flow is less than 5.7 m³ (1,250 lmp. gal.) per day, and
 - c) the strength of the wastewater from the development does not exceed typical wastewater strength.
 - Note: Clause (2)(a) Odour control mechanisms may include the relocation of the vent from the treatment unit to a suitable location.
- 3) Notwithstanding Sentences (1) and (2), a packaged sewage treatment plant serving a development generating more than 5.7 m³ (1,250 lmp. gal.) but less than 25 m³ (5,500 lmp. gal) per day shall be located
 - a) not less than
 - i) 100 m (330 ft.) from the *property* line of an unrelated *development*, if not equipped with odour control devices, and
 - ii) not less than 25 m (82 ft.) from the development served, or
 - b) when equipped with odour control devices, the distance may be less than set out in Clause (a) but not less than the distance away from the development served and the property line of unrelated developments needed to minimize odour impact both on the development and at the property line of unrelated developments.

5.2.2.2. Wastewater Strength

1) A packaged sewage treatment plant shall not receive wastewater having a strength that exceeds typical wastewater unless it can be demonstrated the packaged sewage treatment plant has the capacity to treat the organic loading of the wastewater to achieve the effluent quality required by these standards.

5.2.2.3. Treatment Capacity

- 1) A packaged sewage treatment plant used in an on-site wastewater treatment system shall have a rated treatment capacity
 - a) of not less than the expected peak volume of wastewater per day determined in accordance with Section 2.2., and
 - **b)** that meets the requirements of Article 5.2.1.2.

5.2.2.4. Service Access Not Buried

1) Packaged sewage treatment plant access openings shall not be buried and shall be located at a height above the surrounding landscape that ensures surface water will drain away from the access opening.1

Intent: Sentence (1) — To ensure an access opening for required maintenance.

5.2.2.5. Access Openings Equipped with Lid/Cover

Packaged sewage treatment plant access openings shall be equipped with a secure lid or

 1 Intent: Sentence (1) — To increase safety by preventing unauthorized or accidental entry into the access opening. Acceptable protective measures include, but are not limited to, a padlock, a cover that can only be removed with tools, or a cover having a minimum weight of 29.5 kg (65 lb).

2) All man-way access openings shall be insulated to provide the equivalent of an R-8 insulation value.

5.2.2.6. Base for Packaged Sewage Treatment Plant

1) The bottom of an excavation for a packaged sewage treatment plant shall provide a uniform base to support the tank in a level position and meet the manufacturer's installation instructions.1

 1 Intent: Sentence (1) — A tank must have a stable base so it will not settle, shift, or crack after installation.

5.2.2.7. Insulation of Tank

1) A packaged sewage treatment plant that has less than 1.2 m (4 ft.) of earth cover to protect it from freezing conditions shall be insulated to provide the equivalent of an R-8 insulation value over the top and sides of the tank to a minimum depth of 1.2 m (4 ft.) below grade, or insulated in some other acceptable manner in order to achieve a level of protection from freezing that is equivalent to a tank with a minimum 1.2 m (4 ft.) cover of the in situ soil.

5.2.3. Packaged Sewage Treatment Plants — Requirements for Materials

5.2.3.1. Equipment Structural Requirements and Operational Certification

- 1) Packaged sewage treatment plants shall be certified as meeting the
 - a) National Sanitation Foundation (NSF/ANSI) Standard 40, Class 1, for "Residential Wastewater Treatment Systems,"
 - b) CAN/BNQ-3680-600 Standard for Onsite Residential Wastewater Treatment Technologies, or
 - c) CSA B128.3 Standard for the Performance of Non-potable Water Reuse Systems.
- 2) In addition to Sentence (1), tanks used for packaged sewage treatment plants shall be certified as meeting the structural and material requirements of
 - a) CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks," or
 - b) BNQ Standard NQ 3680-905/208, "Prefabricated Septic Tanks for Residential Use Dimensional and Physical Characteristics."

Section 5.3. Secondary Treatment — Sand Filters

Sand Filters — Objectives and Design Standards 5.3.1.

5.3.1.1. General

1) The treatment objective of an intermittent sand filter is to treat the wastewater to a secondary treated effluent Level 3 standard.

Effluent Treatment Quality 5.3.1.2.

- 1) The effluent produced by an intermittent sand filter that receives primary treated effluent Level 1 shall, at least 80% of the time, be of a quality characterized by the following:
 - a) $cBOD_5$ of less than 15 mg/L,
 - **b)** TSS of less than 15 mg/L.
 - c) less than 50,000 CFU/100 mL, and
 - d) oil and grease content of less than 5 mg/L.

5.3.1.3. Coarse-Sand Sand Filter

- 1) A coarse-sand intermittent sand filter shall
 - a) use filter media as specified in Sentence 5.3.3.4.(1), and
 - **b)** have a filter-media *infiltration* surface area that is based on
 - i) peak daily flow volumes.
 - ii) an effluent hydraulic loading rate of not more than 100 L per square metre (2 Imp. gal. per sq. ft.) per day, and
 - iii) an organic loading rate of not more than 0.015 kg cBOD₅ per sq. metre per day based on peak daily flow volumes.

Medium-Sand Sand Filter 5.3.1.4.

- 1) A medium-sand intermittent sand filter shall
 - a) use filter media as specified in Sentence 5.3.3.4.(2), and
 - b) have a filter media infiltrative surface area based on
 - i) peak daily flow volumes.
 - an effluent hydraulic loading rate of not more than 40 L per square metre (0.83 Imp. gal. per sq. ft.) per day, and
 - an average organic loading rate of not more than 0.0075 kg cBOD₅ per sq. metre per day based on peak daily flow volumes.

5.3.1.5. Application of Effluent

- 1) Effluent shall be evenly applied to the filter media infiltrative surface using a pressure distribution lateral pipe system meeting the requirements of Section 2.6.
- 2) Effluent shall be applied to the filter media infiltrative surface in dose volumes that do not exceed1
 - a) 30% of the *field capacity* of the filter media per dose when using timed dosing, or
 - **b)** 20% of the *field capacity* of the filter media per dose when using demand dosing. Intent: Sentence (2) — Numerous light applications of effluent provide better treatment conditions. This requirement results in between approximately 12 and 24 doses per day to meet the percentage of field capacity per dose. The amount may vary depending on the filter media. A timing device to control the pump is desirable to provide a wait period between each volume per flush and also to provide volumes per flush evenly spaced over a 24-hour period.

5.3.1.6. Alarm Signals

- 1) A sand filter shall include a device capable of
 - a) detecting a high effluent level condition in the sand filter, and
 - **b)** delivering a visible and audible signal to alert the user of the system that the *effluent* level is above normal operating levels.

5.3.1.7. Prevention of Infiltration/Exfiltration

A sand filter container shall prevent the infiltration and exfiltration of water.
 Note: Sentence (1) — A suitable liner containing the sand filter is required to prevent the infiltration and exfiltration of water. A berm may be required on the upslope side of the sand filter to prevent surface storm water runoff from entering the sand filter.

5.3.1.8. Above Ground Filters

- 1) A sand filter constructed above ground or partially above ground shall
 - a) have a container that is capable of holding the filter media and withstanding hydraulic and mechanical forces that may be encountered, and
 - **b)** include additional insulation to minimize the effect of cold weather that is equivalent to the *soil*-insulating factor of a buried *sand filter*.

5.3.1.9. Soil Cover

- Where a soil cover is required, the soil cover over the sand filter surface area and the area immediately around it shall be graded to shed precipitation and to minimize the entrance of surface runoff water and precipitation into the sand filter.
- 2) Except as permitted in Sentence (3), the *soil* cover over the *sand filter* shall be a *soil texture* that allows sufficient air to enter the *sand filter media* below the *soil* cover in order to satisfy the oxygen demand created by the treatment processes in the *sand filter*.
- 3) A piping system may be used to supply an adequate air supply to the *sand filter media* as an alternative to the permeable *soil* cover described in Sentence (2).

5.3.1.10. Open Bottom Sand Filter or Packed Bed Media Filter System Not Allowed

1) An open bottom sand filter design or other open bottom packed bed filter system shall not be used.

5.3.2. Sand Filters — Prescriptive Requirements and Installation Standards

5.3.2.1. Separation Distances

- 1) A sand filter shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 1 m (3.25 ft.) of a property line as measured from the foot of the berm, and
 - **d)** 1 m (3.25 ft.) of a *building*.

5.3.2.2. Base for Intermittent Sand Filter

1) An intermittent sand filter shall be on a stable and level base.

5.3.2.3. Intermittent Sand Filter

- 1) An intermittent sand filter system shall have underdrain piping to collect treated effluent that shall
 - a) extend the full length of the sand filter,
 - **b)** be located at the bottom of the sand filter.
 - c) extend to the surface at both ends of the underdrain piping,
 - d) be located in drain media that has a minimum depth of 150 mm (6 in.), and
 - e) enable collection of the effluent at the bottom of the sand filter to ensure positive drainage to a depth of at least 200 mm (8 in.) below the sand laver.
- 2) An intermittent sand filter system shall have a method of removing effluent collected at the bottom of the sand filter by the underdrain piping that includes the following: 1,2
 - a) a pump housed in a corrosion-resistant vault that will
 - i) withstand the mechanical stresses that it will be subject to,
 - ii) prevent the migration of drain media, sand, or underdrain media to its interior, and
 - iii) provide water-tight access to finished landscape grade with a diameter equal to that of the vault, or
 - **b)** piping that drains to an *effluent*-dosing tank that is external to the sand filter where the effluent is removed by a pump, and
 - c) the depth of underdrain media and the upper operating limit of the associated-effluent pump cycle and alarm shall not allow effluent to rise within 50 mm (2 in.) of the bottom of the filter media.
 - ¹ Note: Sentence (2) The underdrain piping should be installed in a manner that ensures the load of the media above does not press the pipe into the bottom of the sand filter liner, effectively closing the openings in the piping; see applicable sections in the handbook for design and installation procedures.
 - ² Note: Sentence (2) An underdrain pipe laid in the centre of the sand filter along the long axis quickly collects effluent. If the underdrain pipe extends beyond the sand filter to a dose tank, care must be taken to prevent freezing of the pipe, as the trickling effluent will readily freeze. The pump vault may be used as the dosing tank for the downstream soil-based final treatment component if the capacity of the pump vault provides sufficient volume for the dosing of the system.
- 3) Above the drain media, a layer of underdrain media having a minimum depth of 50 mm (2 in.) shall be placed over the layer of drain media that supports the sand filter media.¹
 - Intent: Sentence (3) The media immediately under the filter media (underdrain media, which is pea gravel as specified in Sentence 5.3.3.6.(1)) should be small enough to support the filter media. Below this supporting layer, the underdrain piping should be enveloped in a coarse drain media (larger sized rock, Article 5.3.3.5.) to provide less restriction of effluent flow into the underdrain piping. The layers below the filter media must provide effective drainage to ensure aerobic conditions.
- 4) Above the underdrain media, a minimum depth of 600 mm (2 ft.) of sand filter media shall be placed in a manner that ensures a uniform density and a top surface which is level. 1
 - ¹ Note: Sentence (4) The moisture content of the sand media may cause different placement techniques to ensure uniform density of the sand media.
- 5) A pressurized distribution lateral pipe system shall be included that
 - a) meets the requirements of Section 2.6.,
 - **b)** is situated above the filter media layer, and
 - is placed in
 - i) clean drain media with a minimum depth of 75 mm (3 in.) below the distribution lateral pipes, and that covers the orifice shields protecting the distribution lateral pipe orifices, or
 - ii) a chamber system that is installed in accordance with the manufacturer's instructions and covers a minimum of 90% of the filter media area.
- 6) A geo-textile fabric shall cover the top of the drain media or chamber system in which the pressure distribution lateral pipe system is installed.

- 7) A soil shall cover the intermittent sand filter surface area that
 - a) has a depth of not less than 150 mm (6 in.) and not more than 300 mm (12 in.),
 - b) is of a texture of fine sand, loamy coarse sand, loamy medium sand, or coarse sandy loam.1 and

 - has been seeded to grass or covered with sod.²
 Intent: Clause (7)(b) The soil covering the sand filter must be a coarse soil texture to allow a free flow of air into the sand filter.
 - ² Note: Clause (7)(c) Grass cover must be established as soon as possible to prevent erosion of the soil cover and promote the runoff of precipitation.
- 8) There shall be monitoring ports extending from finished *grade* down to the top of the filter media laver that
 - a) are located so that there is not less than 1 per each 3 m by 3 m (10 ft. by 10 ft.) area of sand layer.
 - b) are located in each continuous row of chambers, if chambers are used,
 - c) have a minimum diameter of 100 mm (4 in.).
 - d) have horizontal or vertical saw cuts from the bottom of the pipe to a height of 100 mm (4) in.) to allow the entry of effluent,
 - e) are accessible from the surface, and
 - f) are equipped with removable caps.

5.3.2.4. **Distribution Laterals**

- 1) The distribution lateral pipe system used to spread the effluent over the sand filter surface area shall meet the requirements of Section 2.6. and shall be designed so that
 - a) there is not less than one orifice for
 - i) each 0.55 m² (6 ft²) of filter media surface *infiltration* area in a medium-sand sand
 - ii) each 0.18 m² (2 ft²) of filter media surface *infiltration* area in a coarse-sand sand
 - b) each orifice serves an area whose length does not exceed its width by more than 1.5 times, and
 - c) the orifices in adjacent laterals create an offset pattern to maximize distribution.

5.3.2.5. Above Ground

1) A sand filter constructed entirely or partially above ground shall be insulated with polystyrene that provides a minimum R-8 insulation value, and shall be provided with a surrounding soil berm having a slope not steeper than 1 vertical to 3 horizontal, or a concrete enclosure having the structural capacity to carry the loads placed on walls.

5.3.3. Sand Filters — Requirements for Materials

5.3.3.1. Underdrain Piping

- 1) *Underdrain piping* shall
 - a) not be smaller than NPS 4 in. pipe with saw cuts halfway through the piping at approximately 50 mm (2 in.) spacing, or
 - b) be an alternative product that will effectively collect effluent from below the filter media without clogging.

5.3.3.2. Sand Filter Container

- 1) A sand filter container shall be
 - a) a reinforced concrete container.
 - b) constructed of other materials that will provide an equivalent performance in which water tightness is expected, or
 - c) a flexible membrane liner having properties that are at least equivalent to 0.76 mm or 760 µm thick (0.03 in.) unreinforced polyvinyl chloride (PVC), protected by a 75 mm (3 in.) thick sand layer beneath the liner.

5.3.3.3. Test for Media

- 1) The sand filter media, drain media, and underdrain media specified in Articles 5.3.3.4., 5.3.3.5., and 5.3.3.6., respectively, shall be tested to determine conformance
 - a) in accordance with ASTM C-136, "Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates," and in conjunction and accordance with ASTM C-117, "Standard Test Method for Materials Finer than No. 200 Sieve in Mineral Aggregates by Washing," and
 - **b)** by a qualified third party.

5.3.3.4. Filter Media

- 1) Except as permitted in Sentence (3), the sand used as filter media in a coarse-sand sand filter shall be well-washed and consist of the following particle size:
 - 100 percent passing the 9.51 mm (3/8 in.) sieve,
 - **b)** 77 to 100 percent passing the 4.76 mm (0.187 in.), No. 4 sieve,
 - c) 53 to 100 percent passing the 2.36 mm (0.0937 in.), No. 8 sieve,
 - d) 15 to 80 percent passing the 1.18 mm (0.0469 in.), No. 16 sieve,
 - e) 3 to 50 percent passing the 0.6 mm (0.0234 in.), No. 30 sieve,
 - f) 0 to 2 percent passing the 0.3 mm (0.0117 in.), No. 50 sieve,
 - g) 0 to 1 percent passing the 0.15 mm (0.0059 in.), No. 100 sieve
 - h) a uniformity coefficient (CU) of between 1 and 4, and
 - an effective particle size (D_{10}) of 0.4 to 0.9 mm.
- 2) Except as permitted in Sentence (3), the sand used as filter media in a medium-sand sand filter shall be well-washed and have a particle size that meets the following criteria:
 - a) 100 percent passing the 9.51 mm (3/8 in.) sieve,
 - **b)** 95 to 100 percent passing the 4.76 mm (0.187 in.), No. 4 sieve,
 - c) 80 to 100 percent passing the 2.36 mm (0.0937 in.), No. 8 sieve.
 - d) 45 to 85 percent passing the 1.18 mm (0.0469 in.), No. 16 sieve,
 - e) 15 to 60 percent passing the 0.6 mm (0.0234-in.), No. 30 sieve,
 - f) 3 to 10 percent passing the 0.3-mm (0.0117-in.), No. 50 sieve,
 - g) 0 to 1 percent passing the 0.15-mm (0.0059 in.), No. 100 sieve,
 - h) a uniformity coefficient (CU) of between 1 and 4, and
 - an effective particle size (D_{10}) of 0.3 to 0.5 mm.
- An alternative media to what is provided in Sentences (1) and (2) may be used as the filter media provided it
 - a) is of equivalent durability,
 - b) has a particle size consistent with the size required for use in a coarse-sand sand filter or medium-sand sand filter.
 - c) is inert so that it will maintain its integrity and not collapse or disintegrate with time, and
 - **d)** is not detrimental to the performance of the intermittent sand filter.

5.3.3.5. Drain Media

- 1) Except as permitted in Sentence (2), drain media shall be clean, washed gravel; clean, crushed rock; or other equivalent media for distributing effluent, with particle size of the following consistency:
 - a) 100 percent passing the 38.1 mm (1-1/2 in.) sieve,
 - b) 50 to 100 percent passing the 9.51 mm (3/8 in.) sieve,
 - c) 6 to 84 percent passing the 4.76 mm (0.187 in.), No. 4 sieve,
 - d) 0 to 24 percent passing the 2.36 mm (0.0937 in.), No. 8 sieve, and
 - e) 0 to 1 percent passing the 1.18 mm (0.0469 in.), No. 16 sieve.
- 2) An alternative media to what is provided in Sentence (1) may be used provided it
 - a) is of equivalent durability,
 - b) has a particle size consistent with the size set out in Sentence (1),
 - c) is inert so that it will maintain its integrity and not collapse or disintegrate with time, and
 - **d)** is not detrimental to the treatment performance of the system.

5.3.3.6. Underdrain Media

- 1) Underdrain media shall be clean, washed pea gravel, or equivalent material with a particle size of the following consistency:
 - a) 100 percent passing the 12.7 mm ($\frac{1}{2}$ in.) sieve.
 - **b)** 50 to 100 percent passing the 9.51 mm, (3/8 in.) sieve,
 - c) 6 to 84 percent passing the 4.76 mm (0.187 in.), No. 4 sieve,
 - d) 0 to 24 percent passing the 2.36 mm (0.0937 in.), No. 8 sieve, and
 - e) 0 to 1 percent passing the 1.18 mm (0.0469 in.), No. 16 sieve.

Section 5.4. Secondary Treatment — Re-circulating **Gravel Filters**

5.4.1. Re-circulating Gravel Filters — Objectives and Design Standards

5.4.1.1. General

1) The treatment objective of a re-circulating gravel filter shall be to treat the wastewater to a secondary treated effluent Level 2 standard.

5.4.1.2. Infiltration Surface Area

- 1) A re-circulating gravel filter using a minimum filter depth media of 600 mm (2 ft.), as specified in Article 5.4.3.4., shall be designed to have a filter media infiltrative surface area based on
 - a) peak daily flow volumes.
 - b) an effluent hydraulic loading rate of not more than 200 L/m2 (4 lmp. gal./ft2) per day, and
 - c) an organic loading rate of not more than 0.04 kg cBOD₅/m² per day.

5.4.1.3. Application of Effluent

- 1) Effluent shall be evenly applied to the filter-media-layer infiltrative surface using a pressuredistribution lateral pipe system meeting the requirements of Section 2.6. and Article 5.3.2.4.
- 2) Effluent shall be applied to the filter-media infiltrative surface in doses that 1
 - a) occur not less than 48 times per day,
 - b) occur at intervals of not more than 30 minutes, and
 - c) do not exceed 8 L (1.76 lmp. gal.) discharged from a single orifice per dose. 1 Intent: Sentence (2) — Numerous light applications of effluent provide better treatment conditions. A timing device to control the pump is desirable to provide a wait period between each volume per flush and also to provide volumes per flush evenly spaced over a 24-hour period.

5.4.1.4. **Effluent Tank**

- 1) A re-circulating gravel filter design shall include a mixing/re-circulation effluent tank that
 - a) has a capacity of 150 percent of peak daily flow volume for residential applications,
 - b) has a capacity of 100 percent peak daily flow volume for commercial applications.
 - c) receives effluent from the upstream primary treatment component,
 - d) receives effluent from the re-circulating gravel filter, and
 - e) includes components required to achieve a 4 to 1 re-circulation ratio.

5.4.1.5. Minimum of One Pass before Discharge

1) The re-circulating gravel filter design shall ensure effluent has passed through the gravel filter at least once prior to discharge to a downstream treatment system component.

5.4.1.6. Detection/Alarm

- 1) A re-circulating gravel filter shall include a device capable of
 - a) detecting a high effluent-level condition, and

b) delivering a visible and audible signal to alert the user(s) of the system that the effluent level is above normal operating levels.

Infiltration/Exfiltration Prevention 5.4.1.7.

1) A re-circulating gravel filter container shall prevent the infiltration and exfiltration of water.

5.4.1.8. Above Ground

- 1) A re-circulating gravel filter constructed above ground or partially above ground shall
 - a) have a container that is capable of holding the filter media and withstanding hydraulic and mechanical forces that may be encountered, and
 - b) provide insulation from cold weather equivalent to the soil insulating factor of a buried gravel filter.

Open Bottom Re-circulating Gravel Filter Not Allowed 5.4.1.9.

1) An open bottom *re-circulating gravel filter* design shall not be used.

5.4.1.10. Soil Cover

1) Where a soil cover is required, the soil cover over a re-circulating gravel filter and the area immediately around it shall be graded to shed precipitation and prevent surface-water run-off from entering the re-circulating gravel filter.

5.4.2. Re-circulating Gravel Filters — Prescriptive Requirements and Installation Standards

5.4.2.1. Separation Distances

- 1) A re-circulating gravel filter shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a water course,
 - c) 3 m (10 ft.) of a property line measured from the foot of the berm, and
 - **d)** 1 m (3.25 ft.) of a *building*.
- 2) Notwithstanding Sentence (1), a re-circulating gravel filter designed to treat in excess of 5.7 m³ (1,250 lmp. gal.) per day shall be located a sufficient additional distance away from buildings and property lines to ensure that odour impact is minimized.

5.4.2.2. Base for Filter

1) A re-circulating gravel filter shall be on a stable and level base.

5.4.2.3. Re-Circulating Gravel Filter System

- 1) A re-circulating gravel filter system shall contain underdrain piping to collect effluent that shall¹
 - a) be located at the bottom of the re-circulating gravel filter,
 - **b)** extend the full length of the *re-circulating gravel filter*,
 - extend to the surface at both ends of the underdrain pipe,
 - d) provide positive drainage to a depth of at least 200 mm (8 in.) below the filter media layer, and

- connect to a pump vault within the re-circulating gravel filter, or extend beyond the edge of the re-circulating gravel filter to provide gravity drainage to the mixing/re-circulation
 - ¹Note: Sentence (1) An underdrain pipe laid in the centre of the re-circulating gravel filter along the long axis collects effluent
- 2) A re-circulating gravel filter system shall contain pumps and control systems that shall ensure that the effluent collected in the bottom on the gravel filter does not come to within 50 mm (2 in.) of the bottom of the filter media.
- 3) The layer of drain media containing the underdrain piping shall have a minimum depth of 150 mm (6 in.).
- 4) The layer of drain media referred to in Sentence (3) shall be covered with a layer of underdrain media specified in Article 5.3.3.6. having a minimum depth of 50 mm (2 in.). Intent: Sentence (4) — The media immediately under the filter media (underdrain media, which is pea gravel as specified in Sentence 5.3.3.6.(1) should be small enough to support the filter media. Below this supporting layer, the underdrain piping should be enveloped in a coarse drain media (larger sized rock, Article 5.3.3.5.) to provide less restriction of effluent flow into the underdrain piping. The layers below the filter media must provide effective drainage to ensure aerobic conditions.
- 5) A minimum of 600 mm (2 ft.) of filter media above the *underdrain media* shall have a level surface and be placed in a manner to ensure uniform density.
- 6) A pressurized distribution lateral pipe system shall be installed that
 - a) is situated above the filter media layer,
 - b) is placed in clean drain media with a minimum depth of 75 mm (3 in.) below the distribution lateral pipes, and that covers the orifice shields, or
 - c) when placed in a chamber system, the chambers shall
 - i) be installed in accordance with the manufacturer's instructions,
 - ii) cover a minimum of 90% of the gravel area, and
 - iii) be set on a minimum of 50 mm (2 in.) of drain media covering the filter media layer.
- 7) A geo-textile fabric shall cover the top of the drain media or chamber system in which the pressure-distribution lateral pipe system is installed.
- 8) The re-circulating gravel filter area shall by covered by a layer of soil that
 - a) has a depth of not less than 150 mm (6 in.) and not more than 300 mm (12 in.),
 - **b)** is of a soil texture classification no finer than loamy coarse sand. ¹ and
 - c) has been seeded to grass or covered with sod.²
 - Intent: Clause (8)(b) The soil covering the re-circulating gravel filter must be very coarse to allow a free flow of air into the gravel

9) There shall be two monitoring ports with a minimum diameter of 100 mm (4 in.) that are accessible from the surface and extend down to the top of the filter media layer.

5.4.2.4. Orifice Spacing

- 1) The distribution lateral pipe system shall be designed so that
 - a) there is not less than one orifice for each 0.18 m² (2 ft.²) of filter media surface *infiltration* area.
 - b) each orifice serves an area whose length does not exceed its width by more than 1.5 times, and
 - c) the orifices in adjacent laterals create an offset pattern to maximize distribution.

² Note: Clause (8)(c) — Grass cover must be established as soon as possible to prevent erosion of the soil cover.

5.4.2.5. Pumps

- 1) Where collected *effluent* is removed from the *re-circulating gravel filter* using a pump located within the *gravel filter*,
 - a) the pump and related apparatus shall be housed in a corrosion resistant vault designed to
 - i) withstand the stresses placed upon it,
 - ii) prevent the migration of drain media, gravel, or underdrain media to its interior, and
 - **iii)** provide water-tight access to finished landscape *grade* with a *diameter* equal to that of the vault, and
 - b) the depth of *underdrain media* and the operating level of the pump cycle and alarm shall not allow *effluent* to rise within 50 mm (2 in.) of the bottom of the filter media.

5.4.2.6. Above Ground Containment

- 1) A re-circulating gravel filter constructed entirely or partially above ground shall be
 - a) provided with a
 - i) surrounding soil berm having a slope not steeper than 1 vertical to 3 horizontal, or
 - ii) concrete enclosure having the structural capacity to carry the loads placed on walls, and
 - b) insulated with polystyrene or equivalent on the walls of the enclosure that provides a minimum R-8 insulation value.

5.4.3. Re-circulating Gravel Filters — Requirements for Materials

5.4.3.1. Underdrain Piping

1) *Underdrain piping* shall not be smaller than NPS 4 inch pipe with saw cuts halfway through the pipe at approximately 50 mm (2 in.) spacing.

5.4.3.2. Re-Circulating Gravel Filter Container

- 1) A re-circulating gravel filter container shall be constructed of
 - a) reinforced concrete or materials that will provide performance and water tightness equivalent to a reinforced concrete container, or
 - b) a flexible membrane liner
 - i) having properties that are at least equivalent to 0.762 mm or 762 μm thick (0.03 in.) unreinforced polyvinyl chloride (PVC), and
 - ii) protected by a 75 mm (3 in.) layer of *sand* beneath the liner that is adequately supported by structurally sufficient sidewall supports provided by void forms when further supported by surrounding earth *berms* or concrete walls.

5.4.3.3. Test Requirements for Gravel Filter Media

- 1) The *re-circulating gravel filter* media shall be tested to determine conformance with the criteria outlined in Article 5.4.3.4. by a sieve analysis test
 - a) in accordance with ASTM C-136, "Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates," and in conjunction with ASTM C-117, "Standard Test Method for Materials Finer than No. 200 Sieve in Mineral Aggregates by Washing," and
 - **b)** performed by a qualified third party.

5.4.3.4. Gravel Filter Media

- 1) The gravel used as filter media shall
 - a) have a *uniformity coefficient* of less than or equal to 2.
 - **b)** have an effective particle size (D_{10}) of 3-4 mm, and
 - c) be washed *gravel* consisting of the following particle sizes:
 - i) 100 percent passing the 9.50 mm (3/8 in.) sieve,
 - ii) 0 to 95 percent passing the 4.76 mm (0.187 in.), No. 4 sieve.
 - iii) 0 to 2 percent passing the 2.36 mm (0.0937 in.), No. 8 sieve, and
 - iv) 0 to 1 percent passing the 0.6 mm (0.0234 in.), No. 30 sieve.
- 2) An alternative media to what is provided in Sentence (1) may be used as filter media if it
 - a) is of equivalent durability,
 - b) has a particle-size distribution consistent with the particle-size distribution required for use in a re-circulating gravel filter,
 - c) is inert so that it will maintain its integrity and not collapse or disintegrate with time, and
 - **d)** is not detrimental to the performance of the *re-circulating gravel filter*.

Part 6 Initial Treatment Components — Effluent and Pre-treatment Tanks

Section 6.1. Effluent Tanks

6.1.1. Effluent Tanks — Objectives and Design Standards

6.1.1.1. General

1) The objective of an *effluent tank* is to retain *effluent* in order to enable the effective delivery of *effluent* in dosed volumes to a downstream component.

6.1.1.2. Tank Capacity

1) Effluent tanks shall have a capacity to manage the wastewater flow as required by design of the downstream component.

6.1.1.3. Prevention of Infiltration/Exfiltration

- 1) Effluent tank access openings and manhole extensions and piping connections shall prevent infiltration and exfiltration.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed, the design of the system shall
 - a) include any anti-floatation measures required,
 - **b)** ensure that the tank can withstand structural stresses caused by the hydrostatic pressure and buoyancy, and
 - **c)** maintain the elevation of piping connections above the projected *water table* level, or include other specific additional measures to ensure that *infiltration* does not occur through piping connections or manhole access risers.

6.1.1.4. Insulation of Tank

1) An *effluent tank* shall have adequate earth cover or other means to protect it from freezing while in operation and during periods of non-use.

6.1.2. Effluent Tanks — Prescriptive Requirements and Installation Standards

6.1.2.1. Separation Distances

- 1) Effluent tanks shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 1 m (3.25 ft.) of a property line, and
 - **d)** 1 m (3.25 ft.) of a building.

6.1.2.2. Service Access

- 1) Effluent tank access openings shall not be buried and shall be located at a height above the surrounding landscape that ensures surface water will drain away from the access opening.¹ Intent: Sentence (1) — Aboveground access openings provide readily available access to the tank as compared to buried access openings, particularly when the ground is frozen. Aboveground access also encourages regular maintenance and provides a permanent and visible marker of the location of the tank.
- All access openings shall be insulated to provide the equivalent of an R-8 insulation value.

6.1.2.3. Access Openings Equipped with Lid/Cover

1) All access openings shall be equipped with a secure lid or cover.¹ Intent: Sentence (1) — To increase safety by preventing unauthorized or accidental entry into the access opening. Acceptable

protective measures include, but are not limited to, a padlock, a cover that can only be removed with tools, or a cover with a minimum weight of 29.5 kg (65 lb).

6.1.2.4. Base for Effluent Tank

1) The bottom of an excavation for an effluent tank shall provide a uniform base to support the tank in a level position and meet the manufacturer's installation instructions. 1

¹ Intent: Sentence (1) — A tank must have a stable base so it will not settle, shift, or crack after installation.

6.1.2.5. Insulation of Tank

1) An effluent tank with less than 1.2 m (4 ft.) of earth cover to protect it from freezing conditions shall be insulated to provide the equivalent of an R-8 insulation value at the top and sides of the tank to a minimum depth of 1.2 m (4 ft.) below grade, or insulated in some other acceptable manner so as to achieve a level of protection from freezing that is equivalent to a tank with a minimum 1.2 m (4 ft.) cover of the in situ soil.

6.1.3. Effluent Tanks — Requirements for Materials

6.1.3.1. General

1) An effluent tank shall be approved equipment that has been certified by an accredited testing agency as meeting or exceeding the structural and material requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks."

Section 6.2. Settling Tanks (Pre-Treatment)

6.2.1. Settling Tanks — Objectives and Design Requirements

6.2.1.1. General

1) The objective of a *settling tank* is to reduce the strength of *wastewater* to a level that is suitable for the downstream component; it may also be used as an *equalization tank* to enable flow equalization with or without the objective of reducing the *wastewater* strength.

6.2.1.2. Settling Tank Used as Pre-aeration Tank

1) A settling tank may be used as a pre-aeration tank where required by the system design.

6.2.1.3. Capacity

1) Settling tanks shall have the capacity to pre-treat and manage the wastewater flow as required by the downstream component and system design.

6.2.1.4. Prevention of Infiltration/Exfiltration

- 1) Settling tank access openings, manhole extensions, and piping connections shall prevent infiltration and exfiltration.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed, the design of the system shall
 - a) include any anti-floatation measures required,
 - **b)** ensure that the tank can withstand structural stresses caused by hydrostatic pressure and buoyancy, and
 - **c)** maintain the elevation of piping connections above the projected *water table* level, or include other specific additional measures to ensure that *infiltration* does not occur through piping connections or manhole access risers.

6.2.1.5. Insulation of Tank

1) A *settling tank* shall have adequate earth cover or other means to protect it from freezing while in operation and during periods of non-use.

6.2.1.6. Service Access

1) The system design shall consider the location and depth below *grade* of the *settling tank* to facilitate accessibility for septage removal, service, and maintenance.¹

¹ Intent: Sentence (1) — The tank should be located where it is unlikely that a deck or other structure will be built over the tank or where access may be otherwise limited for removal of septage by a vacuum truck. The depth of the tank should not exceed the practical suction elevation of vacuum trucks in order to enable septage removal.

6.2.2. Settling Tanks — Prescriptive Requirements and Installation Standards

6.2.2.1. Separation Distances

1) Settling tanks shall not be located within

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- a) 10 m (33 ft.) of a water source or water well,
- **b)** 10 m (33 ft.) of a *water course*,
- c) 1 m (3.25 ft.) of a *property* line, and
- **d)** 1 m (3.25 ft.) of a *building*.
- 2) Notwithstanding Sentence (1), a settling tank that includes pre-aeration in its function shall not be located within
 - a) 10 m (33 ft.) of a water source,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 6 m (20 ft.) of a property line, and
 - **d)** 1 m (3.25 ft.) of a *building*.
- 3) Notwithstanding Sentences (1) and (2), a settling tank that includes pre-aeration in its function may be located not less than 1 m (3.25 ft.) from a property line if
 - a) equipped with odour control mechanisms,
 - b) the plant serves a development where the peak daily flow is less than 5.7 m³ (1,250 lmp. gal.) per day, and
 - c) the strength of the wastewater from the development does not exceed typical wastewater strength.
- 4) Notwithstanding Sentences (1), (2), and (3), a settling tank that includes pre-aeration in its function, and serves a development generating more than 5.7 m³ (1,250 lmp. gal.) but less than 25 m³ (5,500 lmp. gal.) per day, shall be located
 - a) if not equipped with odour control devices, not less than
 - i) 100 m (330 ft.) from the property line of an unrelated development, and
 - ii) not less than 25 m (82 ft.) from the development served, or
 - b) when the settling tank is equipped with odour control devices, the distance may be less than set out in Clause (a) but not less than the distance away from the development served and the property line of unrelated developments needed to minimize odour impact on the *development* and at the *property* line of unrelated *developments*.

6.2.2.2. Access Openings Above Ground

- 1) Settling tank access openings shall not be buried and shall be located at a height above the surrounding landscape that ensures surface water will drain away from the access opening. 1 ¹ Intent: Sentence (1) — Access openings above the ground provide readily available access to the tank as compared to buried access openings, particularly when the ground is frozen. Aboveground access also encourages regular maintenance and provides a permanent and visible marker of the location of the tank.
- 2) All access openings shall be insulated to provide the equivalent of an R-8 insulation value.

Access Openings Equipped with a Secure Lid/Cover 6.2.2.3.

1) All access openings shall be equipped with a secure lid or cover.¹

 1 Intent: Sentence (1) - To increase safety by preventing unauthorized or accidental entry into the access opening of a settling tank. Acceptable protective measures include, but are not limited to, a padlock, a cover that can only be removed with tools, or a cover with a minimum weight of 29.5 kg (65 lb).

6.2.2.4. Base for Settling Tank

1) The bottom of an excavation for a settling tank shall provide a uniform base to support the tank in a level position and meet the manufacturer's installation instructions. 1

Intent: Sentence (1) — A tank must have a stable base so it will not settle, shift, or crack after installation.

6.2.2.5. Protection from Freezing

1) A settling tank with less than 1.2 m (4 ft.) of earth cover to protect it from freezing conditions shall be insulated to provide the equivalent of an R-8 insulation value over the top and sides of the tank to a minimum depth of 1.2 m (4 ft.) below grade, or insulated in some other acceptable manner to achieve a level of protection from freezing that is equivalent to a tank that has a minimum 1.2 m (4 ft.) cover of the in situ soil.

Settling Tanks — Requirements for Materials 6.2.3.

6.2.3.1. General

1) A settling tank shall be certified by an accredited testing agency as meeting or exceeding the structural and material requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks."

Section 6.3. Lift Stations

6.3.1. Lift Stations - Objectives and Design Requirements

General 6.3.1.1.

- 1) The objective of a *lift station* is to accumulate incoming raw wastewater, which is then periodically pumped to a higher elevation where it enters other components or sewer lines in the *wastewater* management and treatment system.
- 2) The design capacity and pumping controls used with the *lift station* shall be capable of supplying small doses of wastewater to the downstream component so that large amounts of wastewater discharged at rapid transfer rates do not overload the capacity of the downstream components.1

Note: The design capacity of the lift station should consider the need for and volume required to provide some emergency storage in the event of a pump failure or power outage.

6.3.1.2. Control Infiltration

- 1) Lift station tank access openings, manhole extensions, and piping connections shall prevent infiltration and exfiltration.
- 2) Where the site evaluation identifies high groundwater conditions at the location and elevation the tank is installed the design of the system shall
 - a) include any anti-floatation measures required,
 - b) ensure that the tank can withstand structural stresses caused by the hydrostatic pressure and buoyancy, and
 - c) maintain the elevation of piping connections above the projected water table level, or include other specific additional measures to ensure that infiltration does not occur through piping connections or manhole access risers.

6.3.1.3. Insulation of Tank

1) A lift station tank shall have adequate earth cover or other means to protect it from freezing while in operation and during periods of non-use.

6.3.1.4. Service Access

1) The system design shall consider the location and depth below *grade* of the *lift station* to facilitate accessibility for service and maintenance.

Intent: Sentence (1) — The tank should be located where it is unlikely that a deck or other structure will be built over the tank or where access for service may be otherwise limited.

6.3.2. Lift Stations — Prescriptive Requirements and Installation Standards

6.3.2.1. Separation Distances

- 1) Lift stations shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a water course,
 - c) 1 m (3.25 ft.) of a property line, and

- **d)** 1 m (3.25 ft.) of a building.
- 2) Notwithstanding Sentence (1), if a lift station tank also provides another function, such as pretreatment or equalization, the requirements for that other type of tank shall apply.

6.3.3. Lift Stations - Requirements for Materials

6.3.3.1. General

1) A lift station tank shall be certified by an accredited testing agency as meeting or exceeding the structural and material requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated Septic Tanks and Sewage Holding Tanks."

Part 7 Site Evaluation

Section 7.1. Site Characteristics and Evaluation **Procedures**

7.1.1. Site Characteristics and Evaluation Procedures

Objectives and Design Standards

7.1.1.1. General

1) The objective of a site evaluation is to assess and quantify the capability of the site to infiltrate and disperse the effluent load into the soil in a manner that achieves the treatment objectives in the soil within the performance boundaries set for the on-site wastewater treatment system.1

Intent: Sentence (1) — The site's "capability" to treat wastewater is a combination of the site's ability to accept the wastewater load, meet separation distances to other features, and contain the depth of suitable soil needed to achieve treatment. For example, the soil may be able to accept the wastewater load without surfacing but a sufficient depth of unsaturated soil may or may not exist under the proposed hydraulic loading to provide final treatment of the wastewater. Together, all of the site characteristics will determine the suitability of a site for a particular treatment system design.

7.1.1.2. Site Evaluation

- 1) A site evaluation shall evaluate and note the
 - a) topography, landscape position of the system, vegetation, and surface drainage characteristics:
 - i) the slope gradient and aspect of each landscape element shall be determined for each potential treatment site investigated,
 - ii) the landscape positions shall be described for each reported site investigated,
 - iii) any vegetation type that favours wet or saturated soils shall be identified using its popular name, if known, and have its location identified in relation to the proposed system,
 - iv) any vegetation that will impact the selection of the location of the treatment system, or will require removal prior to construction of the treatment system, shall be noted, and
 - v) swales, depressions, and other drainage features that may impact system selection and design shall be located and described, and
 - **b)** surface waters, rock outcrops, and other natural features:
 - i) surface waters, including permanent or intermittent streams, lakes, wetlands, and other surface water within 100 m (330 ft.) of the proposed system, shall be located and described.
 - ii) rock outcrops within 50 m (165 ft.) of the soil-based treatment system shall be located and described, and
 - iii) any other natural features that could impact the application and/or design of a treatment system shall be located and described.
- 2) A sufficient number of suitably located soil profiles in the area of the soil-based treatment system shall be examined and described to adequately determine the variability of the soils on the proposed treatment site by
 - a) using excavated soil pits and intact cores of soil, 1 and

- b) completing an investigation to a depth that achieves the objectives of the site evaluation, and in no case shall the depth be less than 300 mm (12 in.) deeper than the *vertical separation* distance required below the proposed *soil-based treatment system*.
 - Note: Clause (2)(a) A typical method of obtaining an intact core of soil is through the use of a Shelby tube.
- 3) The characteristics of each soil profile investigated shall be described using Canadian System of Soil Classification nomenclature, and shall include the following in the soil profile description:¹
 - a) soil horizons: the distance from ground surface to the top and bottom of each soil horizon observed shall be measured and the distinctness and topography of the horizon boundaries described.
 - **b)** soil colour: for each soil horizon identified, the matrix colour and the quantity, size, contrast, and colour and any redoximorphic features present that indicate a seasonally saturated soil shall be described,
 - c) texture:
 - i) for each horizon identified, the *soil texture classification*, including any appropriate *texture* modifier, shall be reflected in the evaluation report, and
 - ii) a soil sample of the most *limiting condition* in the soil profile affecting the design shall be collected and analyzed at a laboratory using a recognized particle size analysis method to determine the texture of the sample,²
 - **d)** structure: for each soil horizon identified, the grade of soil structure observed and the size and class of grade, 0-3 shall be described,
 - **e)** *moist consistence*: for each *structure* observed in the profile, the *consistence* of the *soil* peds shall be described,
 - **f)** compaction: any zones of compaction in the *soil* profile shall be described to estimate its effect on water movement, root penetration, and aeration,
 - **g)** saturated zones: for each *soil* profile described, the depth to any water or the depth to the estimated high level of *seasonally saturated soil*, based on redoximorphic or *gleyed soil* characteristics, shall be measured,
 - h) bedrock and near-impermeable *soil* layers: depth to bedrock and near-impermeable *soil* layers observed shall be measured from the ground surface, and
 - i) restricting layers: for each soil profile described, any horizon or soil layer that is expected to significantly restrict downward water flow shall be identified and measured to determine its depth below ground surface.³

- 4) Investigation of surface elevations in the area of the *soil-based treatment system* shall include
 - a) identifying or establishing a permanent benchmark on the *property* that is shown on the plot plan of the *property* and provide GPS coordinates of the benchmark,
 - **b)** surface elevations and horizontal GPS coordinates at each *soil* profile investigation location and relative location to the benchmark, and
 - c) a topographic survey shall be performed at a scale sufficient to provide 300–600 mm (1–2 ft.) surface contours over the treatment site.
- 5) The degree of slope and slope aspect can be substituted for the topographic survey in Clause (4)(c) if the site topography is a simple planer slope.

¹ Note: Sentence (3) — Refer to the Field Book for Describing and Sampling Soils or the Soil Survey Manual available on the web at: http://sis.agr.gc.ca/cansis/intro.html or as included in the Alberta Private Sewage Soils Description Manual.

² Note: Subclause (3)(c)(ii) — Where a sand fraction modifier such as coarse, medium, fine, or very fine sand is part of the soil texture classification description the laboratory analysis must include the determination of the sand fraction size distribution.

³ Note: Clause (3)(i) — Such horizons may be discerned by evidence of episaturation above the horizon.

- 6) Property land uses and development within 50 m (165 ft.), or where a lagoon is used to within 100 m (330 ft.), of the *on-site wastewater treatment system* shall be identified and described, including¹
 - a) the land use of the property and adjacent properties, and
 - b) GPS coordinates of features such as buildings, water sources, water wells, on-site wastewater systems, roads, driveways, and other features that may impact treatment system location.
 - Note: Sentence (6) Property land uses and development within 50 m (165 ft.) of the treatment system applies to the main property itself as well as adjacent properties.
- 7) An available area for construction of the *on-site wastewater treatment system* shall be determined considering relevant horizontal separation distances from features on the property or adjacent properties that may be required by this Standard and include
 - a) private water sources, water wells, or municipal-licensed water supply wells,
 - **b)** buildings or other property improvements,
 - c) property boundaries,
 - d) surface waters and floodplains,
 - e) right-of-ways and easements, and
 - f) buried water supply piping, power lines, and other public or private utilities crossing the property.
- 7.1.1.3. Hydrogeological Site and Soil Evaluation for On-site Sewage Systems Exceeding 9 m³ Per Day Design Capacity.
 - 1) The objective of a site investigation for a development served by an on-site wastewater treatment system exceeding 9m3 per day design capacity is to evaluate the
 - a) capacity of the surficial and underlying lithology to receive and transport the added wastewater effluent.
 - b) near-surface groundwater conditions and the potential for groundwater mounding, and
 - c) assess the impact of the added effluent on groundwater quality and receiving surface water.
 - 2) Site investigations to achieve the objectives of Sentence (1) shall include a hydrogeological investigation and a soil and site investigation that is consistent with the NDWRCDP document "Guidance for Evaluation of Potential Groundwater Mounding Associated with Cluster and High Density Wastewater Soil Absorption Systems, January 2005," and which also meets the requirements of Articles 7.1.1.1 and 7.1.1.2 in addition to the following:
 - a) a minimum of three groundwater monitoring wells, to a maximum depth of 15 m (50 ft.) and in close proximity to the soil-based treatment area, shall be developed to determine the groundwater depth, aquifer thickness and flow direction,
 - b) investigate and report characteristics of the developed soil horizons and both the underlying unsaturated and saturated lithology to a minimum depth of 15 m (50 ft.) regarding hydraulic conductivity including, for each significant change in the characteristics of the lithology, the following:
 - i) particle-size distribution, and
 - ii) lab hydraulic conductivity testing of intact soil cores for vertical hydraulic conductivity,
 - c) estimate long term groundwater elevation through measurement and consideration of seasonal and long term fluctuations along with groundwater flow direction,
 - **d)** identify existing perched *water tables*, or the potential for perched *water table* formation through the depth of geologic layers investigated,

- **e)** measure horizontal hydraulic conductivity in the saturated zone or zones to be used in estimating *groundwater mounding* using a slug or bail test suitable for evaluating *groundwater mounding* and contaminant transport,
- f) identify potential groundwater discharge areas to nearby surface waters,
- g) determine baseline soil chemistry characteristics of EC, SAR, pH, and Salts,
- h) determine the water chemistry of the domestic water supply to be used for the development regarding SAR and EC in order to assess how the chemistry may affect the long-term hydraulic conductivity of the soil or impact vegetation, and
- i) establish the baseline groundwater quality, including routine groundwater parameters, TOC, N0₃, NH₄ TKN, total P and fecal coliform.
- 3) Notwithstanding the requirement of Clauses 2(a) and 2(b) to develop monitoring wells to a minimum of 15 m (50 ft.) or identify the *soil* lithology through to a depth of 15m (50 ft.), in no case shall a monitoring well or investigation of the geologic lithology
 - a) extend into a confined aquifer, or
 - **b)** be left to remain connected to a confined *aquifer*, should a confined *aquifer* be encountered during drilling or investigation.
- 4) The level and detail of the site assessment may be reduced from that set out in Sentence (2) where an initial assessment of the site characteristics and *soils* as set out in Chapter 2 of the document referenced in Sentence (2) indicates
 - a) there is a low potential for groundwater mounding,
 - **b)** the volume of *wastewater* treated and the consequence of *groundwater mounding* is low, and
 - c) the assessment of the site and considerations of potential risk are reported and justified to the satisfaction of the approving authority.
- 5) A hydrogeological assessment to evaluate *groundwater mounding* impact on the treatment and function of the *effluent infiltration* system resulting from the *infiltration* of the added *wastewater effluent* into the *soil* shall be completed and include
 - a) the evaluation of the potential for *groundwater mounding* negatively affecting the operation of the *on-site wastewater treatment system* based on the design *wastewater* flow volume of the *on-site wastewater treatment system*, and
 - b) the application of the findings of the site investigation, using an analytical or numerical model suitable for the complexity of site conditions to estimate the amount of *groundwater mounding* at the site, considering the criteria set out in the guidance document referenced in Sentence (2) or other recognized guidance documents,
- 6) Where a potential discharge of affected groundwater to a lake, river, stream, or creek located within 1 km of the on-site wastewater system is identified, transport and attenuation modelling shall be done to estimate the total phosphorus, nitrogen (all species), and chloride loading contributed to surface waters in the area.
- 7) The estimation of nutrient loading required by Sentence (6) shall follow the processes identified in the Water Environment Research Foundation (WERF) document "Modeling Onsite Wastewater Systems at the Watershed Scale, 2009" as it relates to the level of risk and sensitivity estimated for the receiving environment, considering the capacity of the *on-site wastewater treatment system*.

7.1.1.4. Site Evaluation Report

1) A site evaluation report documenting the results of the site evaluation shall include the following items or any other relevant design information, and shall form part of the system design documentation:

- a) description of the *property*:
 - i) address and legal. description of the property, and
 - ii) parcel identification number,
- b) date and time of day the evaluation was performed, as well as weather conditions such as cloud cover, temperature, and precipitation,
- c) plan of the *property*, to scale or dimensioned, including the following:
 - i) all property boundaries.
 - ii) buildings, roads, driveways, and other property improvements existing and proposed,
 - iii) existing easements.
 - iv) water wells or proposed well locations located on the property or adjacent properties within a 50 m (165 ft.) radius of the proposed system, along with the classification of whether a private or municipal well,
 - v) water wells or proposed water well locations within a 100 m (330 ft.) radius of a proposed on-site system, if a lagoon is to be used or a licensed municipal water well exists, along with the classification of whether a private or municipal well,
 - vi) topography of the proposed treatment site(s),
 - vii) surface waters, rock outcrops, and drainage features,
 - viii) soil pit or boring locations with surface elevations,
 - ix) location and elevation of a permanent benchmark, and
 - **x)** outline of available soil-based treatment area(s),
- d) descriptions of each soil profile investigated provided in an appropriate format, 1
- e) a statement regarding the treatment capability and dispersal capacity of the available site(s).
- f) where the soil profile includes features that will require the lateral movement of water through the soil away from the dispersal system, identify constraints on the system design and allowable effluent hydraulic loading rates as they relate to linear loading rates.
- **g)** a summary of the significant *limiting conditions* of the *soil* profile and site,
- h) a justification of the locations and number of soil profiles investigated, and
- i) a description of the *development* being served, including
 - i) characteristics affecting the determination of peak and average wastewater flows to be used in the design,
 - ii) the peak daily wastewater flow volume to be used for the system design, and
 - iii) anticipated influent wastewater strength.
- ¹ Note: Clause (1)(d) Forms for reporting the soil profile descriptions are available in the Alberta Private Sewage Systems Standard of Practice Handbook; other equivalent forms may be used.

7.1.2. Site Characteristics and Evaluation Procedures

 Prescriptive Requirements and Installation Standards

Number of Soil Profiles Investigated 7.1.2.1.

- 1) Soil profiles shall be investigated at a minimum of two locations within or immediately adjacent to the proposed location of the soil-based treatment component in order to assess the hydraulic and treatment capacity of the soil, at least one of which is an excavated soil test pit, and the other location or locations may be a solid-core soil sample, except as allowed by Article 8.7.2.4 for open discharge systems.
- 2) As soil variability increases, or the area required for the system increases,
 - a) additional soil profiles shall be investigated, and

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- b) the number of locations needed to investigate the soil profile at the site shall be justified in the site evaluation report.
- 3) The GPS coordinates of the soil profile locations investigated shall be taken and included in the site evaluation report.

Minimum Depth of Soil Investigation 7.1.2.2.

- 1) The soil profiles shall be investigated to at least 300 mm (1 ft.) below the minimum vertical separation depth needed for the anticipated type of system to show that there is sufficient suitable soil depth below the soil infiltration surface to
 - a) provide the required vertical separation, and
 - b) determine the effluent hydraulic linear loading capacity of the soil.

7.1.2.3. Percolation Test

1) The results of a percolation test shall only be used in support of a design that is based on a soil profile investigation and site evaluation required by this standard.

7.1.2.4. Site Evaluation Report

1) A report as required by Article 7.1.1.4. shall be developed and included in the system design information.

Part 8 General Soil-based Treatment

Section 8.1. Soil-based Treatment

8.1.1. Soil-based Treatment — Objectives and Design Standards

8.1.1.1. General

1) The design of any soil-based effluent treatment system shall meet the requirements of this Section.

8.1.1.2. Infiltration Area

- 1) In determining the soil infiltration surface area required for a soil-based effluent treatment system, the following shall be considered in the design:
 - a) hydraulic loading capabilities of the soil profile,
 - **b)** *linear loading* rate limitations of the soil profile.
 - c) organic loading on the soil infiltration surface resulting from the effluent strength,
 - d) treatment capability of the soil profile,
 - e) depth of suitable soil required to achieve treatment objectives, and
 - f) achievement of treatment objectives at a depth that does not exceed 2.4 m (8 ft.), or a lesser depth as required by the site conditions and intended treatment boundary limits.

8.1.1.3. Effluent Loading Rates On Soil and Restrictions on Coarse Sand

1) The effluent hydraulic loading rate on the soil infiltration surface shall be based on the soil texture and structure as set out in Table 8.1.1.10. when the required vertical separation distance below the infiltrative surface is available.¹

Intent: Sentence (1) — The soil texture classification and soil structure are key indicators of the hydraulic conductivity of the soil or the rate at which the soil will accept and transmit water. The soil texture classification of samples taken from the most limiting design layer in the soil profile shall be determined by lab tests. Other field criteria must also be given consideration when sizing a system, such as type of clay, seasonal high water table and water quality; for example, the water's sodium adsorption ratio.

2) Effluent shall not be applied where the in-situ soil has the soil texture classification of coarse sand unless it can be demonstrated that the soil profile includes horizons of other suitable textures that will result in effective treatment and protection of groundwater.

8.1.1.4. Vertical Separation

- 1) Soil-based treatment systems shall maintain a vertical separation between the soil infiltration surface and a restricting layer of not less than
 - a) 1500 mm (5 ft.) when receiving primary treated effluent Level 1,
 - **b)** 900 mm (3 ft.) when receiving secondary treated effluent (Level 2 or better),
 - c) 900 mm (3 ft.) below a treatment mound as measured from the bottom of the required 300 mm (1 ft.) depth of sand layer intended to provide secondary treatment, or
 - d) the depth of soil required to achieve a 7-day effluent travel time to the design boundary depth, provided the treatment boundary limit depth does not exceed 2.4 m (8 ft.), as set out in Article 8.1.1.5.

2) If there is a very shallow restricting layer, fill material may be used if allowed and as specified in the system-type section of this standard to provide the required *vertical separation*, but in no case shall there be less than 300 mm (1 ft.) of in situ soil that is assigned an effluent hydraulic loading rate within this standard below the fill material and above the restricting layer.

8.1.1.5. Loading Rates and Vertical Separation Exceptions

- 1) Effluent hydraulic loading rates and/or vertical separation distances may vary from those set out in Table 8.1.1.10. and Article 8.1.1.4., respectively, and subject to Sentence (2), if
 - a) the effluent hydraulic loading rate selected will result in a minimum 7-day effluent travel time to the vertical separation performance treatment boundary limit based on
 - i) the mobile soil water content at field capacity.
 - ii) a maximum treatment boundary limit depth that does not exceed 2.4 m (8 ft.), and
 - iii) peak design flow volumes as determined by applying the requirements of Section 2.2.,
 - **b)** a minimum *vertical separation* of 900 mm (3 ft.) to a restrictive layer maintained when the system is located within 2 km (1.25 miles) of a
 - i) lake.
 - ii) river,
 - iii) stream, or
 - iv) creek, and
 - c) the effluent is delivered to the soil infiltration surface using a pressure distribution lateral pipe system in all cases where the vertical separation distance is less than required in Clause 8.1.1.4.(1)(a).
- 2) Vertical separation distances may be reduced to a minimum of 600 mm (2 ft.) if the
 - a) effluent being applied will meet the qualities set out for secondary treated effluent Level 3-DII.
 - b) the system is not located within 2 km (1.25 miles) of a lake, river, stream, or creek,
 - c) the system is not located over GWUDI which can be classified as a domestic use aguifer, and
 - **d)** the objective of a 7-day *effluent* travel time is achieved.
- 3) Where the soil profile includes coarse fragments, the effluent hydraulic loading rate shall be reduced
 - a) to ensure a 7-day travel time is achieved, and
 - **b)** as required by Article 8.1.2.4.

8.1.1.6. Effluent Soil Infiltration Surface Area Design

- 1) The design of the soil-based treatment system shall be based on peak daily flow volumes and the effluent hydraulic loading rates set out in this Standard for primary and secondary treated effluent when the effluent is
 - a) primary treated effluent Level 1 that at least 80% of the time has a strength of
 - i) 150 mg/L cBOD₅ or less,
 - ii) 100 mg/L TSS or less, and
 - iii) 15 mg/L oil and grease or less, or

- secondary treated effluent (Level 2, 3, or 4) that at least 80% of the time has a strength
 - i) 25 mg/L cBOD₅ or less,
 - ii) 30 mg/L TSS or less, and
 - iii) 10 mg/L oil and grease or less.
- 2) When the effluent strength exceeds the values referred to in Sentence (1), the effluent hydraulic loading rate shall be reduced to achieve an organic loading rate on the soil infiltration surface that does not exceed the organic loading rate that would result from the anticipated *effluent* strength set out in Sentence (1).

8.1.1.7. System Geometry and Linear Loading Rate Design

- 1) The design and geometry of the soil-based treatment area shall result in an effluent hydraulic linear loading rate that does not exceed the soil profile's capability to allow the horizontal movement of the effluent away from the treatment system when vertical flow will be restricted and shall consider
 - a) the values set out in Table 8.1.1.10. that relate horizontal movement of effluent through the soil to the characteristics of a soil profile and the slope of the landscape, or
 - b) a comprehensive and documented assessment and calculation of the soil's capacity to transmit the *effluent* horizontally, as set out in Article 8.1.1.9.

8.1.1.8. Pressure Distribution Required

- 1) Secondary treated effluent shall be applied to any soil-based treatment system using a pressure distribution lateral pipe system that meets the requirements of Section 2.6.
- 2) A pressure distribution lateral pipe system that meets the requirements of Section 2.6. and having orifice spacing of not more than 900 mm (3 ft.) shall be used to apply effluent to soils having a texture of medium sandy loam or coarse sandy loam or any coarser-textured soil, as set out in Sentence 8.2.2.2.(1)

8.1.1.9. Groundwater Mounding Considerations Required

- 1) In the design of a soil-based effluent treatment system, the potential for groundwater mounding below the soil-based effluent treatment system shall be assessed for all systems where the¹
 - a) available vertical separation distance to a restrictive soil layer does not exceed the required vertical separation depth by not less than 300 mm (1 ft.) except where the prescriptive requirements of Article 8.1.2.3. are applied,
 - b) daily peak flow exceeds 5.7 m³ (1,250 lmp. gal.) per day, in which case the site investigation shall include an investigation of the soil capability and capacity to disperse water from the site, and the design documentation shall include a calculation of the potential groundwater mounding height to determine whether the height will negatively impact the system's treatment effectiveness, or
 - c) daily peak flow exceeds 9 m³ per day, in which case the requirements of Article 7.1.1.3. shall be applied with regard to site investigation and estimation of groundwater mounding and nutrient loading.

¹ Note: Sentence (1) — Guidance on the intensity of the investigation based on related risk along with recognized methods are available from; Poeter E., J. McCray, G. Thyne, and R. Siegrist. 2005. Guidance for Evaluation of Potential Groundwater Mounding Associated with Cluster and High-Density Wastewater Soil Absorption Systems, January 2005.. Prepared for the National Decentralized Water Resources Capacity Development Project, Project No. WU-HT-02-45, Washington University, St. Louis, MO, by the International Groundwater Modeling Center, Colorado School of Mines, Golden, CO. It can be obtained online at www.ndwrcdp.org. or at National Small Flows Clearinghouse; P.O. Box 6064; Morgantown, WV 26506-6065; Tel: (800) 624-8301; WWCDRE46. Direct link to document: http://www.ndwrcdp.org/research_project_WU-HT-02-45.asp

8.1.1.10. Effluent Loading Rates on Soil Infiltration Surface

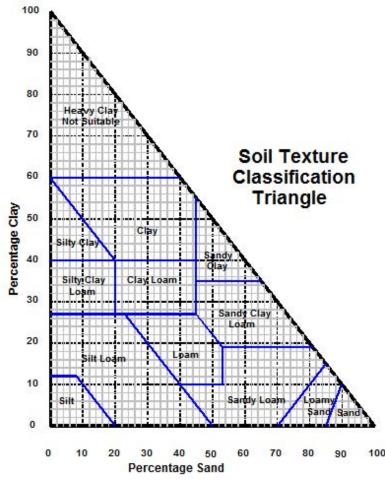
- 1) The effluent hydraulic loading rates and effluent hydraulic linear loading rates suitable for the soil profile identified at the site, as characterized by the texture and structure of the soil, shall be determined by using Table 8.1.1.10.
- 2) The top of a columnar structured soil horizon shall be considered a restrictive layer.
- 3) Where the *consistence* of the peds in a horizon are very firm or harder (wet *consistence*) or hard or harder (dry consistence), the horizon is not suitable for an effluent hydraulic loading rate and shall be considered a restrictive layer.
- 4) Prismatic structured soil shall be considered a restrictive layer, even if it is identified in Table 8.1.1.10 with an effluent hydraulic loading rate, if the
 - a) soil consistence is very firm or harder (wet consistence) or hard or harder (dry consistence).
 - b) measured soil electrical conductivity is greater than 4,
 - c) soil sodium absorption ratio (SAR) is greater than 8,
 - d) soil coefficient of linear extensibility (COLE) is greater than 3%, or
 - e) soil dispersion test shows more than slight dispersion of the soil.

Table 8.1.1.10. (Metric) Effluent Soil Loading Rates and Linear Loading Rates (Litres)											
					Hydraulic Linear Loading Rate, L/day/m						
	Efflu	Effluent Slope of land									
Soil Characteristics			loading rate: L/day/sq. metre		0 - 4%		>4 - 9%		>9%		
	Structure		Effluent Quality cBOD ₅		Infiltration distance ¹ , m		Infiltration distance ¹ , m		Infiltration distance ¹ , m		
Texture	Shape	Grade	30-150 mg/L	<30 mg/L	0.3 < 0.6	0.6 <1.2	0.3 < 0.6	0.6 <1.2	0.3 <0.6	0.6 <1.2	
COS ² , MS, LCOS, LMS Requires pressure distribution		0SG	14.7	14.7	74.6	89.5	89.5	104.4	104.4	119.3	
FS,VFS,LFS,LVFS Requires pressure distribution		0SG	19.6	24.5	67.1	82.0	74.6	89.5	89.5	104.4	
		OM	9.8	29.4	52.2	59.7	61.2	68.6	89.5	104.4	
COSL, MSL	PL	1	9.8	24.5	52.2	59.7	61.2	68.6	74.6	89.5	
Requires pressure distribution		2,3	0.0	9.8	37.3	44.7	40.3	47.7	43.3	50.7	
	PR ³ /BK	1	19.6	29.4	67.1	82.0	74.6	89.5	89.5	104.4	
	/GR	2,3	29.4	29.4	67.1	82.0	74.6	89.5	89.5	104.4	
		OM	8.8	17.6	34.3	38.8	40.3	44.7	47.7	55.2	
	PL	1	8.8	17.6	34.3	38.8	40.3	44.7	47.7	55.2	
FSL,VFSL	PL	2,3	0.0	7.3	37.3	44.7	40.3	47.7	43.3	50.7	
	PR ³ /BK	1	8.8	22.0	52.2	59.7	56.7	64.1	61.2	68.6	
	/GR	2,3	15.7	30.8	56.7	64.1	61.2	68.6	65.6	73.1	
		OM	8.8	22.0	34.3	38.8	40.3	44.7	47.7	55.2	
	PL	1	14.7	22.0	52.2	59.7	56.7	64.1	61.2	68.6	
L	ΓL	2,3	0.0	7.3	37.3	44.7	40.3	47.7	43.3	50.7	
	PR ³ /BK	1	14.7	22.0	52.2	59.7	56.7	64.1	61.2	68.6	
	/GR	2,3	22.0	30.8	56.7	64.1	61.2	68.6	65.6	73.1	
		OM	0.0	8.8	37.3	44.7	40.3	47.7	43.3	50.7	
	PL	1	0.0	7.3	37.3	44.7	40.3	47.7	43.3	50.7	
SIL		2,3	0.0	0.0							
	PR ³ /BK	1	14.7	22.0	40.3	44.7	44.7	49.2	52.2	59.7	
	/GR	2,3	22.0	30.8	47.7	55.2	52.2	59.7	56.7	64.1	
SCL, CL, SICL, SI		OM	0.0	0.0							
	PL	1	0.0	7.3	25.4	32.8	28.3	35.8	31.3	38.8	
		2,3	0.0	0.0							
	PR ³ /BK	1	8.8	13.2	37.3	44.7	40.3	47.7	43.3	50.7	
	/GR	2,3	13.2	22.0	43.3	50.7	47.7	55.2	52.2	59.7	
SC, C, SIC		OM	0.0	0.0							
	PL	1,2,3,	0.0	0.0							
	PR ³ /BK	1	0.0	0.0							
	/GR	2,3	6.9	9.8	37.3	44.7	40.3	47.7	43.3	50.7	
НС		OM	0.0	0.0							
	PL	1,2,3,	0.0	0.0							
	PR ³ /BK	1	0.0	0.0							
	/GR	2,3	4.4	7.8	31.3	38.8	34.3	41.8	37.3	44.7	

Table 8.1.1.10 Soil Texture and Structure Abbreviations										
COS – Coarse Sand		LVFS – Loamy Ve	ry Fine Sand	SI – Silt						
MS –Medium Sand		COSL – Coarse Sa	andy Loam	SCL – Sandy Clay Loam						
LCOS - Loamy Coarse Sand		MSL – Medium Sa	ndy Loam	CL – Clay Loam						
LMS – Loamy Medium Sand		FSL – Fine Sandy	Loam	SICL – Silty Clay Loam						
FS – Fine Sand		VFSL – Very Fine	Sandy Loam	SC – Sandy Clay						
LFS – Loamy Fine Sand		L – Loam		SIC – Silty Clay						
VFS – Very Fine Sand		SIL – Silt Loam		C – Clay	HC – Heavy Clay					
PL – Platy	PR – Prismation	BK – Blocky	GR -Granular	M - Massive	SG - Single Grain					
0 – Structureless	1 – Weak	2 – Moderate	3– Strong							

¹ Note: Infiltration distance is the depth of suitable soil below the in situ soil infiltration surface the effluent is applied to and the restrictive layer.

Figure 8.1.1.10. Soil Texture Classification Triangle



Note: Plotting the percentage of sand and clay provides the remaining percentage of silt.

Table 8.1.1.10 Infiltration rates in L/d/m² for wastewater effluent strength of <30 mg/L BOD₅ or wastewater effluent strength of <30 mg/L BOD₅ and hydraulic linear loading rates in L/d/m of system length based on the soil characteristics of texture and structure and the site conditions of slope and infiltration depth to restrictive soil layers. Values assume daily wastewater volume estimates used in the design are based on the values set out in Subsection 2.2.2. or include the same safety factor. If horizon consistence is stronger than firm or any cemented class or the clay mineralogy is smectitic, the horizon is limiting regardless of other soil characteristics (adapted from 2000, E. Jerry Tyler).

² Note: The application of effluent to Coarse Sand textured soil is not allowed except where the requirements of Sentence 8.1.1.3.(2) are met.

³ See restriction on prismatic soils set out in Sentence 8.1.1.10.(4)

8.1.1.11. Supplementary Air Supply to Soil-based Effluent **Treatment Systems**

- 1) A positive pressure air supply for the purpose of promoting aerobic conditions may be provided to treatment field trenches, treatment mounds, or sand filters, provided the
 - a) effluent hydraulic load on the system does not exceed the loading rates allowed by this standard on the soil profile at the site and for the effluent quality applied,
 - b) requirements of 7-day travel time through the *vadose zone* is not compromised.
 - c) effluent is distributed by pressure distribution lateral pipes, and
 - d) system is designed in such a way that it will not cause effluent to be pushed back into the effluent chamber when air is introduced.

¹ Note: If the supply of air for the sewage system is taken from inside a building, the designer must ensure that the removal of air from the building will not create an unsafe depressurization of the building that may affect fuel burning appliances or cause problems with the building ventilation system.

8.1.2. Soil-based Treatment — Prescriptive Requirements and Installation Standards

8.1.2.1. Evaluation

- 1) For the design of in situ soil-based treatment systems, the soil at the location of the system and required surrounding area shall be evaluated in accordance with Part 7 to identify the soil characteristics and conditions needed to determine the
 - a) appropriate soil infiltration surface effluent hydraulic loading rate, and
 - **b)** depth to seasonally saturated soil conditions or restrictive layers that
 - i) limit available vertical separation, and
 - ii) are needed to select acceptable linear loading rates for the system design.

8.1.2.2. Infiltration Loading Rate

- 1) The soil infiltration surface loading rate shall not exceed the amount set out in Table 8.1.1.10. based on the soil characteristics identified by the site evaluation.
- 2) Except where determined in accordance with the requirements of Article 8.1.1.5., the effluent hydraulic loading rate applied to a soil infiltration surface shall not exceed
 - a) 14.7 litres per sq. metre (0.3 lmp. gal. per sq. ft.) per day on coarse sand, medium sand, loamy coarse sand, or loamy medium sand textured soils,
 - **b)** 29.4 litres per sq. metre (0.6 lmp. gal. per sq. ft.) per day on fine sand, very fine sand, loamy fine sand, loamy very fine sand, coarse sandy loam, or medium sandy loam textured soils, and
 - c) 40.7 litres per sq. metre (0.83 lmp. gal. per sq. foot) per day on fine sandy loam and very fine sandy loam to clay-textured soils.
- 3) Effluent shall not be applied to soils having a texture of coarse sand except where conditions allow such a design in compliance with Sentence 8.1.1.3.(2).

8.1.2.3. Linear Loading Rates Not Exceeded

1) Except as provided for in Article 8.1.1.7., the geometry of the soil infiltration surface shall be designed to ensure the *linear loading* rates set out in Table 8.1.1.10. are not exceeded.

8.1.2.4. Infiltration Loading Rate Reduced, Coarse Fragments

- 1) The effluent hydraulic loading rate on soils that have a soil texture classification of coarse sand, medium sand, loamy course sand, or loamy medium sand, that also have a coarsefragment content by volume that exceeds1
 - a) 35% but is less than or equal to 60%, shall be reduced to 9.8 litres per sq. metre (0.2) Imp. gal. per sq. ft.) per day for both primary and secondary treated effluent,
 - b) 60% but is less than or equal to 75%, shall be reduced to 7.4 litres per sq. metre (0.15 Imp. gal. per sq. ft.) per day for both primary and secondary treated effluent, or
 - **c)** 75%, shall be reduced to 0.0 litres per sq. metre (0.0 lmp. gal. per sq. ft.) per day.

 Note: Increasing volumes of coarse fragments in the soil limit the amount of soil particle surface area in the soil that is needed to achieve treatment. The water holding capacity of these soils is also limited so it becomes difficult to achieve the required 7 day travel time to the treatment boundary. As coarse fragment content increases, the effluent loading rate must be reduced to achieve the treatment objectives of the Standard.

Section 8.2. Treatment Fields

8.2.1. Treatment Fields — Objectives and Design Standards

8.2.1.1. General

- 1) A treatment field shall meet the following objectives:
 - a) provide temporary storage of the effluent until it is able to infiltrate into the soil,
 - **b)** break down the *organic loading* contained in the *effluent*,
 - c) provide an area of soil over which the effluent is spread to reduce the hydraulic and organic loading on each part of the soil infiltration surface,
 - d) spread the effluent over a suitably sized area to enable sufficient oxygen to be transferred through the soil in order to achieve treatment objectives and long-term utilization, and
 - e) introduce the effluent into the soil and be constructed in a manner that minimizes the risk of effluent breakout through the material covering the soil infiltration surface area that provides a barrier against direct contact with the effluent.
- 2) The design of a treatment field shall meet all requirements set out in Section 8.1.

8.2.1.2. Effluent Treatment Quality in Soil

- 1) A treatment field shall treat the applied effluent as it migrates through the soil, as measured at the *vertical separation* boundary required for the design and *effluent* quality being applied, to the following quality:
 - a) fecal coliform < 10 cfu/100 mL above background levels, or
 - **b)** fecal coliform < 2 MPN/gram of dry soil above background levels.

8.2.1.3. **Effluent Loading Rates**

- 1) The effluent hydraulic loading rates for sub-surface treatment fields are set out in Article 8.1.1.10. and are based on effluent qualities that are equal to or better than primary treated effluent Level 1 or secondary treated effluent.
- 2) If the strength of the *effluent*
 - a) is higher than secondary treated effluent, the effluent hydraulic loading rates shall be based on primary treated effluent Level 1, or
 - b) is higher than primary treated effluent Level 1, the effluent hydraulic loading rate shall be reduced as required to result in a mass organic loading rate on the soil infiltration surface that does not exceed the calculated organic loading resulting from the application of effluent that meets the primary treatment standard.

8.2.1.4. **Gravity Distribution**

- 1) A treatment field utilizing gravity distribution over the soil infiltration surface shall receive a dose volume that
 - a) encourages spreading over the entire soil infiltration surface, and
 - b) is within the range of 3.4 and 12 L per square metre (0.07 to 0.25 lmp. gal. per sq. ft.) of weeping lateral trench per dose.

8.2.1.5. Depth of Weeping Lateral Trench

1) The depth of the *weeping lateral trench* bottom shall be as shallow as possible, while considering the need for frost protection, in order to maximize the transfer of oxygen through the *soil* at the site to the *soil infiltration surface* and *vadose zone* below the trench bottom.

8.2.1.6. Trench Width and Separation

- The width of a trench used in a system design shall consider the organic loading on the soil infiltration surface and the ability of the soil to transmit the required oxygen demand to the trench bottom and vadose zone.
- 2) Adequate separation between trenches shall be provided to enable sufficient re-aeration of the subsurface *soil* receiving *effluent*.

8.2.1.7. Effluent Loading Rate on Trench Bottom

1) The design *effluent hydraulic loading rate* on the trench bottom area of a *treatment field* shall be based on Table 8.1.1.10. and comply with Article 8.1.2.2.

8.2.1.8. Pressure Distribution Reduction in Trench Bottom Area

1) The effluent hydraulic loading rate may be increased by a factor of 1.2 on a conventional treatment field or gravel substitute treatment field, supplied with primary treated effluent Level 1 when pressure distribution lateral piping is used in accordance with Section 2.6., but in no case shall the resulting effluent hydraulic loading rate exceed the effluent hydraulic loading rate for secondary treated effluent on that same soil profile or limited elsewhere in this standard.¹

¹ Note: Sentence (1) — Notwithstanding the provisions of this Article, limits on loading rates also need to consider effluent hydraulic loading rate limits established for coarse-textured soils and/or coarse-fragment content as set out in other articles to ensure a minimum 7-day travel time to the treatment boundary is achieved.

8.2.1.9. Serial Distribution Prohibited

1) A treatment field shall not use serial distribution as a method to distribute effluent to weeping lateral trenches.¹

¹ Intent: Sentence (1) — The effluent should be distributed to each weeping lateral trench evenly. The effluent should not be allowed to flow through one weeping lateral trench to reach another at a lower elevation.

8.2.1.10. Equal Distribution to Gravity Weeping Laterals

1) When gravity distribution is used to supply *effluent* to the *treatment-field weeping lateral trenches*, the *effluent* distribution system shall be designed to provide approximately equal *effluent* distribution to each *weeping lateral trench*.

8.2.1.11. Monitoring Effluent Ponding Depth

1) To facilitate monitoring of the *soil-based treatment system*, each *weeping lateral trench* shall be equipped with a method of evaluating the ponding depth within the length of the *weeping lateral trenches*.

8.2.1.12. Treatment Field Layout

1) The geometry of the *treatment field* layout shall consider the *linear loading* rates set out in this Standard, or shall be determined by calculation of *groundwater mounding* impacts to

ensure that the cumulative loading from numerous trenches does not exceed the capacity of the soil to transmit the effluent away from the weeping lateral trenches.

8.2.1.13. Fine Textured Soil Restriction

1) A treatment field shall not be installed on soils that have an effluent hydraulic loading rate of less than 9.80 L per square metre (0.2 Imp. gal. per sq. ft.) per day.

8.2.2. Treatment Fields — Prescriptive Requirements and Installation Standards

8.2.2.1. Separation Distances

- 1) A treatment field, measured from any part of a weeping lateral trench, shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - **b)** 100 m (330 ft.) of a licensed municipal water well,
 - c) 15 m (50 ft.) of a water course, except as provided in Article 2.1.2.4,
 - **d)** 1.5 m (5 ft.) of a *property* line,
 - e) 10 m (33 ft.) of a basement, cellar, or crawl space, 1
 - f) 1 m (3.25 ft.) of a *building* that does not have a permanent foundation,
 - g) 5 m (17 ft.) of a building that has a permanent foundation but does not have a basement, cellar, or crawl space, and
 - h) 5 m (17 ft.) from a septic tank or packaged sewage treatment plant.

 Note: Clause (1)(d) The 10 m (33 ft.) requirement to a basement, cellar, or crawl space is intended to protect excavations below grade from accumulating migrating effluent. A crawl space that is not below grade, or where the level of the ground surface at the soilbased treatment area is below the level of the crawl space, the separation required is 5 m (17 ft.) clearance, as it can be treated as a building without a basement.

8.2.2.2. Coarse-Textured Soil - Restrictions On Effluent **Application**

- 1) Except as allowed by Sentence (2), a pressure effluent distribution lateral pipe system having orifices spaced at not more than 900 mm (3 ft.), and meeting the requirements of Section 2.6., shall be used to distribute the effluent over the soil infiltration surface of a treatment field when the texture of the soil at and below the effluent infiltrative surface has a soil texture of
 - a) coarse sand,
 - **b)** medium sand,
 - c) loamy coarse sand,
 - **d)** loamy medium sand,
 - **e)** fine sand,
 - f) very fine sand,
 - g) loamy fine sand,
 - h) loamy very fine sand,
 - i) coarse sandy loam, or
 - j) medium sandy loam.
- 2) Notwithstanding Sentence (1), gravity distribution of the effluent is allowed if, within the allowed depth to the *treatment boundary limit*, there is an in situ soil horizon
 - a) having a soil texture of very fine or fine sandy loam or finer textured soil with a minimum thickness of not less than 900 mm (3 ft.), and

b) the finer-textured soil horizon described in Clause (a) extends over the entire area of the treatment field.

¹ Note: Sentence 2) — The trenches cannot be lined with imported material to take the place of the in situ soil.

8.2.2.3. Weeping Lateral Trench Construction

- 1) A weeping lateral trench shall
 - a) be not more than 900 mm (3 ft.) deep,¹
 - **b)** be between 300 mm (12 in.) and 900 mm (3 ft.) wide,
 - c) have a *nominally level* bottom,
 - d) include a void space created by
 - i) a chamber,
 - ii) weeping lateral trench media meeting the requirements of Sentence 8.2.3.1.(1) placed at the bottom of the trench filling the entire width of the trench to a depth of 300 mm (1 ft.), or
 - iii) sand meeting the requirements of Sentence 8.2.3.1.(2) placed in the bottom 150 mm (6 in.) of the trench, covered by 150 mm (6 in.) of weeping lateral trench media,
 - e) provide a minimum of 30% void volume under compression conditions equal to the weight of 1 m (3.25 ft.) of earth cover, and
 - f) be covered with a material that will prevent migration of soil particles into the void space of the distribution media and allow the movement of air into the system that is either
 - i) a geotechnical filter fabric that allows the movement of air and water through it,
 - ii) 75 mm (3 in.) of a non-oil-seed straw, or other equivalent fibrous material, or
 - iii) a material having equivalent properties.

2) A weeping lateral trench shall be located so as to provide a minimum of 900 mm (3 ft.) of earth between the side wall of the trench and the sidewall of an adjacent weeping lateral trench.

8.2.2.4. Gravity Distribution Weeping Lateral Pipe

- 1) A gravity distribution weeping lateral pipe shall be
 - a) laid nominally level at a maximum depth of 600 mm (2 ft.) below the finished ground surface, as measured from the top of the pipe, and
 - **b)** installed with the top of the pipe at the top of the *drain media* used in the trench.

8.2.2.5. Weeping Lateral Connected to Gravity Distribution Header

1) Where weeping lateral pipes connect to a gravity distribution header or field header, all piping in the treatment field shall be installed at the same elevation.

8.2.2.6. Gravity Weeping Laterals at Different Elevations

- 1) Where weeping lateral pipes in the field are at different elevations either
 - a) pressure distribution supply to each weeping lateral trench shall be used, or
 - **b)** a distribution box shall be used to distribute the *effluent* evenly to each *weeping lateral* pipe.

Note: Clause (1)(a) — While no minimum depth is specified in this Standard, a cover of 300 mm (12 in.) of soil over the top of the gravel and effluent pipe has typically been maintained, although there are many examples of weeping lateral trenches being placed at shallower depth throughout Alberta without encountering freezing problems. The burial depth required for adequate frost protection depends on a number of factors which include typical snow cover, type of soil at the site, and length of time the system may go without receiving effluent that adds heat to the soil.

8.2.2.7. Distribution Box

- When used in a system, a distribution box shall¹
 - a) have an internal dimension not exceeding 300 mm (12 in.).
 - **b)** provide relatively equal distribution to all outlets, and
 - c) be readily accessible for inspection and service and adequately protected from frost. Intent: Sentence (1) — To ensure relatively equal distribution to all weeping laterals. The maximum internal dimension of the distribution box minimizes the impact that either soil movement, or frost heaving that tips the box out of level, will have on the even distribution of the effluent. Accessibility is required to confirm distribution during service.

8.2.2.8. Drop Boxes

- 1) Notwithstanding Sentence 8.2.1.10.(1), where drop boxes are used to distribute effluent to weeping lateral trenches the
 - a) treatment field may be installed on sloping ground.
 - b) invert of the outlet piping to the next drop box shall be
 - i) above the top of the weeping lateral pipe outlet, and
 - ii) a minimum of 25 mm (1 in.) below the invert of the inlet piping to the drop box, and
 - c) drop box serving each weeping lateral pipe shall have provisions for preventing effluent from entering the weeping lateral pipe to facilitate resting of the lateral.

1 Intent: Sentence (1) — A drop box system is a form of an anaerobic effluent treatment system. It is intended to be used primarily in very porous soil structures where the creation of a restricting layer of biomat is desired. This biomat reduces the infiltration rate of effluent into the soil. This design is used to reduce infiltration rates where desired. A drop box cannot be used as a "distribution box" for distributing effluent evenly to weeping lateral trenches.

2) Where drop boxes are used, the operation manual shall specifically identify the requirement to periodically redirect effluent flow.

8.2.2.9. Location Restriction

- 1) A treatment field shall not be located under
 - a) a roadway or driveway,
 - **b)** a paved area,
 - c) a vehicle parking lot,
 - d) any structure, or
 - e) a vegetable garden.

8.2.2.10. Monitoring Ports

1) A minimum 100 mm (4 in.) monitoring port, fitted with a mechanically fastened top, extending from the surface of the ground to the depth of the soil infiltration surface, shall be provided within 4.5 m (15 ft.) from each end of a weeping lateral trench.

8.2.2.11. Raised Treatment Field Contact with In Situ Soil

- 1) Where the bottom of the trench forming the soil infiltration surface is within the surface vegetation thatch zone or above the elevation of the in situ soil,
 - a) the soil interface at the in situ surface directly below the trench bottom shall be broken up, or the thatch removed, to develop strong contact between the fill material of the trench and the in situ soil.
 - b) the fill material that is directly under the trench bottom, from the in situ soil surface to the finished elevation of the soil infiltration surface area, shall meet the requirements of the sand specified in Article 8.4.3.1., and
 - c) effluent shall be distributed through the laterals using a pressure distribution lateral pipe system meeting the requirements of Section 2.6.

2) A raised treatment field shall not be used unless there is a minimum of 600 mm (2 ft.) of in situ soil that is assigned an effluent hydraulic loading rate in Table 8.1.1.10. below the raised treatment field.

Raised Treatment Field Fill Material 8.2.2.12.

- 1) Coarse sand, medium sand, fine sand, loamy medium sand or loamy coarse sand fill material shall be used for the backfill material covering the area of the raised treatment field, and it shall be¹
 - a) placed over the gravel layer of the trenches or over the chambers to a depth of 300 mm (1 ft.) to 600 mm (2 ft.), and
 - b) the finished grading of the fill material shall ensure positive drainage of precipitation off the area of the raised treatment field.
 - 1 Intent: Sentence (1) To provide an adequate slope (1% or more) on the top of the field to prevent excessive infiltration and ponding of precipitation and snow melt on the area of the field.
- 2) In addition to the requirements of Sentence (1), 75 mm (3 in.) of soil having a texture not finer than sandy loam and not coarser than loamy fine sand shall be placed over the fill material to cover the entire area of the raised treatment field in order to support a grass vegetative cover.

Grass Cover on Raised Treatment Field 8.2.2.13.

1) A grass cover shall be established over the entire area of the raised treatment field.1 Intent: Sentence (1) — A contractor meets the requirement of this Sentence by seeding the area to grass, leaving the responsibility to the owner to water and maintain the grass cover. The grass cover is needed to prevent erosion of the area and limit infiltration under heavy precipitation events.

Side Slopes of Raised Treatment Field Area 8.2.2.14.

1) The side slopes on the area covering the raised treatment field shall not be steeper than 1:3 (one vertical to three horizontal).

8.2.3. Treatment Fields — Requirements for Materials

8.2.3.1. Weeping Lateral Trench Media

- 1) Except as provided in Sentence (3), the drain media used in a weeping lateral trench shall
 - a) consist of clean washed *gravel*, clean crushed rock, or other equivalent media that will maintain structural integrity and not be degraded by the environment created in the treatment field trench.
 - b) have a particle-size distribution by weight of
 - i) 100 percent passing the 50 mm (2 in.) sieve,
 - ii) 0 to 25 percent passing the 12.5 mm (½ in.) sieve.
 - iii) 0 to 10 percent passing the 9.51 mm (3/8 in.), sieve,
 - iv) 0 to 2 percent passing the 1.18 mm (3/64 in.), No. 16 sieve, and
 - v) 0 to 1 percent passing the 0.15 mm (0.0059 in.) No, 100 sieve, and,
 - c) be able to withstand vertical and horizontal loads from backfill equal to a minimum of 1 m (3.25 ft.) of earth cover.
- 2) Sand used for the sand layer allowed in a treatment field trench shall have
 - a) a particle-size distribution that meets

- i) the concrete sand specification provided in CAN/CSA-A23.1, "Concrete Materials and Methods of Concrete Construction,"
- ii) the concrete sand specification provided in ASTM-C33, "Standard Specification for Concrete Aggregates," or
- iii) the particle-size distribution required for a medium-sand sand filter as set out in Sentence 5.3.3.4.(2),
- b) no more than 1 percent of a particle size passing through a 0.15 mm (0.0059 in.), No. 100 sieve,
- c) an effective particle size (D_{10}) of not less than 0.3 mm, and
- d) a uniformity coefficient (CU) of between 4 and 6.
- 3) When shredded tires are used as weeping lateral trench media, they shall be individual pieces
 - a) between 25 mm (1 in.) and 50 mm (2 in.) in size, and
 - **b)** washed free of particles, *fines*, and dust.

8.2.3.2. **Piping**

1) Piping used in a treatment field shall meet the requirements of Section 2.5.

Section 8.3. Chamber System Treatment Fields

8.3.1. Chamber System Treatment Fields — Objectives and Design Standards

8.3.1.1. General

- 1) The objectives set out in Subsection 8.2.1. apply to chamber system treatment fields.
- 2) The design of chamber system treatment fields shall meet requirements set out in this Standard except as provided in this Section.

Serial Distribution Prohibited 8.3.1.2.

1) Serial distribution shall not be used as the method of distributing effluent to weeping lateral trenches that use chambers.

8.3.1.3. Chamber Dimensions

1) Chambers shall be a minimum of 300 mm (1 ft.) wide and a maximum of 900 mm (3 ft.) wide.

Calculation of Infiltration Area 8.3.1.4.

1) The effective soil infiltration surface area provided by chambers shall be calculated using the exterior width at the base of the chamber.

8.3.1.5. Calculation of Trench Bottom Area

- 1) Notwithstanding Article 8.2.1.7., and as limited by Article 8.3.1.6, the effluent hydraulic loading rates for a treatment field using chambers may be increased by a factor of
 - a) 1.1 when primary treated effluent Level 1 is distributed in the trench by gravity,
 - **b)** 1.3 when the *primary treated* effluent *Level 1* is distributed using *pressure* distribution lateral piping and no reduction in area has been calculated for the use of pressure distribution lateral piping as provided in Article 8.2.1.8., and
 - c) 1.1 when secondary treated effluent is distributed using pressure distribution, or
 - d) 1.2 when secondary treated effluent is distributed using pressure distribution on timed dosing.

Loading Rate Not to Exceed 7 Day Travel Time Limits 8.3.1.6.

1) The effluent hydraulic loading rate on the actual open area provided by the chambers shall not exceed the effluent hydraulic loading rates set out in Articles 8.1.1.2., 8.1.1.3., and 8.1.1.5., or that would result in the travel time of effluent to the treatment boundary limit to be less than 7 days, as limited by Clause 8.1.1.4.(1)(d).

8.3.2. Chamber System Treatment Fields — Prescriptive Requirements and Installation Standards

8.3.2.1. Separation Distances

1) The location of a sub-surface chamber system shall comply with the requirements of Article 8.2.2.1. that sets out the minimum separation distances for *treatment fields*.

8.3.2.2. Manufacturer's Instructions

1) Chamber systems shall be installed in accordance with the manufacturer's instructions, except that in the event of a conflict with this Standard, the requirements of this Standard shall apply.

8.3.2.3. Prevention of Soil Disturbance and Erosion

- 1) Chamber system installations that do not include effluent distribution piping running the total length of the trench shall include a means to dissipate the hydraulic energy of the effluent delivered to the trench in order to minimize the disturbance and erosion of soil at the trench bottom where the effluent is delivered by using¹
 - a) geotextile fabric covering the width of the trench under the chamber in the most upstream 1.5 m (5 ft.) portion of the weeping lateral trench or other area that receives effluent.
 - **b)** a minimum of 50 mm (2 in.) of *gravel* in the most upstream 1.5 m (5 ft.) portion of all weeping lateral trenches or any other area that receives effluent, or
 - c) other suitable means to dissipate the hydraulic energy of the effluent it is receiving and prevent erosion or disturbance of the trench bottom.

1 Intent: Sentence (1) — To prevent erosion or disturbance of the trench bottom by the effluent that spills into the chamber rather than being piped the entire length of the chamber lateral.

8.3.3. Chamber System Treatment Fields — Requirements for Materials

Certification 8.3.3.1.

1) All Chambers shall be certified as meeting or exceeding the requirements of the American Association of State Highway and Transportation Officials H -10 or H -20 ratings.

Section 8.4. Treatment Mounds

8.4.1. Treatment Mounds — Objectives and Design Standards

8.4.1.1. General

- 1) The design and installation of a *treatment mound* has the following objectives:
 - a) breaking down the *organic loading* contained in the sewage effluent,
 - b) enabling the transfer of an adequate supply of oxygen into the sand layer through the disturbed soil used to construct the berm covering the sand layer of the treatment mound.
 - c) providing an area of soil over which the effluent is spread to reduce the hydraulic and organic loading on each part of the soil infiltration surface,
 - d) utilizing the upper biological layers of the soil and maximize the available vertical separation distance to underlying restrictive layers in the soil by constructing the mound on top of the in situ soil, and
 - e) to introducing the effluent into the soil and be constructed in a manner that minimizes the risk of effluent breakout through the soil used to construct the berm of the treatment mound covering the sand layer and provide a barrier against direct contact with the effluent.
- 2) The design of a treatment mound shall meet all requirements set out in Section 8.1.

8.4.1.2. Effluent Treatment Quality in Soil

- 1) At a depth of 900 mm (3 ft.) below the bottom of the required thickness of the sand layer and in the effluent/groundwater plume at the edge of the berm, the treated effluent shall meet the following criteria:
 - a) fecal coliform < 10 CFU/100 mL above background levels, or
 - **b)** fecal coliform < 2MPN/gram of dry soil above background levels.
- 2) The effluent/groundwater plume shall not exceed background levels of fecal organisms 8 m (25 ft.) horizontally from the soil-based treatment area, as measured from the edge of the treatment mound berm, including during typical periods of climatic stress and/or typical/maximum designed flow volumes.

8.4.1.3. Sand Layer — Orientation on Slopes

- 1) The geometry of the sand layer shall conform to the surface slope contour of the site it is placed on, such that
 - a) the long axis of the sand layer (its longest dimension), including any 3 m (10 ft.) segment of the sand layer, shall be oriented at 90 degrees to the slope direction,
 - b) the downslope edge of the sand layer where it makes contact with the in situ (original) soil surface shall
 - i) be level along its length within 2% as measured from end to end or in any 3-m (10 ft.) segment of the sand layer, and
 - ii) be level within 100 mm (4 in.) as measured within any 600 mm (2 ft.) segment of its length, and

- c) when placed on a convex slope, the deflection of curvature of the sand layer where it meets the in situ soil will not exceed 15%, as measured by the horizontal deflection from a plane drawn from each end of the sand layer.
- 2) If there is documentation that the direction of groundwater movement is different from the slope of the land, the direction of groundwater movement must be considered in determining the preferred orientation of the sand layer as it relates to groundwater flow direction and soil characteristics for the purpose of managing linear loading rates and the impact of *groundwater mounding* below the system.

8.4.1.4. Sand Layer — Primary Treated Effluent

- 1) The sand layer of a mound receiving primary treated effluent Level 1 shall
 - a) have a surface area designed on the basis of an effluent hydraulic loading rate of not more than 40 L per square metre (0.83 lmp. gal. per sq. ft.) per day,
 - b) regardless of whether primary treated effluent Level 1 or secondary treated effluent is applied, have a sand layer surface area that does not exceed the effluent hydraulic loading rates determined under Articles 8.1.1.2, 8.1.1.3, 8.1.1.4, 8.1.1.5, and 8.1.2.4., and Sentences 8.1.2.2.(2) and (3) if the in situ soil is:
 - i) coarse sand.
 - ii) medium sand,
 - iii) fine sand,
 - iv) very fine sand.
 - v) loamy coarse sand,
 - vi) loamy medium sand,
 - vii) loamy fine sand,
 - viii) loamy very fine sand,
 - ix) coarse sandy loam, or
 - x) medium sandv loam.
 - c) not exceed 3 m (10 ft.) in width, measured at the top of the sand layer,
 - d) have a length that takes into account the effluent hydraulic linear loading rate limits set out in Article 8.1.2.3. or as determined under Article 8.1.1.7. that are based on soil texture, structure, consistency, and infiltration distance (depth) to seasonally saturated soil and restricting layers at the site,¹
 - e) be not less than 300 mm (1 ft.) thick, and
 - f) be on or above the existing soil.²
 - ¹ Note: Clause (1)(d) Article 8.1.2.3. provides a prescriptive solution for determining acceptable linear loading rates.

Sand Layer — Secondary Treated Effluent 8.4.1.5.

- 1) A treatment mound that receives secondary treated effluent shall be designed
 - a) using a sand layer that has a minimum average thickness of 75 mm (3 in.),
 - b) with a minimum distance of 900 mm (3 ft.) to a restrictive layer, as measured from the top surface of the 75 mm (3 in.) sand layer,
 - c) with a sand layer surface area designed on the basis of an effluent hydraulic loading rate of not more than 40 L per square metre (0.83 lmp. gal. per sq. ft.) per day, and
 - d) with a sand layer surface area required to ensure that the effluent hydraulic loading rate does not exceed the effluent hydraulic loading rates determined under Articles 8.1.1.2., 8.1.1.3., 8.1.1.4., 8.1.1.5., and 8.1.2.4., and Sentences 8.1.2.2.(2) and (3) if the in situ soil texture is:

² Intent: Clause (1)(f) — This Clause requires the mound to be built on the existing grade of the soil. Soil should not be stripped away so as to create a depression in the ground, or be replaced by fill material.

- i) coarse sand,
- ii) medium sand,
- iii) fine sand,
- iv) very fine sand,
- v) loamy coarse sand,
- vi) loamy medium sand,
- vii) loamy fine sand.
- viii) loamy very fine sand,
 - ix) coarse sandy loam, or
 - x) medium sandy loam.

Suitability of In-Situ Soil and Vertical Separation 8.4.1.6.

- 1) A treatment mound may be used as a final treatment component where
 - a) the in-situ (original) soil has an assigned loading rate as determined by Table 8.1.1.10. to a depth of at least 300 mm (1 ft.), and
 - b) a minimum vertical separation of 900 mm (3 ft.) is maintained between the bottom of the required depth of sand layer and any restrictive layer below the treatment mound.1

8.4.1.7. Infiltration Into In Situ Soil

- 1) The area of contact with the in situ soil that is within the berm forming the mound, excluding the end slopes, shall provide a soil infiltration surface area into the in situ soil that1
 - a) is not less than the required soil infiltration surface area determined by Article 8.1.1.10. using loading rates for secondary treated effluent Level 2, and
 - b) when on a slope exceeding 1 percent, includes only the area downslope of the upslope side of the sand layer area receiving the effluent to the downslope edge of the berm.

2) The fill soil forming the berm covering the required soil infiltration surface area required by Sentence (1) shall be a soil that has a soil texture classification of coarse sand, medium sand, fine sand, loamy medium sand, or loamy coarse sand.

8.4.1.8. Distribution of Effluent

- 1) The distribution of effluent onto the sand layer shall be done using pressure distribution lateral pipes that are located in¹
 - a) a layer of gravel over the sand layer as set out in Article 8.4.2.5, or
 - b) chambers that provide an effective effluent infiltrative area within the internal opening area of the chambers over the sand layer that is not less than 80% of the required sand layer area determined by the design effluent hydraulic loading rate.

 1 Intent: Sentence (1) — The actual open area under the chambers providing direct effluent contact with the sand layer must comprise at least 80% of the required area. The internal dimensions of the chamber need to be measured, as there is normally a significant footprint area of the chambers that covers a portion of the sand layer. The gravel layer or chambers must provide a void space for temporary storage of the effluent delivered during a dose event and during peak flow periods.

¹ Note: Clause (1)(b) — The sand layer receiving the effluent may be increased in thickness to provide the vertical separation required. Using the same sand as is required for the 300 mm (1 ft.) sand layer is advised. The fill must have a textural classification not finer than fine sand. Sand with any significant percentage of silt or clay content should not be used, as it will cause excessive compaction and will be washed down over time through the fill material as the effluent is applied, resulting in the development of a restrictive layer.

¹ Intent: Sentence (1) — To ensure that an adequate area of soil is available for the effluent to infiltrate into the in situ soil, and that the permeability of the berm fill material enables the effluent to be readily distributed over the infiltration area and thereby prevent the effluent from mounding in the sand layer.

8.4.1.9. Using Chambers

1) Where chambers are used, a pressure effluent distribution lateral pipe shall be provided for each of the chamber-sand layer contact areas provided by the chambers.

8.4.1.10. Maximum Dose Volume

1) The design of the treatment mound and pressure distribution lateral pipe system shall be based on achieving the ability to deliver individual doses of effluent over the entire sand layer area that do not exceed 20% of the average daily effluent volume. 1

¹ Intent: Sentence (1) — Smaller doses provide better treatment conditions. Doses may be smaller than 20%. A 20% dose volume results in 5 doses per day. The entire sand layer does not have to be dosed during an individual dose event; however, the design must ensure that each area of the sand layer served by an individual orifice receives not more than 20% of the average daily flow. For example, if a distribution system was designed with two alternating zones, the system needs to be designed on the basis of 10 doses per day in total — 5 doses for each zone.

8.4.1.11. Pressure Distribution Required

1) Distribution of effluent shall be achieved using a pressure distribution lateral pipe system meeting the requirements of Section 2.6. and effectively distribute the effluent as set out in Article 8.4.2.6.

8.4.1.12. **Effluent Ponding Monitoring Pipes**

- 1) The *mound* design shall include *effluent* ponding monitoring pipes that enable monitoring the depth of effluent ponding at the sand layer infiltration surface and at the sand layer-in situ soil interface.
- At a minimum there shall be
 - a) two effluent ponding monitoring pipes to monitor the depth of effluent ponding at the interface of the sand layer and in situ soil, each one located at a quarter of the length of the sand layer and not more than 4.5 m (15 ft.) from each end of the sand layer, and along the centre line of the sand layer on a site having less than a 1% slope or on the downslope side of the sand layer, if on a slope greater than 1%,
 - **b)** effluent ponding monitoring pipes shall be provided to monitor ponding of effluent on the sand layer infiltration surface and be located within 1.5m (5 ft.) of each end of the sand layer and, if chambers are used, an effluent ponding monitoring pipe shall be provided at those positions for each continuous row of chambers.
- 3) The effluent ponding monitoring pipe shall
 - a) extend to finished grade,
 - **b)** be fitted with a manufactured access box, and
 - c) be provided with perforations that
 - i) allow entry of ponded effluent while excluding the sand or gravel media surrounding the access port, and
 - ii) are located within the vertical section of the mound they are intended to monitor the depth of ponded effluent in, as required by Sentence (1) or (2)

8.4.2. Treatment Mounds — Prescriptive Requirements and Installation Standards

8.4.2.1. Separation Distances

1) A treatment mound shall not be located within

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- a) 15 m (50 ft.) of a water source or water well,
- **b)** 100 m (330 ft.) from a licensed municipal water well
- c) 15 m (50 ft.) of a water course, except as provided in Article 2.1.2.4.,
- d) 3 m (10 ft.) of a property line,
- **e)** 3 m (10 ft.) of a septic tank,
- f) 10 m (33 ft.) of a basement, cellar, or crawl space, and
- **q)** 10 m (33 ft.) of a *building* that does not have a basement, cellar, or crawl space.
- 2) For the purposes of Sentence (1), all measurements are to be taken from the point where the side slope of the *mound berm* intersects with the natural *soil* contour.

8.4.2.2. Diverting Run-off Water

1) Whenever treatment mounds are located on slopes, a diversion shall be constructed immediately upslope of the upper side of the mound berm to intercept and direct run-off water away from the mound.

8.4.2.3. Sand Layer Thickness

1) The sand layer that primary treated effluent Level 1 is distributed over shall be a minimum of 300 mm (1 ft.) thick, and the top of the sand layer shall be nominally level.

8.4.2.4. Placement of Sand Layer

- 1) The sand layer and fill material shall be put in place using methods that minimize compaction of the soil under the sand layer and prevent smearing or glazing of the soil under the *mound* area that would be at least equivalent to using track-type machinery and ensuring at least 150 mm (6 in.) of sand is kept beneath the track-type machinery.
- 2) The in situ soil shall be broken up and the sand layer material and berm fill material shall be integrated into the in situ soil.

8.4.2.5. Use of Gravel

- 1) When *gravel* is used over the sand layer,
 - a) not less than 150 mm (6 in.) of gravel shall be placed over the contact area below the distribution lateral pipes,
 - b) not less than 25 mm (1 in.) of gravel shall be placed over the distribution lateral pipes, and
 - c) the gravel layer shall be covered with
 - i) straw or equivalent fibrous material to an un-compacted depth of 75 mm to 100 mm (3 to 4 in.), or
 - ii) a geotechnical fabric suitable for the purpose of preventing the migration of the covering soil into the gravel while allowing the movement of air and water.

Orifice Spacing over Sand Layer 8.4.2.6.

1) The pressure effluent distribution lateral pipe supplying effluent to the sand layer shall be spaced evenly over the sand layer with orifice spacing that provides one orifice for every 0.5 square metres (5.5 sq. ft.) or less of the sand layer.

8.4.2.7. Mound Berm Fill Material

- 1) Coarse sand, medium sand, fine sand, loamy medium sand, or loamy coarse sand fill material shall be used to form the berm of the overall mound required to cover the soil infiltration surface area and it shall be
 - a) placed to a minimum depth of 150 mm (6 in.) at the sides of the sand layer, and
 - b) provide a slope to ensure drainage of surface water from the mound. Intent: Sentence (1) — To provide an adequate slope on the top of the treatment mound in order to prevent storm water from standing on the top of the mound. A minimum 4% slope (0.5 inch per foot) is recommended.
- 2) In addition to the requirements of Sentence (1), 75 mm (3 in.) of soil having a texture not finer than sandy loam and not coarser than loamy fine sand shall be placed over the fill material to cover the entire area of the mound in order to support a grass cover.

8.4.2.8. **Grass Cover**

1) A vegetative (grass) cover shall be established over the entire area of the mound.¹ 1 Intent: Sentence (1) — A contractor meets the requirement of this Sentence by seeding the mound to grass, leaving to the owner the responsibility to water and maintain the grass cover. The grass cover is needed to prevent erosion of the mound and to assist in evaporating the effluent.

8.4.2.9. Side Slopes of Mound

1) The side slopes of the *mound* shall not be steeper than 1:3 (one vertical to three horizontal).

8.4.3. Treatment Mounds — Requirements for **Materials**

8.4.3.1. Sand

- 1) Sand used for the sand layer shall have
 - a) a particle-size distribution that meets
 - i) the concrete sand specification provided in CAN/CSA-A23.1, "Concrete Materials and Methods of Concrete Construction,"
 - ii) the concrete sand specification provided in ASTM-C33, "Standard Specification for Concrete Aggregates," or
 - iii) the particle-size distribution required for a medium-sand sand filter as set out in Sentence 5.3.3.4.(2),
 - **b)** an effective particle size (D_{10}) of not less than 0.3 mm,
 - c) a uniformity coefficient (CU) of between 4 and 6, and
 - d) less than 1% fines content by weight.

8.4.3.2. Drain Media

- 1) Drain media used in a mound shall
 - a) consist of clean washed gravel, clean crushed rock, or other equivalent media that will maintain structural integrity and not be degraded by the environment created in the treatment field trench,
 - b) have a particle-size distribution by weight of
 - i) 100 percent passing the 50 mm, (2 in.) sieve,
 - ii) 0 to 25 percent passing the 12.5 mm, (½ in.) sieve,
 - iii) 0 to 10 percent passing the 9.51 mm (3/8 in.), sieve,
 - iv) 0 to 2 percent passing the 1.18 mm (3/64 in.), No. 16 sieve, and

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- v) 0 to 1 percent passing the 0.15 mm (0.0059 in.) No, 100 sieve, and
- c) be able to withstand vertical and horizontal loads from backfill equal to a minimum of 1 m (3.25 ft.) of earth cover.

8.4.3.3. Chambers

1) All Chambers shall meet or exceed the requirements of the American Association of State Highway and Transportation Officials H -10 or H -20 ratings.

Section 8.5. Sub-surface Drip Dispersal and Irrigation

8.5.1. Sub-surface Drip Dispersal and Irrigation — Objectives and Design Standards

8.5.1.1. Effluent Treatment Quality in Soil

- 1) At a depth of 900 mm (3 ft.) below the drip dispersal lines and in the wastewater effluent/groundwater plume at a distance of not more than 900 mm (3 ft.) from the edge of the soil-based treatment area, the treated effluent shall meet the following criteria:
 - a) fecal coliform < 10 CFU/100 mL above background levels, or
 - b) fecal coliform < 2 MPN/gram of dry soil above background levels.
- 2) The effluent/groundwater plume shall contain no viable fecal organisms 8 m (27 ft.) horizontally from the soil-based treatment area, as measured from the edge of the soilbased treatment area, including during typical periods of climatic stress and/or typical maximum designed flow volumes.

8.5.1.2. General

1) The design of a subsurface drip dispersal system shall meet all requirements set out in Section 8.1.

Required Effluent Quality and SAR Limits 8.5.1.3.

- 1) Effluent delivered to a drip dispersal system shall be treated to a
 - a) secondary treated effluent Level 2 standard or better, and
 - b) secondary treated effluent Level 3–D2 standard or better when the drip tubing is installed with less than 300 mm (1 ft.) of cover.
- 2) Effluent shall have an SAR of less than 10 when the drip dispersal tubing is placed at a depth of less than 450 mm (18 in.) below ground surface and the effluent hydraulic loading rates are selected to meet typical irrigation needs (as opposed to effluent dispersal at the rates set out in this Standard) to prevent negative impact on vegetation at the ground surface due to the accumulation of sodium in the root zone of the vegetation.

8.5.1.4. Dispersal

- 1) The drip dispersal system shall be designed to prevent instantaneous loading during a dose event from saturating the soil within 50 mm (2 in.) of the ground surface.
- 2) The geometry and orientation of the drip dispersal area shall not cause the *hydraulic* loading to exceed the linear loading capacity of the soil as determined in Article 8.1.1.7. or 8.1.2.3.

8.5.1.5. Winter Use Restrictions and Design

- 1) Where the system is used for a *development* that requires *wastewater* treatment during the period of November 30 to March 31
 - a) the system shall be protected from freezing and all piping sloped to ensure drainage of all piping back to the dose tank, and
 - b) an alternate system meeting the requirements of this Standard shall be provided for use in the event the drip distribution system freezes.

8.5.1.6. **Effluent Loading Rates**

- 1) The effluent hydraulic loading rates shall not exceed those set out in Table 8.1.1.10. or otherwise restricted by this Standard.
- 2) The effluent soil infiltration surface area supplied by a single drip dispersal tube shall be considered to be no more than 300 mm (12 in.) on either side of the drip dispersal tubing for a total calculated soil infiltration surface width of not more than 600 mm (2 ft.) per drip dispersal lateral.

8.5.1.7. Drip Dispersal Tubing Layout and Dosing Design

- 1) The drip dispersal tubing shall be equipped with pressure compensating orifices.
- 2) A means of preventing root intrusion into the emitters/orifices shall be provided in the system design.
- 3) The system shall have a means of inhibiting bacterial growth and the accumulation of slime in the emitters/orifices.
- 4) A minimum of one orifice shall be provided for each 0.37 square metres (4 sq. ft.) of soil infiltration surface area.
- 5) The system shall be dosed using timed dosing controls to ensure that dosing events occur at evenly spaced intervals over a 24-hour period.
- 6) Drip dispersal tubing shall have orifices that have a rated flow of not more than 2 L per hour (0.44 lmp. gal. per hour or 0.53 U.S. gal. per hour) when installed in soil that has a texture of
 - a) sandy clay loam,
 - **b)** clay loam,
 - c) silty clay loam,
 - d) sandy clay,
 - e) clay,
 - f) silty clay, or
 - **q)** heavy clay.
- 7) Drip dispersal tubing shall be installed
 - a) following the slope contour,
 - b) as level as possible, and
 - c) at a depth of between 150 mm (6 in.) and 900 mm (36 in.) below finished grade.

8.5.1.8. Drip Dispersal Tubing Flushing Requirements

- The system shall be capable of flushing all parts of the drip dispersal piping at a minimum flow velocity of 0.6 m/s (2 ft/s).¹
 - Note: Sentence (1) Backwashing/flushing with a return to a location set out in Sentence (3) may be done continuously or periodically based on a pre-set interval, the number of dosing cycles, or the measurement of pressure difference across the filter (such as a 20% difference in pressure), or any combination of these criteria.
- The volume of a flushing dose shall be at least twice the volume of all pressurized piping.
- 3) The return line used to facilitate flushing shall return to the *building sewer* where it connects to an initial treatment component, or into an initial treatment component in a manner that does not result in undesirable disturbance of the settling tank or septic tank.

8.5.1.9. Operational Control Required

- 1) The operation of a drip dispersal system of any capacity shall be managed using a control panel that can
 - a) monitor the volume per flow event and per day applied to the soil,1
 - b) provide for automatic flushing of filters and drip laterals with filtered effluent, initiated by a timer and/or a pre-set pressure differential across the filters,
 - c) deliver designer-specified volumes of effluent to each field zone (adjustable and variable between zones) at designer-specified time intervals,
 - **d)** monitor alarm conditions (e.g., high water, power outage),
 - e) monitor flow variance and provide indication of when flow is ±20% of design, indicating servicing is required,
 - f) monitor pump run times,
 - g) monitor numbers and times of filter and field flushing cycles,
 - h) record the operational events for a minimum of the previous 30 days, and
 - i) meet any additional requirements for system controls set out in Sections 2.3. and

8.5.2. Sub-surface Drip Dispersal and Irrigation — Prescriptive Requirements and Installation Standards

8.5.2.1. Separation Distances

- 1) An effluent drip dispersal system, measured from any part of the drip dispersal tubing, shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - **b)** 100 m (330 ft.) of a licensed municipal water well,
 - c) 15 m (50 ft.) of a water course, except as required by Article 2.1.2.4.,
 - **d)** 1.5 m (5 ft.) of a *property* line,
 - e) 10 m (33 ft.) of a basement, cellar, or crawl space, except that this distance may be reduced to 1.5 m (5 ft.) when the system is used specifically for irrigation and the effluent hydraulic loading rates do not exceed irrigation needs,
 - f) 1 m (3.25 ft.) of a building that does not have a permanent foundation,

¹ Note: Clause (1)(a) — This may be accomplished by the ability of a control system to count and record dose events and pump run times during a 24 hr. period.

- g) 5 m (17 ft.) of a building that has a permanent foundation but does not have a basement, cellar, or crawl space, except that this distance may be reduced to 1.5 m (5 ft.) when the system is used specifically for irrigation and the effluent hydraulic loading rates do not exceed irrigation needs, and
- h) 5 m (17 ft.) of a septic tank or packaged sewage treatment plant, except that this distance may be reduced to 1.5 m (5 ft.) when the system is used specifically for irrigation and the effluent hydraulic loading rates do not exceed irrigation needs.

¹ Note: Clause (1)(d) — The 10 m (33 ft.) requirement to a cellar, basement, or crawl space is intended to protect excavations below grade from accumulating migrating effluent. A crawlspace that is not below grade, or where the level of the ground surface at the soil-based treatment area is below the level of the crawlspace, would not require 10 m (33 ft.) clearance and could be treated as a building with a permanent foundation without a basement.

8.5.2.2. Prohibited Locations

- 1) An effluent drip dispersal system shall not be located under
 - a) a roadway or driveway,
 - b) a paved area,
 - c) a vehicle parking lot,
 - d) any structure, or
 - e) a vegetable garden.

8.5.2.3. Linear Loading Limits

1) The arrangement of the drip dispersal tubing shall ensure that the maximum *linear loading* as set out in Table 8.1.1.10. or determined in accordance with Article 8.1.1.7. is not exceeded.

8.5.2.4. Clean-outs and Piping Access

- 1) Clean-outs shall be provided for the supply and return piping.
- 2) Access from the ground surface shall be provided to all valves, air release/intake valves, filters, and the two drip emitters located along the highest and lowest orifices.

8.5.2.5. Manufacturer's Recommended Practices

A drip dispersal system shall be installed following all of the manufacturer's
recommendations except where the manufacturer's recommendations conflict with the
requirements of this Standard, in which case the requirements of this Standard shall
apply.

8.5.3. Sub-surface Drip Dispersal and Irrigation — Requirements for Materials

8.5.3.1. Piping

- 1) Piping other than sub-surface drip dispersal tubing used in a drip dispersal system shall comply with the requirements of Section 2.5.
- 2) Sub-surface drip dispersal tubing shall
 - **a)** have a warranty provided by the manufacturer for use with *wastewater* and for resistance to root intrusion,
 - **b)** incorporate emitters with a maximum nominal rated discharge of 3.64 L (0.8 lmp. gal.) per hour, except where required to be less, as set out in Sentence 8.5.1.7.(6), and

- c) be colour-coded purple or permanently marked at 1 m (3.25 ft.) intervals to identify that the pipe contains non-potable water from a wastewater source.
- 3) The emitter discharge rate referred to in Clause (2)(b) may be controlled by the use of pressure-compensating emitters.
- 4) Equipment used in a drip dispersal system must be specifically designed and intended for use in a drip dispersal system or recommended by the manufacturer for that use.

Section 8.6. LFH At-grade Treatment Systems

8.6.1. LFH At-grade Treatment Systems— Objectives and Design Standards

8.6.1.1. General

- 1) An LFH At-grade system shall meet the following objectives:
 - a) break down the organic loading contained in the effluent,
 - b) provide an area of soil over which the effluent is spread to reduce the hydraulic and organic loading on each part of the soil infiltration surface,
 - c) spread the effluent over a suitably sized area to enable sufficient oxygen to be transferred through the soil in order to achieve treatment objectives and long-term utilization, and
 - d) introduce the effluent into the soil and be constructed in a manner that minimizes the risk of effluent breakout through the material covering the soil infiltration surface area that provides a barrier against direct contact with the effluent.
- 2) The design of an LFH At-grade system shall meet all requirements and objectives set out in Section 8.1.

8.6.1.2. Effluent Treatment Objectives in Soil

- 1) An LFH At-grade system shall treat the applied effluent as it migrates through the soil, as measured at the vertical separation treatment boundary limit required for the design and effluent quality being applied, to the following quality:
 - a) fecal coliform < 10 cfu/100 mL above background levels, or
 - **b)** fecal coliform < 2 MPN/gram of dry soil above background levels.

8.6.1.3. Applied Effluent Quality

1) The effluent applied to the soil infiltration surface of an LFH At-grade system shall meet a secondary treatment standard Level 2 as set out in Article 5.1.1.1. or better quality.

8.6.1.4. Located in Forested Area

- 1) The LFH At-grade system shall be located in a forested area that
 - a) provides shelter from the cooling effect of winds and also maximizes snow cover over the system, and
 - b) has a minimum 50 mm (2 in) LFH layer that allows the relatively fast horizontal spread of the applied effluent over the soil-based treatment area that is under the cover material of the system.

8.6.1.5. Cover Material and Stability

- 1) The material covering the LFH At-grade system soil infiltration surface area shall be consistent with the ecology of the forested area and be effective at minimizing the risk of direct contact with the effluent by humans and animals.
- 2) The depth of the cover material shall be a minimum of 230 mm (9 in.) above the infiltration chambers after settlement of the cover material occurs.²
- 3) The slope of the cover material shall be minimized to prevent slumping and loss of cover depth, or be stabilized using acceptable methods.

4) The cover material shall extend a sufficient distance beyond the *infiltration* chambers to ensure that the effluent applied at the design effluent hydraulic loading rate infiltrates into the soil within the cover material to prevent risk of direct contact.

Note: Sentence (1) — The cover material typically used is wood chips. Wood chips are suitable with the forest ecology where these systems are to be installed. The wood chips allow the forest undergrowth to grow through the cover material, consolidating the entire system into the forest floor over time This is important to minimize the risk of direct contact with the effluent by people or animals.

² Note: Sentence (2) — The depth of the cover material at time of installation will need to be substantially more than 230 mm (9 in.) to allow for settling and still achieve a minimum 230 mm (9 in.) cover after settlement. Fresh wood chips will settle substantially while old weathered wood chips will not settle as much. Anticipating that fresh wood chips may settle by 50% is not unreasonable.

8.6.1.6. Effluent Loading Rates

- 1) The effluent hydraulic loading rate on the soil infiltration surface directly under the infiltration chambers shall not exceed 40.7 litres per sq. metre per day (0.83 gal./sq. ft./d) or as limited by Sentences 8.1.2.2 (2) and 8.1.1.2 (3) to achieve effective treatment of the effluent.
- 2) Notwithstanding Sentence (1),
 - a) the area provided by the actual internal open area of the chamber needs to cover a minimum of 80% of the required soil infiltration surface area determined under Sentence (1), or
 - b) the effluent hydraulic loading rate can be increased by a factor as allowed by Article 8.3.1.5.
- 3) The design effluent hydraulic loading rate on the soil infiltration surface area under the LFH At-grade system cover material shall not exceed the values set out in Table 8.1.1.10.¹
- 4) The soil infiltration surface area required by Sentence (3) shall include the area covered by the infiltration chambers and the cover material
 - a) on both sides of the *infiltration* chamber when the slope is less than 1%, or
 - b) only on the downslope side of the *infiltration* chamber when the system is on a slope greater than 1%.

Note: Sentence (3) — The total area covered by both the infiltration chambers and cover material, as set out in Sentence 4, is determined by dividing the peak daily wastewater flow by the allowed effluent hydraulic loading rate set out in Table 8.1.1.10. for the soil at the site.

8.6.1.7. Time Controlled Pressure Distribution of Effluent Required

- 1) Effluent shall be distributed using an effluent pressure distribution lateral pipe system meeting the design requirements and objectives of Subsection 2.6.1.
- 2) Time controlled dosing of the individual doses of effluent applied to the LFH At-grade system shall be evenly spread over a 24-hr. period, and the volume of each effluent dose shall be minimized to achieve as many doses as possible in a 24-hr. period based on system design flows.

8.6.1.8. System Geometry and Linear Loading Rate Design

- 1) The design and geometry of the effluent soil-based treatment area of the LFH At-grade system shall result in an effluent hydraulic linear loading rate that does not exceed the soil profile's capability to allow the horizontal movement of the effluent away from the treatment system when downward vertical effluent flow will be restricted and shall be designed to meet
 - a) the values set out in Table 8.1.1.10. that relate horizontal movement of effluent through the soil to the characteristics of the soil profile and the slope of the landscape, or

b) a comprehensive and documented assessment and calculation of the soil's capacity to transmit the effluent horizontally, as set out in Article 8.1.1.9.

8.6.1.9. Orientation on Slopes

- 1) The geometry of the LFH At-grade system shall conform to the surface slope contour of the site it is placed on such that
 - a) the long axis of the LFH At-grade system, including any 3 m (10 ft.) segment of the LFH At-grade system, shall be oriented at 90 degrees to the slope direction, and
 - **b)** the downslope edge of the *LFH At-grade* system where it makes contact with the in situ soil surface shall
 - i) be level along its length within 2% as measured from end to end or in any 3 m (10 ft.) segment of the LFH At-grade system,
 - ii) be level within 100 mm (4 in.) as measured within any 600 mm (2 ft.) segment of its length, and
 - when placed on a convex slope, the deflection of curvature of the LFH Atgrade system where it meets the in situ soil will not exceed 15%, as measured by the horizontal deflection from a plane drawn from each end of the LFH Atgrade system.

8.6.2. LFH At-grade Treatment Systems -Prescriptive Requirements and Installation Standards

8.6.2.1. Separation Distances

- 1) An LFH At-grade system shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - b) 100 m (330 ft.) of a municipal licensed water well,
 - c) 15 m (50 ft.) of a water course, except as restricted in Article 2.1.2.4.,
 - d) 3 m (10 ft.) of a property line where the ground is level or slope is less than 1%,
 - e) 6 m (20 ft.) of a property line that is located downslope of the LFH At-grade system where the slope is 1% or more,
 - f) 3 m (10 ft.) of a septic tank, packaged sewage treatment plant, effluent tank, or other tank in the system, and
 - g) 10 m (33 ft.) of a building.
- 2) For the purposes of Sentence (1), all measurements are to be taken from the point where the side slope of the *cover* material intersects with the natural *soil* contour.

Infiltration Chambers Covering the Effluent Pressure 8.6.2.2. **Distribution Laterals**

- 1) Each distinct row of *infiltration* chambers that provide the direct soil infiltration surface area required for the LFH At-grade system shall include at least one effluent pressure distribution lateral pipe that has orifices spaced at not more than 600 mm (2 ft.) apart and that meets the requirements of Section 2.6.
- 2) Chambers shall meet the requirements set out in Sub-section 8.6.3.

8.6.2.3. Individual Infiltration Chamber Laterals Level Throughout Length

- 1) Each lateral that consists of the effluent pressure distribution lateral pipe and covering infiltration chamber shall be level along the long axis within
 - a) 2% end to end.
 - b) 2% within any 3 m (10 ft.) segment of the lateral, and
 - c) 10 cm (4 in.) within any 600 mm (2 ft.) segment.

8.6.2.4. Design for 5 Individual Doses Per Day

1) The design of the pressure distribution lateral pipe system, the effluent tank, and pump control settings shall be based on achieving the ability to deliver individual doses of effluent that do not exceed 20% of the design average daily effluent volume over the entire LFH At-grade system.1

Intent: Sentence (1) — Smaller individual-dose volumes provide better treatment conditions and minimize the chance that the effluent will break out of the At-grade system due to a large individual-dose volume. Doses may be smaller than 20%. A 20% dose volume results in 5 doses per day. The entire At-grade systems does not have to be dosed during an individual dose event; however, the design must be based on each dosed area of the At-grade system receiving 5 doses of effluent per day based on average daily flow. For example, if a distribution system was designed with two alternating zones, the system needs to be designed on the basis of 10 doses per day in total — 5 doses for each zone.

Cover Material Depth, Slope and Stabilization 8.6.2.5.

- 1) The cover material shall be a minimum of 225 mm (9 in.) in thickness over all infiltration chambers in the LFH At-grade system when settled. 1
- 2) The cover material shall consist of materials set out in Article 8.6.3.2.
- 3) The placed cover material shall have a maximum slope of
 - a) 2 horizontal to 1 vertical when no stabilization method is used, or
 - b) 1 horizontal to 1 vertical when acceptable geo-tech erosion control and slope stabilizing material is used to contain and stabilize the cover material.
 - ¹ Note: Sentence (1) The depth of the cover material at time of installation will need to be substantially more than 230 mm (9 in.) to allow for settling and still achieve a minimum 230 mm (9 in.) cover after settlement. Fresh wood chips will settle substantially while old weathered wood chips will not settle as much. Anticipating that fresh wood chips may settle by 50% is not unreasonable.

Minimize Impact on LFH Layer and Underlying Soil 8.6.2.6. **During Construction**

- 1) The LFH layer of the soil profile shall not be removed in the area of the LFH At-grade system.
- 2) Brush and small trees shall be cut off at ground level, not pulled out of the ground.
- 3) The installation shall be carried out in a manner that minimizes compaction of the soil under the LFH At-grade system and the downslope side of the LFH At-grade system.

8.6.2.7. Effluent Monitoring Access Ports

- 1) The LFH At-grade system shall include access ports into the infiltration chambers that have a minimum dimension of 100 mm (4 in.) and that terminate at the surface of the cover material in order to enable monitoring the depth of effluent ponding and soil moisture conditions at the soil infiltration surface.
- 2) At a minimum, there shall be two access ports as required by Sentence (1), each one located not more than 4.5 m (15 ft.) from each end of a continuous row of infiltration chambers that cover an individual effluent pressure distribution lateral pipe.
- 3) The access ports required by Sentence (1) shall
 - a) be accessible from the surface of the cover material at finished elevation,
 - **b)** be fitted with a mechanically fastened top to prevent the entry of foreign material,

- c) allow viewing of both the infiltration chamber interior and soil infiltration surface, and
- d) provide access for sampling of the soil infiltration surface.

8.6.3. LFH At-grade Treatment System - Material Requirements

8.6.3.1. Infiltration Chamber

1) All chambers shall meet or exceed the requirements of the American Association of State Highway and Transportation Officials H -10 or H -20 ratings.

8.6.3.2. Cover Material

- 1) The cover material used shall be
 - a) wood chips of a size that easily allows the grain of the wood to be seen (sawdust is not acceptable), or
 - b) peat moss that is seeded with a vegetative selection that is free of invasive species and suitable to the forest ecology in order to establish a vegetative cover that will stabilize the peat moss.
- 2) Material used to stabilize cover material shall be a geo-tech erosion control and stabilizing material that
 - a) will hold the LFH At-grade system cover material in place to prevent slumping from mechanical or natural forces, and
 - **b)** is made of a decomposable material.

Section 8.7. Open Discharge Systems

8.7.1. Open Discharge Systems— Objectives and **Design Standards**

8.7.1.1. General

- 1) The design of an open discharge system shall meet all requirements set out in Section 8.1. except for the effluent hydraulic loading rates.
- 2) An open discharge system shall not be used on soils that have a soil texture classification of coarse sand, medium sand, fine sand, loamy medium sand, or loamy coarse sand within 1.5 m (5 ft.) of the ground surface.
 - ¹ Intent: Sentence (2) The soil the effluent is discharged onto must have a textural class that will encourage the spreading of effluent, as opposed to allowing the effluent to quickly enter the soil in a concentrated area causing saturated flow.
- 3) The design and location of an open discharge system that discharges effluent onto the surface of the ground must ensure that the effluent is contained on the property.
- 4) An open discharge system shall be designed to minimize the pooling of effluent on the ground surface.
- 5) The design of the *open discharge system* outlet and the landscaping of the area of the open discharge system shall ensure that the effluent does not migrate more than 30 m (100 ft.) before infiltrating into the ground.

8.7.1.2. Preventing Erosion

1) The soil that the effluent is discharged onto shall be protected from erosion caused by the discharge of effluent from the outlet.1

Intent: Sentence (1) — The design of the point of discharge must include landscaping to effectively disperse the effluent while also protecting the soil from erosion.

8.7.2. Open Discharge — Prescriptive Requirements and Installation Standards

8.7.2.1. Separation Distances

- 1) An open discharge system may be installed in a location that provides separation distances from the point of discharge of not less than
 - a) 50 m (165 ft.) to a water source or water well,
 - **b)** 100 m (330 ft.) from a licensed municipal water well
 - c) 45 m (150 ft.) to a water course except as required by Article 2.1.2.4.,
 - **d)** 90 m (300 ft.) to a *property* line, and
 - **e)** 45 m (150 ft.) to a building.
- 2) The effluent discharge piping shall be buried to at least the point where the separation distances set out in Sentence (1) are met.

8.7.2.2. Open Discharge Prohibited

1) An open discharge system shall not be installed on a property located within a quarter section where more than 4 parcels, excluding the remnant of the parcel, have been subdivided out of the quarter section.1

1 Intent: Sentence (1) — Existing systems may remain in operation but once the number of subdivided parcels exceeds 4, additional open discharge systems are not allowed.

- 2) An open discharge system shall not be used where
 - a) the expected peak volume of wastewater per day, as determined by Section 2.2., exceeds 3 m3 (660 lmp. gal.) per day, except as allowed in Article 8.7.2.3., or
 - b) the strength of the effluent will exceed the quality of primary treated effluent Level 1.

8.7.2.3. Multiple Discharge Systems

1) Where there are multiple open discharge systems located on a property or where there are no property lines in the area being developed, the distance between the outlets of the open discharge systems shall be not less than 180 m (600 ft.), except where the combined expected peak daily flow is less than 4.091 m³ (900 lmp. gal.), in which case the distance between open discharge system outlets shall be at least 30 m (100 ft.).

8.7.2.4. Soil Test Pit Required

1) Notwithstanding the requirements of Sentence 7.1.2.1. (1), a minimum of one soil test pit is adequate for the evaluation of soil suitability for an open discharge system.

8.7.3. Open Discharge Systems -Requirements for Materials

Gravel 8.7.3.1.

1) If gravel is used at the outlet of the open discharge system to protect the soil from erosion, it does not need to meet any of the specifications in this Standard for gravel.

Part 9 Evaporative and Storage Lagoons

9.1.1. Lagoons — Objectives and Design Standards

9.1.1.1. Seepage

- 1) A *lagoon* shall be designed to control seepage
 - a) with a liner, consisting of porous material in which seepage is governed by Darcy's Law, which has a maximum hydraulic conductivity calculated by the following equation:

Maximum
$$K_T = \frac{C \times T}{T + 2}$$

where:

 K_T = maximum hydraulic conductivity of liner in the field, being at least one order of magnitude greater than the laboratory value, metres/second

T = required or proposed thickness of liner, metres

 $C = 5.2 \times 10^{-9}$ metres/second.

- **b)** with a flexible polymeric membrane liner having a minimum thickness of 0.5 mm or 500 µm (20 mils), and
 - i) membranes less than 1.5 mm or 1,500 µm (60 mils) thick are covered with a 300 mm (1 ft.) layer of fine grained soil on the slopes to prevent liner damage, and
 - ii) PVC and other membranes that are susceptible to weathering when exposed shall be covered with *soil* on both the side slopes and bottom.

9.1.1.2. Evaporation

- 1) A lagoon shall be designed to achieve the evaporation of the wastewater or effluent it receives.
- 2) Notwithstanding Sentence (1), when a lagoon is intended to serve only as storage for the winter months or high-flow periods so the accumulated effluent can be applied to a soil-based effluent treatment and dispersal system during warm weather months, the lagoon shall have a storage capacity of not less than one year average wastewater flow.

9.1.1.3. Dimensions

- 1) A *lagoon* shall be designed to provide¹
 - a) a wastewater depth of not greater than 1.5 m (5 ft.),
 - **b)** a 600 mm (2 ft.) freeboard height above the design operating depth,
 - c) a berm slope not steeper than 1 vertical to 3 horizontal,
 - d) sufficient surface area to evaporate 150% of the expected annual volume of wastewater or effluent discharged into it, based on mean flow volumes, and the design surface area of the *lagoon* shall²
 - i) consider the net evaporation at the system location determined by the average annual precipitation and evaporation rates recorded by the Prairie Farm Rehabilitation Administration as reproduced in Appendix A.2.A. and Appendix A.2.B., and
 - ii) provide adequate storage to hold expected volumes of wastewater or effluent during winter or other periods of low net evaporation,

- e) a minimum berm width of 1.8 m (6 ft.), as measured at the top of the berm, and
- f) a finished elevation of the *berm* that will be above the surrounding *grade*, to prevent the entry of surface run-off water into the *lagoon*.
 - ¹ Intent: Sentence (1) Lagoons for private systems built to this Standard are not meant to rely on periodic discharge and must be sized to evaporate all sewage. Annual precipitation and evaporative rates must be considered in the design.

9.1.1.4. Influent Receiving Pit

- 1) The *wastewater* or *effluent* shall enter the *lagoon* into a receiving pit that is accessible for periodic cleaning, and the receiving pit shall have the
 - a) capacity to provide storage of accumulating sludge below the elevation of the wastewater inlet pipe that is at least the volume of 2 times the average daily flow volume, and
 - **b)** inlet pipe entering into it at an elevation that is a minimum of 600 mm (2 ft.) below the bottom of the *lagoon*.¹

9.1.1.5.

Fencing of Lagoons

 A lagoon serving other than a single-family dwelling or duplex or where the design operating depth exceeds 600 mm (2 ft.) shall be fenced.¹

¹ Intent: Sentence (1) — The fence should be designed to preclude the entrance of children and to discourage trespassing. The fence should also serve to preclude the entrance of livestock. Fences should be located away from the outside toe of the berm to facilitate mowing and maintenance operations. Where the lagoon is located near developed areas, a chain link fence may be required to prevent children from gaining entry. In addition, an access gate should be provided to allow the entry of maintenance equipment, and this gate should be equipped with a lock to prevent the entrance of unauthorized personnel. Signs should be posted to identify the lagoon and advise against trespassing.

9.1.2. Lagoons — Prescriptive Requirements and Installation Standards

9.1.2.1. Separation Distances

- 1) A lagoon serving a single-family dwelling or duplex shall not be located within
 - a) 100 m (330 ft.) of a water source or water well,
 - **b)** 100 m (330 ft.) of a municipal licensed water well,
 - c) 90 m (300 ft.) of a water course,
 - d) 30 m (100 ft.) of a property line, and
 - e) 45 m (150 ft.) of a building.
- 2) A *lagoon* serving other than a single-family *dwelling* or duplex shall not be located within
 - a) 100 m (330 ft.) of a water source or water well,
 - **b)** 100 m (330 ft.) of a municipal licensed water well,
 - c) 90 m (300 ft.) of a water course,
 - **d)** 30 m (100 ft.) of a *property* line,
 - e) 90 m (300 ft.) of a building, and
 - f) 90 m (300 ft.) of a numbered primary or secondary road.
- 3) *All* measurements shall be taken from the outside of the *berm*, where the side slope of the *berm* intersects with the natural ground surface.

² Note: Clause (1)(d) — Formulas to calculate the required size of the lagoon are included in Appendix A.2.

¹ Intent: Clause (1)(b) — Entering the pipe in this pit should provide a constant 600-mm (2-ft.) cover of water over the pipe that should provide protection from frost. The pit should be approximately 1.8 m x 1.8 m x 1.8 m (6 ft. X 6 ft. X 6 ft.) deep with the pipe entering 1.2 m (4 ft.) above the bottom of the pit.

Part 10 Privies

10.1.1. Privies — Objectives and Design Standards

10.1.1.1. Containment of Waste

1) A *privy* shall adequately contain the waste to prevent contamination of water sources.

10.1.2. Privies — Prescriptive Requirements and Installation Standards

Location of Privies 10.1.2.1.

- 1) Except as provided in Sentence (2), a privy shall not be located within
 - a) 15 m (50 ft.) of a water source or water well,
 - b) 15 m (50 ft.) of a water course, except as required by Article 2.1.2.4..
 - c) 5 m (17 ft.) of a property line,
 - d) 6 m (20 ft.) of a store, restaurant, or other place where food is stored, prepared, or consumed, and
 - e) 3.5 m (11.5 ft.) of a single-family dwelling.
- 2) Notwithstanding the requirements of Sentence (1), a privy equipped with a water-tight holding tank to contain the wastes shall not be located within
 - a) 10 m (33 ft.) of a water source or water well,
 - **b)** 10 m (33 ft.) of a *water course*,
 - c) 1 m (3 ft.) of a property line as measured from the tank wall, and
 - d) 1.8 m (6 ft.) of a property line as measured from the tank vent termination.
- 3) A privy equipped with a watertight holding tank to contain the wastes shall be located where it is accessible for removal of the waste by a vacuum truck.

10.1.2.2. Restriction on Receiving Water-carried Wastes

- 1) A privy that uses an earthen pit to contain the waste shall not have wastewater directed to the pit.
- 2) A privy equipped with a watertight holding tank to contain wastes may receive greywater from outdoor washstands or from a residence.

10.1.2.3. Accessories Required for Water-tight Holding Tanks

- 1) A watertight *holding tank* used to contain the waste from a *privy* shall
 - a) include an opening to facilitate pump out of the tank, and
 - b) include child protection bars to prevent accidental entry into the tank when used in a location where public access is expected.
- 2) The bars referred to in Clause (1)(b) shall be
 - a) spaced so that a spherical object having a diameter of 100 mm (4 in.) cannot pass through, and
 - **b)** aligned to minimize the accumulation of waste material.

10.1.2.4. Restricted Use of Earthen Pit Privy

1) An earthen pit *privy* may be used only for private use and shall not be used to serve a public or commercial facility.

10.1.2.5. Earthen Privy Soil Conditions

- 1) The soil in which an earthen privy pit is constructed shall
 - a) be fine sandy loam or finer textured,
 - **b)** not include any lenses of *soil* coarser than *fine sandy loam* within the depth of the pit, and
 - c) include *soil* to a depth of at least 600 mm (2 ft.) below the bottom of the pit that is *fine sandy loam* or finer *texture*.
- 2) Below the bottom of the earthen pit there shall be a minimum of 1.2 m (4 ft.) of soil to saturated soil conditions or bedrock.

10.1.2.6. Maximum Depth of Earthen Pit Privy

1) The depth of an earthen pit serving a *privy* shall not exceed 1.2 m (4 ft.) below *grade*.

10.1.2.7. Protection from Surface Water Infiltration

- 1) The privy shall be located where it will not be subject to pooling of surface water runoff.
- 2) An earthen-pit *privy* shall include a *berm* surrounding the pit that is a minimum of 150 mm (6 in.) above the surrounding ground surface to prevent the entry of surface water runoff.
- 3) Openings into a tank used for a *privy* shall be a minimum of 150 mm (6 in.) above the surrounding finished ground surface to prevent surface water runoff from entering the tank.

10.1.2.8. Venting of Storage Tank

 The tank of a privy accessible to the public shall be ventilated with the termination of the vent above the roof of the privy and at least 3.5 m (11.5 ft.) from any adjacent building opening.

10.1.2.9. Privy Structure

- 1) A sanitary *privy* shall be provided with
 - a) a self-closing door,
 - **b)** natural lighting,
 - c) seats and covers of non-absorbent, easily cleanable material,
 - d) ventilation of the privy enclosure to the outside,
 - e) insect-proof screens on ventilation openings, and
 - f) a toilet paper dispenser.

10.1.3. Privies — Requirements for Materials

10.1.3.1. Tanks Used under a Privy

1) A tank used to contain the waste from a *privy* shall meet or exceed the requirements of CAN/CSA-B66, "Design, Material, and Manufacturing Requirements for Prefabricated

- Septic Tanks and Sewage Holding Tanks," and be certified by an accredited testing agency.
- 2) A tank used to contain the waste from a privy shall be structurally capable of carrying the load of the privy structure and person traffic.

Alberta Private Sewage Systems Standard of Practice	

APPENDIX A

A.1. Pressure Distribution Lateral Pipe System Tables

A.1.A. Number of Orifices per *Distribution Lateral Pipe*

A.1.A. Number of Orifices in a <i>Distribution Lateral Pipe</i>												
	Orifice Diameter			(3.2r			•		2" (4r	nm)		
	NPS Pipe Size				<u> </u>							
Squirt	of Distribution											
Height, ft.	Lateral Pipe	3/4" 10mm	1" 25mm	1-¼"	1-½"	2" 51mm	3/4" 10mm	1" 25mm	1-¼" 32mm	1-½"	2" 51mm	
l leight, it.	Distribution Lateral	1311111	•	•	•	31111111	1311111	•	•	•	31111111	
		Ο.	Maximum Orifices Permitted					Maximum				
	Length, ft.	Offices Permitted					0	Orifices Permitted				
2 to 4	10	-	-	-	-	-	-	-	-	-	-	
	15	-	-	-	-	-	-	-	-	-	-	
	20	-	-	-	-	-	-	-	-	-	-	
	25	-	-	-	-	-	-	-	-	-	-	
	30	-	-	-	-	-	-	-	-	-	-	
	35	-	-	-	-	-	-	-	-	-	-	
	40	-	-	-	-	-	-	-	-	-	-	
	45 50	-	-	-	-	-	-	-	-	-	-	
	55	-	_	-	-	-	-		-	_	-	
	60	_	_	_	_	_	_	_	_	_	_	
	65	-	-	-	-	-	-	-	-	-	-	
5 to 9	10	20	20	20	20	20	20	20	20	20	20	
	15	26	30	30	30	30	17	30	30	30	30	
	20	22	40	40	40	40	14	27	40	40	40	
	25	20	37	50	50	50	13	24	48	50	50	
	30	18	33	60	60	60	11	21	44	60	60	
	35	16	31	70	70	70	11	20	40	60	70	
	40	15	29	58	80	80	10	18	37	56	80	
	45	14	27	55	82	90	9	17	35	53	90	
	50	14	25	52	78	100	-	16	33	50	96	
	55	13	24	49	74	110	-	15	32	47	91	
	60	12	23	47	70	120	-	15	30	45	87	
	65	12	22	45	67	130	-	14	29	43	83	
10 to 15	10	20	20	20	20	20	20	20	20	20	20	
	15	26	30	30	30	30	17	30	30	30	30	
	20	23	40	40	40	40	15	27	40	40	40	
	25	20	38	50	50	50	13	24	50	50	50	
	30	18	34	60	60	60	12	22	45	60	60	
	35	17	32	65	70	70	11	20	41	62	70	
	40	16	29	60	80	80	10	19	39	58	80	
	45	15	28	56	85	90	10	18	36	54	90	
	50	14	26	53	80	100	-	17	34	51	99	
	55	13	25	51	76	110	_	16	33	49	94	
	60	13			72			15				
			24	48		120	-		31	46	89	
	65	-	23	46	69	130	-	15	30	44	86	

(continued)

Table A.1A Continued

	Orifice Diameter		3/16	" (4.8	mm)		7/32" (5.6mm)				
	NPS Pipe Size			(
Squirt	of Distribution										
Height,	Lateral Pipe	3/4"	1"	1-1/4"	1-1/2"	2"	3/4"			-1/2"	2"
ft.	Lateral Pipe	19mm	25mm	32mm	38mm	51mm	19mm 2	25mm 32	mm 38	mm	51mm
ıt.	Distribution		Ma	aximu	ım			Max	imun	1	
	Lateral Length, ft.	0	rifice	s Pei	rmitte	ed	Orifices Permitted				
2 to 4										1	
2 10 4	10	-	-	-	-	-	10	19	20	30	20
	15 20	-	-	-	-	-	8 7	15 13	30 27	40	30 40
	25		-	_		-	6	12	24	36	50
	30		_	_	_	_	6	11	22	32	60
	35	_	_	_	_	_	-	10	20	30	57
	40	-	-	-	-	_	-	9	19	28	53
	45	-	-	-	-	-	-	9	17	26	50
	50	-	-	-	-	-	-	-	16	25	47
	55	-	-	-	-	-	-	-	16	23	45
	60	-	-	-	-	-	-	-	15	22	43
	65	-	-	-	-	-	-	-	14	21	41
5 to 9	10	14	20	20	20	20	11	20	20	20	20
	15	12	22	30	30	30	9	16	30	30	30
	20	10	19	38	40	40	7	14	28	40	40
	25	9	16	34	50	50	7	12	25	37	50
	30	8	15	30	46	60	6	11	22	34	60
	35	7	14	28	42	70	-	10	21	31	59
	40	-	13	26	39	75	-	10	19	29	55
	45	-	12	25	37	71	-	9	18	27	52
	50	-	11	23	35	67	-	-	17	26	49
	55	-	11	22	33	63	-	-	16	24	47
	60	-	10	21	31	60	-	-	16	23	44
10 to 15	65	-	10	20	30	58	-	-	15	22	43
10 10 15	10	15	20	20	20	20	11	20	20	20	20
	15	12	22	30	30	30	9	16	30	30	30
	20	10	19	39	40	40	8	14	29	40	40
	25	9	17	35	50	50	7	13	25	38	50
	30	8	15	31	47	60	6	11	23	35	60
	35	8	14	29	43	70	-	10	21	32	61
	40	-	13	27	40	77	-	10	20	30	57
	45	-	12	25	38	73	-	9	19	28	53
	50	-	12	24	36	69	-	9	18	26	50
	55	-	11	23	34	65	_	-	17	25	48
	60	_	-	22	32	62	_	_	16	24	46
	65	-	-	21	31	60	-	-	15	23	44

(continued)

Table A.1.A. Continued

A.1.A. N	lumber of Orifices	in a	Dis	tribut	ion l	Late	al P	ipe				
	Orifice Diameter			' (6.4r				•	" (7.1	mm)		
Squirt Height,	NPS Pipe Size of Distribution Lateral Pipe	³¼" 19mm	1" 25mm	1-1/4"	1-1/2"	2" 51mm	³¼" 19mm	1" 25mm	1-¼" 32mm	1-½" 38mm	2" 51mm	
ft.	Distribution		M	aximu	ım		Maximum					
	Lateral Length, ft.	Orifices Permitted				o	Orifices Permitted					
2 to 4	10	8	15	20	20	20	6	12	20	20	20	
	15	6	12	24	30	30	5	9	19	28	30	
	20	6	10	21	31	40	4	8	16	24	40	
	25	5	9	18	27	50	-	7	15	22	42	
	30	-	8	17	25	48	-	7	13	20	38	
	35	-	8	15	23	44	-	-	12	18	35	
	40	-		14	21	41			11	17	32	
	45	-	-	13	20	38	-	-	11	16	30	
	50	-	-	13	19	36	-	-	10	15	29	
	55	-	-	12	18	34	-	-	-	14	27	
	60	-	-	12	17	33	-	-	-	14	26	
	65	-	-	1	16	31	-	-	-	13	25	
5 to 9	10	8	15	20	20	20	7	12	20	20	20	
	15	7	12	25	30	30	5	10	20	30	30	
	20	6	11	21	32	40	5	8	17	25	40	
	25	5	9	19	28	50	-	7	15	22	43	
	30	-	9	17	26	49	-	7	14	20	39	
	35	-	8	16	24	46	-	-	13	19	36	
	40	-	-	15	22	42	-	-	12	18	34	
	45	-	-	14	21	40	-	-	11	16	32	
	50	-	-	13	20	38	-	-	10	16	30	
	55	-	-	13	19	36	-	-	-	15	28	
	60	-	-	12	18	34	-	-	-	14	27	
40 : 45	65	-	-	-	17	33	-	-	-	14	26	
10 to 15	10	8	16	20	20	20	7	12	20	20	20	
	15	7	13	26	30	30	5	10	20	30	30	
	20	6	11	22	33	40	5	9	17	26	40	
	25	5	10	20	29	50	-	8	16	23	44	
	30	-	9	18	26	51	-	7	14	21	40	
	35	-	8	16	24	47	-	-	13	19	37	
	40	-	8	15	23	44	-	-	12	18	35	
	45	-	-	14	21	41	-	-	11	17	32	
	50	-	-	14	20	39	-	-	11	16	31	
	55	-	-	13	19	37	-	-	-	15	29	
	60	-	-	12	18	35	-	-	-	15	28	
	65	-	-	-	18	34	-	-	-	14	27	

(continued)

Table A.1.A. Continued

A.1.A. Number of Orifices in a <i>Distribution Lateral Pipe</i>											
	Orifice Diameter		mm)								
	NPS Pipe Size			`							
	of Distribution										
Squirt	Lateral Pipe	3/4"	1"	1-1/4"	1-1/2"	2"					
Height, ft.	Laterarripe	19mm	25mm	32mm	38mm	51mm					
	Distribution		M	aximu	ım						
	Lateral Length, ft.	Orifices Permitted									
2 to 4	10	5	9	19	20	20					
	15	4	8	16	23	30					
	20	4	7	13	20	38					
	25	-	6	12	18	34					
	30	-	-	11	16	31					
	35	-	-	10	15	28					
	40	-	-	9	14	26					
	45	-	-	9	13	25					
	50	-	-	-	12	23					
	55	-	-	-	12	22					
	60	-	-	-	-	21					
5 to 9	65	-	-		-	20					
0 10 0	10	5	10	20	20	20					
	15 20	4	8 7	16 14	24 21	30 39					
	25	-	6	12	18	35					
	30		6	11	17	32					
	35			10	15	29					
	40	_	_	10	14	27					
	45	_	_	9	13	26					
	50	_	_	-	13	24					
	55	_	_	_	12	23					
	60	_	_	_	-	22					
	65	-	-	_	-	21					
10 to 15	10	5	10	20	20	20					
	15	4	8	17	25	30					
	20	4	7	14	21	40					
	25	-	6	13	19	36					
	30	-	6	11	17	33					
	35	-	-	11	16	30					
	40	-	-	10	15	28					
	45	-	-	9	14	26					
	50	-	-	-	13	25					
	55	-	-	-	12	24					
	60	-	-	-	12	23					
	65	-	-	-	-	22					

A.1.B. Orifice Discharge Rates

Pressure		Orifice Diameter, Inches											
<i>Head</i> , ft.	1/8	5/32	3/16	7/32	1/4	9/32	5/16	11/32	3/8				
2.0	-	-	-	0.66	0.87	1.10	1.36	1.64	1.95				
2.5	-	-	-	0.74	0.97	1.23	1.52	1.83	2.18				
3.0	-	-	-	0.81	1.06	1.35	1.66	2.01	2.39				
3.5	-	ı	-	0.88	1.15	1.45	1.79	2.17	2.58				
4.0	-	ı	-	0.94	1.23	1.55	1.92	2.32	2.76				
4.5	-	-	-	1.00	1.30	1.65	2.03	2.46	2.93				
5.0	0.34	0.54	0.77	1.05	1.37	1.74	2.14	2.59	3.09				
5.5	0.36	0.56	0.81	1.10	1.44	1.82	2.25	2.72	3.24				
6.0	0.38	0.59	0.85	1.15	1.50	1.90	2.35	2.84	3.38				
6.5	0.39	0.61	0.88	1.20	1.56	1.98	2.45	2.96	3.52				
7.0	0.41	0.63	0.91	1.24	1.62	2.06	2.54	3.07	3.6				
7.5	0.42	0.66	0.95	1.29	1.68	2.13	2.63	3.18	3.78				
8.0	0.43	0.68	0.98	1.33	1.74	2.20	2.71	3.28	3.9				
8.5	0.45	0.70	1.01	1.37	1.79	2.26	2.80	3.38	4.03				
9.0	0.46	0.72	1.04	1.41	1.84	2.33	2.88	3.48	4.14				
9.5	0.47	0.74	1.06	1.45	1.89	2.39	2.96	3.58	4.20				
10.0	0.49	0.76	1.09	1.49	1.94	2.46	3.03	3.67	4.3				
10.5	0.50	0.78	1.12	1.52	1.99	2.52	3.11	3.76	4.48				
11.0	0.51	0.80	1.15	1.56	2.04	2.58	3.18	3.85	4.58				
11.5	0.52	0.81	1.17	1.59	2.08	2.63	3.25	3.94	4.68				
12.0	0.53	0.83	1.20	1.63	2.13	2.69	3.32	4.02	4.78				
12.5	0.54	0.85	1.22	1.66	2.17	2.75	3.39	4.10	4.88				
13.0	0.55	0.86	1.24	1.69	2.21	2.80	3.46	4.18	4.98				
13.5	0.56	0.88	1.27	1.73	2.26	2.85	3.52	4.26	5.07				
14.0	0.57	0.90	1.29	1.76	2.30	2.91	3.59	4.34	5.17				
14.5	0.58	0.91	1.31	1.79	2.34	2.96	3.65	4.42	5.26				
15.0	0.59	0.93	1.34	1.82	2.38	3.01	3.71	4.49	5.35				

based on $q = 16.37Cd^2h^{\frac{1}{2}}$ where q = Imperial gallons per minute flow rate C = coefficient of discharge (0.60)d = diameter in inches h = *pressure head* in feet

Use A Minimum 2.0 ft. (600 mm) Of Pressure Head Note: Some pump manufacturers rate pump capacities in US gallons. Pump ratings in US gallons must be converted to Imperial gallons. US Gallons x = 0.83 = 1 Gallons

This table is used to determine the flow rate of an orifice size at a selected pressure head. To determine the total flow, multiply the flow rate for an orifice by the number of orifices in the distribution lateral pipes.

A.1.B.2. C	A.1.B.2. Orifice Discharge Rate in Litres per Minute											
Pressure			0	rifice D	iameter	, mm (i	n.)					
<i>Head</i> , mm	3.2 mm (1/8")	4.0 mm (5/32")	4.8 mm (3/16")	5.6 mm (7/32")	6.4 mm (¼")	7.1 mm (9/32")	7.9 mm (5/16")	8.7 mm (11/32")	9.5 mm (3/8")			
600	_	-	-	3.02	3.95	4.99	6.17	7.46	8.88			
750	-	-	-	3.38	4.41	5.58	6.89	8.34	9.93			
900	-	-	-	3.70	4.83	6.12	7.55	9.14	10.87			
1050	-	-	-	4.00	5.22	6.61	8.16	9.87	11.75			
1200	-	-	-	4.27	5.58	7.06	8.72	10.55	12.56			
1350	-		-	4.53	5.92	7.49	9.25	11.19	13.32			
1500	1.56	2.44	3.51	4.78	6.24	7.90	9.75	11.80	14.04			
1650	1.64	2.56	3.68	5.01	6.54	8.28	10.23	12.37	14.72			
1800	1.71	2.67	3.84	5.23	6.84	8.65	10.68	12.92	15.38			
1950	1.78	2.78	4.00	5.45	7.11	9.00	11.12	13.45	16.01			
2100	1.85	2.88	4.15	5.65	7.38	9.34	11.54	13.96	16.61			
2250	1.91	2.99	4.30	5.85	7.64	9.67	11.94	14.45	17.19			
2400	1.97	3.08	4.44	6.04	7.89	9.99	12.33	14.92	17.76			
2550	2.03	3.18	4.58	6.23	8.14	10.30	12.71	15.38	18.30			
2700	2.09	3.27	4.71	6.41	8.37	10.60	13.08	15.83	18.84			
2850	2.15	3.36	4.84	6.58	8.60	10.89	13.44	16.26	19.35			
3000	2.21	3.45	4.96	6.76	8.82	11.17	13.79	16.68	19.85			
3150	2.26	3.53	5.09	6.92	9.04	11.44	14.13	17.10	20.34			
3300	2.31	3.62	5.21	7.09	9.25	11.71	14.46	17.50	20.82			
3450	2.37	3.70	5.32	7.25	9.46	11.98	14.79	17.89	21.29			
3600	2.42	3.78	5.44	7.40	9.67	12.23	15.10	18.28	21.75			
3750	2.47	3.85	5.55	7.55	9.87	12.49	15.42	18.65	22.20			
3900	2.52	3.93	5.66	7.70	10.06	12.73	15.72	19.02	22.64			
4050	2.56	4.01	5.77	7.85	10.25	12.98	16.02	19.38	23.07			
4200	2.61	4.08	5.87	7.99	10.44	13.21	16.31	19.74	23.49			
4350	2.66	4.15	5.98	8.14	10.63	13.45	16.60	20.09	23.91			
4500	2.70	4.22	6.08	8.27	10.81	13.68	16.89	20.43	24.32			

Note: This table is used to determine the flow rate of an orifice size at a selected pressure head. To determine the total flow, multiply the flow rate for an orifice by the number of orifices in the distribution lateral pipes.

A.1.C.1. Friction Loss in PVC Schedule 40 Pipe - Imperial & U.S. Gallons

		riction						-	-				50)
Flow Imp		Nom	inal Pipe D	Diameter (i	n.)		Flow US		Nom	inal Pipe [Diameter (in.)	
gpm	3/4	1	1 1/4	1 ½	2	3	gpm	3/4	1	1 1/4	1 ½	2	3
1	0.35	0.11	0.03	0.01	0.00	0.00	1	0.25	0.08	0.02	0.01	0.00	0.00
2	1.27	0.39	0.10	0.05	0.01	0.00	2	0.91	0.28	0.07	0.03	0.01	0.00
3	2.69	0.83	0.22	0.10	0.03	0.00	3	1.92	0.59	0.16	0.07	0.02	0.00
4	4.59	1.42	0.37	0.18	0.05	0.01	4	3.27	1.01	0.27	0.13	0.04	0.01
5	6.93	2.14	0.56	0.27	0.08	0.01	5	4.95	1.53	0.40	0.19	0.06	0.01
6	9.71	3.00	0.79	0.37	0.11	0.02	6	6.93	2.14	0.56	0.27	0.08	0.01
7	12.92	3.99	1.05	0.50	0.15	0.02	7	9.22	2.85	0.75	0.35	0.11	0.02
8	16.54	5.11	1.35	0.64	0.19	0.03	8	11.80	3.65	0.96	0.45	0.13	0.02
9	20.56	6.35	1.67	0.79	0.23	0.03	9	14.67	4.53	1.19	0.56	0.17	0.02
10	24.99	7.72	2.03	0.96	0.28	0.04	10	17.83	5.51	1.45	0.69	0.20	0.03
11	29.80	9.21	2.42	1.15	0.34	0.05	11	21.27	6.57	1.73	0.82	0.24	0.04
12	35.01	10.82	2.85	1.35	0.40	0.06	12	24.99	7.72	2.03	0.96	0.28	0.04
13	40.60	12.54	3.30	1.56	0.46	0.07	13	28.97	8.95	2.36	1.11	0.33	0.05
14		14.38	3.79	1.79	0.53	0.08	14	33.23	10.27	2.70	1.28	0.38	0.06
15		16.34	4.30	2.03	0.60	0.09	15	37.76	11.66	3.07	1.45	0.43	0.06
16		18.42	4.85	2.29	0.68	0.10	16	42.54	13.14	3.46	1.63	0.48	0.07
17		20.60	5.42	2.56	0.76	0.11	17		14.70	3.87	1.83	0.54	0.08
18		22.90	6.03	2.85	0.84	0.12	18		16.34	4.30	2.03	0.60	0.09
19		25.31	6.66	3.15	0.93	0.14	19		18.06	4.76	2.25	0.67	0.10
20		27.83	7.33	3.46	1.03	0.15	20		19.86	5.23	2.47	0.73	0.11
25		42.05	11.07	5.23	1.55	0.23	25		30.01	7.90	3.73	1.11	0.16
30			15.51	7.33	2.17	0.32	30		42.05	11.07	5.23	1.55	0.23
35			20.63	9.75	2.89	0.42	35			14.73	6.96	2.06	0.30
40			26.42	12.48	3.70	0.54	40			18.85	8.91	2.64	0.39
45			32.85	15.52	4.60	0.67	45			23.44	11.07	3.28	0.48
50			39.92	18.85	5.59	0.82	50			28.49	13.46	3.99	0.58
55 60				22.49	6.67	0.98 1.15	55 60			33.98 39.92	16.05	4.76 5.59	0.70 0.82
65				26.42 30.63	7.83 9.08	1.13	65			39.92	18.85 21.86	6.48	0.02
70				35.14	10.42	1.53	70				25.08	7.44	1.09
75				39.92	11.84	1.73	75				28.49	8.45	1.24
80					13.34	1.95	80				32.10	9.52	1.39
85					14.92	2.18	85				35.91	10.65	1.56
90					16.58	2.43	90				39.92	11.84	1.73
95					18.33	2.68	95					13.08	1.91
100					20.15	2.95	100					14.38	2.11
125					30.45	4.46	125					21.73	3.18
150 175					42.67	6.25 8.31	150 175					30.45 40.50	4.46 5.93
200						10.64	200					40.50	7.59
250						16.07	250						11.47
300						22.52	300						16.07
500		<u>I</u>				ZZ.JZ	300		<u> </u>				10.07

Note: The values contained within the bolded lines represent a flow velocity within the desired range of 2 to 5 ft. per second. Flow velocity should exceed 2 ft. per second to achieve required scouring of deposits and growth on pipe walls cause by the effluent. Flow velocity over 5 ft. per second should be used cautiously due to excessive pressure being created from sudden flow stops caused by quick closing valves or shock occurring from trapped air in portions of the effluent lines.

A.1.C.2. Friction Loss in PVC Schedule 40 Pipe - Metric

A.1.C.2. Friction Loss in mm <i>Pressure Head</i> per 30.5 Metres in Schedule 40 PVC Pipe (C=150)											
Flow L/min.		N	lominal Pipe	Diameter (in	.)						
L/IIIII.	3/4	1	1 1/4	1 ½	2	3					
5	128	40	10	5	1	0					
10	462	143	38	18	5	1					
15	979	302	80	38	11	2					
20	1667	515	136	64	19	3					
25	2519	778	205	97	29	4					
30	3530	1090	287	136	40	6					
35	4695	1450	382	180	53	8					
40	6010	1857	489	231	68	10					
45	7473	2309	608	287	85	12					
50	9082	2806	739	349	103	15					
55	10833	3347	881	416	123	18					
60	12725	3931	1035	489	145	21					
65	14756	4559	1200	567	168	25					
70		5228	1377	650	193	28					
75		5940	1564	739	219	32					
80		6694	1763	833	247	36					
85		7488	1972	931	276	40					
90		8323	2192	1035	307	45					
95		9199	2422	1144	339	50					
100		10114	2663	1258	373	55					
120		14172	3732	1763	523	77					
140			4963	2344	695	102					
160			6354	3001	890	130					
180			7901	3732	1107	162					
200			9602	4535	1345	197					
220			11453	5410	1604	235					
240 260				6355 7369	1884 2185	276 320					
280				8452	2506	367					
300				9603	2847	417					
320				10820	3208	470					
340					3589	525					
360					3989	584					
380					4409	645					
400					4848	710					
450					6028	882					
500					7325	1072					
550					8738	1279					
600						1502					
700						1998					
800						2558					
900						3181					

The values contained within the bolded lines represent a flow velocity within the desired range of 2 to 5 ft. per second. Flow velocity should exceed 2 ft. per second to achieve required scouring of deposits on pipe walls. Flow velocity over 5 ft. per second should be used cautiously due to excessive pressure being created from sudden flow stops caused by quick closing valves.

A.1.C.3. Friction Loss in Polyethylene Pipe - Gallons

A.1.	A.1.C.3. Friction Loss in Feet <i>Pressure Head</i> per 100 Feet in Polyethylene Pipe, "Carlon" (C=147)												
Flow Imp		Nomir	nal Pipe	Diamete	er (in.)		Flow US		Nomi	nal Pipe	Diamet	er (in.)	
gpm	3/4	1	1 1/4	1 ½	2	3	gpm	3/4	1	1 1/4	1 ½	2	3
1	0.37	0.11	0.03	0.01	0.00	0.00	1	0.26	0.08	0.02	0.01	0.00	0.00
2	1.32	0.41	0.11	0.05	0.02	0.00	2	0.94	0.29	0.08	0.04	0.01	0.00
3	2.80	0.86	0.23	0.11	0.03	0.00	3	2.00	0.62	0.16	0.08	0.02	0.00
4	4.76	1.47	0.39	0.18	0.05	0.01	4	3.40	1.05	0.28	0.13	0.04	0.01
5	7.19	2.22	0.59	0.28	0.08	0.01	5	5.13	1.59	0.42	0.20	0.06	0.01
6	10.08	3.11	0.82	0.39	0.11	0.02	6	7.19	2.22	0.59	0.28	0.08	0.01
7	13.41	4.14	1.09	0.52	0.15	0.02	7	9.57	2.96	0.78	0.37	0.11	0.02
8	17.16	5.30	1.40	0.66	0.20	0.03	8	12.25	3.78	1.00	0.47	0.14	0.02
9	21.34	6.59	1.74	0.82	0.24	0.04	9	15.23	4.71	1.24	0.59	0.17	0.03
10	25.94	8.01	2.11	1.00	0.30	0.04	10	18.51	5.72	1.51	0.71	0.21	0.03
11	30.94	9.56	2.52	1.19	0.35	0.05	11	22.08	6.82	1.80	0.85	0.25	0.04
12	36.34	11.23	2.96	1.40	0.41	0.06	12	25.94	8.01	2.11	1.00	0.30	0.04
13	42.14	13.02	3.43	1.62	0.48	0.07	13	30.08	9.29	2.45	1.16	0.34	0.05
14		14.93	3.93	1.86	0.55	0.08	14	34.50	10.66	2.81	1.33	0.39	0.06
15		16.97	4.47	2.11	0.63	0.09	15	39.19	12.11	3.19	1.51	0.45	0.07
16 17		19.12	5.03	2.38	0.71	0.10	16 17	44.16	13.64	3.59	1.70	0.50	0.07
18		21.39	5.63 6.26	2.66 2.96	0.79	0.12	18		15.26	4.02 4.47	1.90 2.11	0.56	0.08
19		23.77	6.92	3.27	0.88	0.13 0.14	19		16.97 18.75	4.94	2.33	0.63 0.69	0.09
20		28.89	7.61	3.59	1.07	0.14	20		20.62	5.43	2.56	0.76	0.10
25		43.65	11.49	5.43	1.61	0.10	25		31.15	8.20	3.87	1.15	0.17
30		10.00	16.11	7.61	2.26	0.33	30		43.65	11.49	5.43	1.61	0.24
35			21.42	10.12	3.00	0.44	35		10.00	15.29	7.22	2.14	0.31
40			27.42	12.95	3.84	0.56	40			19.57	9.24	2.74	0.40
45			34.10	16.11	4.78	0.70	45			24.34	11.50	3.41	0.50
50			41.44	19.57	5.80	0.85	50			29.57	13.97	4.14	0.61
55				23.35	6.92	1.01	55			35.28	16.66	4.94	0.72
60				27.42	8.13	1.19	60			41.44	19.57	5.80	0.85
65				31.80	9.43	1.38	65				22.70	6.73	0.99
70				36.47	10.81	1.58	70				26.03	7.72	1.13
75				41.44	12.29	1.80	75				29.58	8.77	1.28
80					13.85	2.03	80				33.33	9.88	1.45
85 90					15.49 17.22	2.27 2.52	85 90				37.28 41.44	11.05 12.29	1.62 1.80
95					19.03	2.79	95				41.44	13.58	1.99
100					20.92	3.06	100					14.93	2.19
125					31.61	4.63	125					22.56	3.30
150					44.29	6.48	150					31.61	4.63
175						8.62	175					42.05	6.15
200						11.04	200						7.88
250						16.68	250						11.91
300						23.37	300						16.68

The values contained within the bolded lines represent a flow velocity within the desired range of 2 to 5 ft. per second. Flow velocity should exceed 2 ft. per second to achieve required scouring of deposits on pipe walls. Flow velocity over 5 ft. per second should be used cautiously due to excessive pressure being created from sudden flow stops caused by quick closing valves.

A.1.C.4. Friction Loss in Polyethylene Pipe - Metric

A.1.C.4. Friction Loss in mm <i>Pressure Head</i> per 30.5 Metres in Polyethylene Pipe, "Carbon" (C=147)											
Flow L/min.		Nomi	nal Pipe D	iameter (ir	n.)						
-	3/4	1	1 1/4	1 ½	2	3					
5	133	41	11	5	2	0					
10	480	148	39	18	5	1					
15	1016	314	83	39	12	2					
20	1731	535	141	67	20	3					
25	2615	808	213	100	30	4					
30	3664	1132	298	141	42	6					
35	4873	1506	396	187	56	8					
40	6239	1927	508	240	71	10					
45	7758	2397	631	298	88	13					
50	9428	2912	767	362	107	16					
55	11246	3474	915	432	128	19					
60	13210	4081	1075	508	151	22					
65	15318	4732	1246	589	175	26					
70		5428	1429	675	200	29					
75		6166	1624	767	227	33					
80		6948	1830	864	256	38					
85		7773	2047	967	287	42					
90		8640	2275	1075	319	47					
95		9549	2515	1188	352	52					
100		10500	2765	1306	387	57					
120		14711	3874	1830	543	79					
140			5152	2434	722	106					
160			6596	3116	924	135					
180			8202	3874	1149	168					
200			9967	4708	1396	204					
220			11889	5616	1665	244					
240				6597	1956	286					
260	-			7650	2268	332					
280 300				8774	2601	381 433					
320				9968 11232	2956 3330	488					
340				11202	3726	545					
360	1				4141	606					
380	1				4577	670					
400	1				5032	737					
450					6258	916					
500	1				7604	1113					
550					9071	1328					
600						1560					
700						2074					
800						2656					
900						3302					

The values contained within the bolded lines represent a flow velocity within the desired range of 2 to 5 ft. per second. Flow velocity should exceed 2 ft. per second to achieve required scouring of deposits on pipe walls. Flow velocity over 5 ft. per second should be used cautiously due to excessive pressure being created from sudden flow stops caused by quick closing valves.

A.1.C.5. Friction Loss Equivalent Lengths for Fittings - Polyethylene Pipe

	A.1.C.5. Friction Loss Equivalent Lengths for Polyethylene Piping Insert Fittings											
Expressed in Approximate Length of Straight Pipe												
Pipe Size (in.)		Male/Female Couplings and Elbows and Fittings Rui Pipe Adapters the Run Branch Foot Motres Foot Motres										
	Feet	Metres	Feet	Metres	Feet	Metres						
1/2	1	0.3	0.5	0.15	3	0.91						
3/4	1.5	0.46	0.75	0.23	4.3	1.31						
1	2	0.61	1	0.3	6	1.83						
1 1/4	2.7	0.82	1.3	0.4	8.6	2.62						
1 ½	3.4	1.04	1.6	0.49	10.5	3.2						
2	4.4	1.34	2 0.61 13.2 4.02									
3	6.2 1.89 2.9 0.88 17 5.18											

A.1.C.6. Friction Loss Equivalent Lengths for Fittings – Schedule 40 PVC Pipe

A.1.C.6. Friction Loss Equivalent Length – Schedule 40 PVC Pipe									
Expressed in Approximate Length of Straight Pipe (feet)									
		Nominal Pipe Size (inches)							
Fitting	1/2	3/4	1	1 1/4	1 ½	2	2 ½	3	
90° Elbow	1.5	2	2.5	3.8	4	5.7	6.9	7.9	
45° Elbow	8.0	1.1	1.4	1.8	2.1	2.6	3.1	4	
Gate valve	0.3	0.4	0.6	0.8	1	1.5	2	3	
Tee Flow on Run	1	1.4	1.7	2.3	2.7	4.3	5.1	6.2	
Tee Flow to Branch	4	5	6	7	8	12	15	16	
Male/Female Threaded Adapter	1	1.5	2	2.8	3.5	4.5	5.5	6.5	

A.1.D.1. Liquid Volume of Pipes

Nominal Pipe Diameter, Inches	Volume (per 100 feet of pipe)				
	Litres Imp Gallons				
3/4	8.7	1.90			
1	17	3.74			
1 ¼	30	6.48			
1 ½	40	8.82			
2	66	14.66			
3	145	30.00			
4	250	55.10			

A.1.E.1. Effluent Soil Loading Rates and Linear Loading Rates (Imp. gal.)

Table A.1.E.1. Effluent Soil Loading Rates and Linear Loading Rates (Imp. Gal.)

(IIIIp. Gai.)					Hydraulic Linear Loading Rate, gal/day/ft.					
							Slope	of land		
Soil charac	Infiltration loading rate: gal/day/ft²		0-4%		>4-9%		>9%			
Texture	Structure		Effluent Quality cBOD ₅		Infiltration distance ¹ , in.		Infiltration distance ¹ , in.		Infiltration distance ¹ , in.	
	Shape	Grade	30-150 mg/L	<30 mg/L	12-<24	24-<48	12-<24	24-<48	12-<24	24-<48
COS ² , MS, LCOS, LMS Requires pressure distribution	I	0SG	0.3	0.3	5.0	6.0	6.0	7.0	7.0	8.0
FS,VFS,LFS,LVFS Requires pressure distribution	1	0SG	0.4	0.5	4.5	5.5	5.0	6.0	6.0	7.0
		OM	0.2	0.6	3.5	4.0	4.1	4.6	6.0	7.0
COSL, MSL	PL	1	0.2	0.5	3.5	4.0	4.1	4.6	5.0	6.0
Requires pressure		2,3	0.0	0.2	2.5	3.0	2.7	3.2	2.9	3.4
distribution	PR ³ /BK	1	0.4	0.6	4.5	5.5	5.0	6.0	6.0	7.0
	/GR	2,3	0.6	0.6	4.5	5.5	5.0	6.0	6.0	7.0
		OM	0.18	0.36	2.3	2.6	2.7	3.0	3.2	3.7
	PL	1	0.18	0.36	2.3	2.6	2.7	3.0	3.2	3.7
FSL,VFSL		2,3	0.0	0.15	2.5	3.0	2.7	3.2	2.9	3.4
	PR ³ /BK	1	0.18	0.45	3.5	4.0	3.8	4.3	4.1	4.6
	/GR	2,3	0.32	0.63	3.8	4.3	4.1	4.6	4.4	4.9
		OM	0.18	0.45	2.3	2.6	2.7	3.0	3.2	3.7
·	PL	1	0.3	0.45	3.5	4.0	3.8	4.3	4.1	4.6
L		2,3	0.0	0.15	2.5	3.0	2.7	3.2	2.9	3.4
	PR ³ /BK	1	0.3	0.45	3.5	4.0	3.8	4.3	4.1	4.6
	/GR	2,3	0.45	0.63	3.8	4.3	4.1	4.6	4.4	4.9
		0M	0.0	0.18	2.5	3.0	2.7	3.2	2.9	3.4
CII	PL	1	0.0	0.15	2.5	3.0	2.7	3.2	2.9	3.4
SIL	PR ³ /BK	2,3	0.0	0.0	2.7	2.0	2.0	2.2	- 2 E	1.0
	/GR	1	0.3	0.45	2.7 3.2	3.0	3.0	3.3	3.5	4.0
	/GR	2,3 0M	0.45 0.0	0.63	3.2		3.5	4.0	3.8	4.3
				0.0	17	- 2.2	1.0			- 2.6
SCL, CL, SICL, SI	PL	2,3	0.0	0.15	1.7	2.2	1.9	2.4	2.1	2.6
	PR ³ /BK	۷,5 1	0.0	0.0	2.5	3.0	2.7	3.2	2.9	3.4
	/GR	2,3	0.18	0.45	2.9	3.4	3.2	3.7	3.5	4.0
SC, C, SIC	/GIX	0M	0.0	0.43						
	PL	1,2,3,	0.0	0.0						
	PR ³ /BK	1,2,3,	0.0	0.0						
	/GR	2,3	0.14	0.0	2.5	3.0	2.7	3.2	2.9	3.4
	/01\	2,3 0M			Z.3 	3.0			2.9	
НС	PL	1,2,3,	0.0	0.0						
ПС	PR ³ /BK	1,2,3,	0.0	0.0						
	/GR				2.1		2.3	2.8	2.5	3.0
	/GR	2,3	0.09	0.16	۷.۱	2.6	۷.۵	۷.0	۵.5	ა.0

Table A.1.E.1. Soil Texture and Structure Abbreviations

COS – Coarse Sai	nd	LVFS – Loamy	Very Fine Sand		SI – Silt		
MS –Medium San	d	COSL – Coarse	Sandy Loam	SCL – Sandy Clay Loam			
LCOS – Loamy Co	oarse Sand	MSL – Medium	Sandy Loam	CL – Clay Loam			
LMS – Loamy Med	dium Sand	FSL – Fine San	dy Loam	SICL – Silty Clay Loam			
FS – Fine Sand		VFSL – Very Fine Sandy Loam			SC – Sandy Clay		
LFS – Loamy Fine Sand		L – Loam			SIC – Silty Clay		
VFS – Very Fine Sand		SIL - Silt Loam			C – Clay	HC – Heavy Clay	
PL – Platy	PR – Prismatic	BK – Blocky	GR – Granular M -		- Massive	SG—Single Grain	
0 – Structureless	1 – Weak	2 – Moderate	3 – Strong				

¹ Note: Infiltration distance is the depth of suitable soil below the in situ soil infiltration surface the effluent is applied to and the restrictive

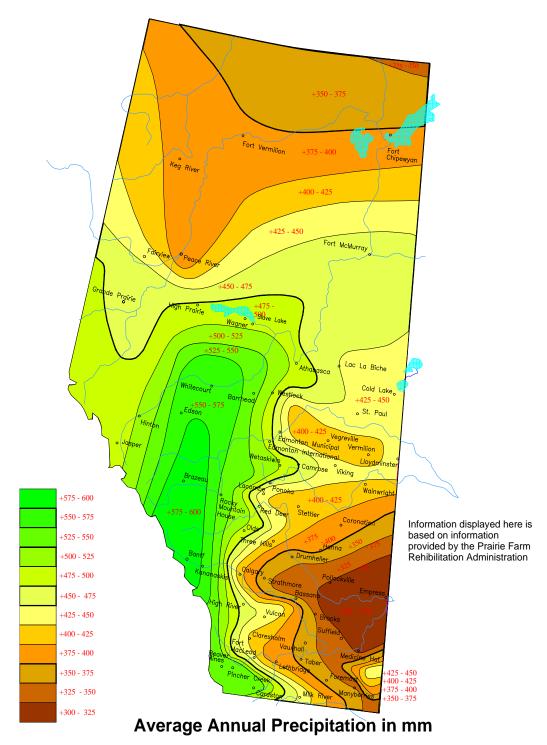
Table 8.1.1.10. Infiltration rates in gal/d/sq. ft. of wastewater effluent strength of >30 mg/L cBOD₅ or wastewater effluent strength of <30 mg/L cBOD5 and hydraulic linear loading rates in gal/d/ft. of system length based on soil characteristics of texture and structure and the site conditions of slope and infiltration depth to restrictive soil layers. Values assume daily wastewater volume estimates used in the design are based on the values set out in Subsection 2.2.2. or include the same safety factor. If horizon consistence is stronger than firm or any cemented class or the clay mineralogy is smectitic, the horizon is restrictive regardless of other soil characteristics (adapted from 2000, E.

² Note: The application of effluent to Coarse Sand textured soil is not allowed except where the requirements of Sentence 8.1.1.3.(2) are

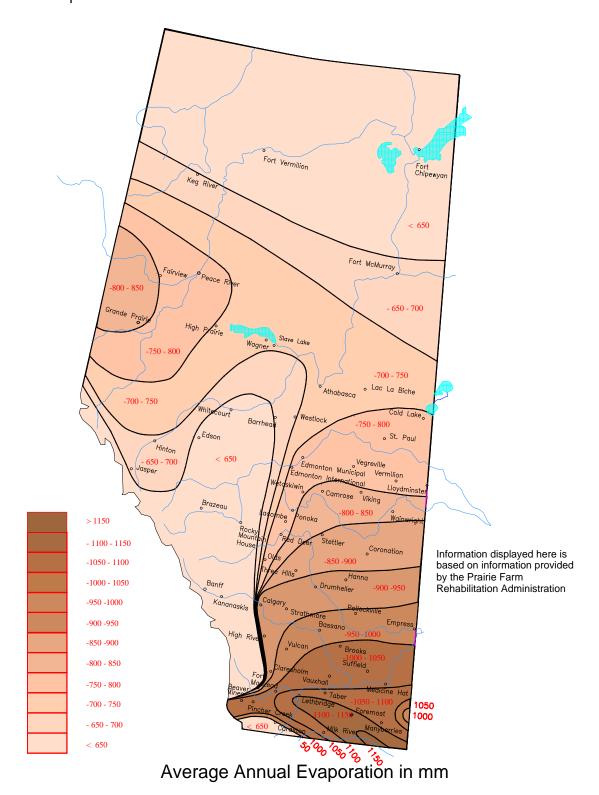
³See restriction on prismatic soils set out in Sentence 8.1.1.10.(4)

A.2. Lagoon System Design Data

A.2.A. Precipitation Rates



A.2.B. Evaporation Rates



A.2.C. Calculation of Lagoon Surface Area Requirements for Evaporation

Note: The following formulas are used to determine the required surface area of a lagoon to accomplish the evaporation of 150% of the expected average sewage volume per year based on average precipitation and evaporation rates (safety factor = 1.25).

Gal of Evap. per Sq. Ft per Year =
$$\frac{(\text{inches of evap. per year - inches of precip. per year)} \times 144}{277 \text{ cubic inches per Imperial gallon}}$$

Litres of Evap. per Sq. M. per Year = $(mm \text{ of Evap. per year - } mm \text{ of Precip. per year}) \times 1$

Square Feet Required =
$$\frac{\text{Average Gallons of Sewage per Year} \times 1.5}{\text{Gallons of Evap. per Square Foot per Year}}$$

Average Litres of Sewage per Year \times 1.5 Square Metres Required = Litres of Evap. per Square Metre per Year

A.2.D. Lagoon Volumes

A.2.D. Calculation of Sewage Lagoon Volume							
Approximate Volume in Litres (gal.)	Size at Base in Metres (ft.)	Size at Mid Depth 750 mm (2.5 ft.)	Size at Full Depth 1500 mm (5 ft.)	Size at Top of <i>Berm</i> 600 mm (2.0 ft.) Freeboard, (2100 mm (7.0 ft.) Above Bottom of <i>Lagoon</i>)			
138,106	4.57 x 4.57	9.14 x 9.14	13.72 x 13.72	17.37 x 17.371			
(30,420)	(15 ft. x 15 ft.)	(30 ft. x 30 ft.)	(45 ft. x 45 ft.)	(57 ft. x 57 ft.)			
184,142	6.10 x 6.10	10.67 x 10.67	15.24 x 15.24	18.90 x 18.90			
(40,560)	(20 ft. x 20 ft.)	(35 ft. x 35 ft.)	(50 ft. x 50 ft.)	(62 ft. x 62 ft.)			
237,260	7.62 x 7.62	12.19 x 12.19	16.76 x 16.76	18.90 x 18.90			
(52,260)	(25 ft. x 25 ft.)	(40 ft. x 40 ft.)	(55 ft. x 55 ft.)	(67 ft. x 67 ft.)			
297,460	9.14 x 9.14	13.72 x 13.72	18.29 x 18.29	21.95 x 21.96			
(62,520)	(30 ft. x 30 ft.)	(45 ft. x 45 ft.)	(60 ft. x 60 ft.)	(72 ft. x 72 ft.)			
364,743	10.67 x 10.67	15.24 x 15.24	19.81 x 19.81	23.47 x 23.47			
(80,340)	(35 ft. x 35 ft.)	(50 ft. x 50 ft.)	(65 ft. x 65 ft.)	(77 ft. x 77 ft.)			
439,109	12.19 x 12.19	16.76 x 16.76	21.34 x 21.34	24.99 x 24.99			
(96,720)	(40 ft. x 40 ft.)	(55 ft. x 55 ft.)	(70 ft. x 70 ft.)	(82 ft. x 82 ft.)			
609,086	15.24 x 15.24	19.21 x 19.11	24.38 x 24.38	28.04 x 28.04			
(134,160)	(50 ft. x 50 ft.)	(65 ft. x 65 ft.)	(80 ft. x 80 ft.)	(92 ft. x 92 ft.)			
807,393	18.29 x 18.29	22.86 x 22.86	27.43 x 27.43	31.09 x 31.09			
(177,840)	(60 ft. x 60 ft.)	(75 ft. x 75 ft.)	(90 ft. x 90 ft.)	(102 ft. x 102 ft.)			
1034,030	21.34 x 21.34	25.91 x 25.91	30.48 x 30.48	34.14 x 34.14			
(227,760)	(70 ft. x 70 ft.)	(85 ft. x 85 ft.)	(100 ft. x 100 ft.)	(112 ft. x 112 ft.)			
1,883,918	30.48 x 30.48	35.05 x 35.05	39.62 x 39.62	43.28 x 43.28			
(414,960)	(100 ft. x 100 ft.)	(115 ft. x 115 ft.)	(130 ft. x 130 ft.)	(142 ft. x 142 ft.)			
2,592,158	36.58 x 36.58	41.15 x 41.15	45.72 x 45.72	49.38 x 49.38			
(570,960)	(120 ft. x 120 ft.)	(135 ft. x 135 ft.)	(150 ft. x 150 ft.)	(162 ft. x 162 ft.)			
3,866,990	45.72 x 45.72	50.29 x 58.21	54.86 x 54.86	58.52 x 58.52			
(851,760)	(150 ft. x 150 ft.)	(165 ft. x 165 ft.)	(180 ft. x 180 ft.)	(192 ft. x 192 ft.)			
4,514,694	53.34 x 53.34	57.91 x 57.91	62.48 x 62.48	66.14 x 66.14			
(1,128,660)	(175 ft. x 175 ft.)	(190 ft. x 190 ft.)	(205 ft. x 205 ft.)	(217 ft. x 217 ft.)			
6,558,302	60.96 x 60.96	65.53 x 65.53	70.10 x 70.10	73.76 x 73.76			
(1,444,560)	(200 ft. x 200 ft.)	(215 ft. x 215 ft.)	(230 ft. x 230 ft.)	(242 ft. x 242 ft.)			
9,957,854	76.20 x 76.20	80.77 x 80.77	85.34 x 85.34	89.0 x 89.0			
(2,193,360)	(250 ft. x 250 ft.)	(265 ft. x 265 ft.)	(280 ft. x 280 ft.)	(292 ft. x 292 ft.)			
14,065,646	91.44 x 91.44	96.01 x 96.01	100.60 x 100.60	104.3 x 104.3			
(3,098,160)	(300 ft. x 300 ft.)	(315 ft. x 315 ft.)	(330 ft. x 330 ft.)	(342 ft. x 342 ft.)			
24,405,905	121.90 x 121.50	126.50 x 126.50	131.1 x 131.1	134.7 x 134.7			
(5,375,760)	(400 ft. x 400 ft.)	(415 ft. x 415 ft.)	(430 ft. x 430 ft.)	(442 ft. x 442 ft.)			

Note: To calculate the volume of a square or rectangular lagoon of a size not listed above, the following formula may be used based on an inside *berm* slope of 3 horizontal to 1 vertical.

Volume={H} over {0.167} times (A+4B+C) times 28.33

V = Volume in litres H = Depth of liquid (maximum of 1.5 metres)

A = Area of bottom of *lagoon* in square metres

B = Area at mid-depth in square metres

C = Area at the high water level in square metres (maximum 1.5 metre depth)

A.3. Alberta Design Data

A.3.A. Alberta C	limate Desig		Town						
		De	sign Tem	nperature	e	Degree	15	One	
	Elevation	Janu	arv	Julv	2.5%	-Days	Min.	Day	Ann. Tot.
Site Name	, m	2.5% °C	1%°C	Dry °C	Wet °C	Below 18°C	Rain, mm	Rain, 1/50, mm	Ppn., mm
Acadia Valley	716	-33	-36	31	20	5500	18	75	310
•	1098	-33 -32	-36 -34	28	18		17	95	440
Airdrie						5200			
Athabasca	515	-35	-38	28	19	6000	18	86	480
Banff	1400	-30	-32	27	17	5500	18	65	500
Barrhead	645	-34	-37	28	19	6000	20	86	475
Bashaw	793	-36	-39	27	19	5600	21	85	460
Bassano	792	-32	-34	28	18	5350	17	85	340
Beaumont	735	-37	-40	27	19	5700	20	90	475
Beaver Lodge	730	-35	-38	28	18	5900	25	92	470
Berwyn	643	-40	-42	27	18	6350	14	80	395
Black Diamond	1159	-32	-34	28	18	5300	16	90	495
Blackfalds	880	-34	-38	28	19	5700	19	95	475
Bon Accord	625	-37	-40	27	19	5750	19	85	485
Bonnyville	564	-36	-39	28	20	6100	21	75	430
Bow Island	799	-32	-36	32	20	4800	17	80	340
Bowden	991	-34	-38	28	19	5700	17	95	480
Brooks	760	-32	-34	32	19	5200	18	86	340
Bruderheim	637	-37	-40	27	19	5800	19	95	480
Calgary	1045	-31	-33	29	17	5200	23	103	425
Calmar	730	-35	-38	27	19	5600	20	95	490
Campsie	660	-34	-37	28	19	6000	20	86	475
Camrose	740	-33	-35	29	19	5700	20	92	470
Canmore	1375	-31	-32	27	17	5500	18	65	500
Cardston	1130	-30	-33	29	18	4750	20	108	550
Carstairs	1060	-33	-36	28	18	5600	17	105	475
Castor	816	-33	-36	29	20	5600	21	85	405
Claresholm	1030	-31	-34	29	18	4800	15	103	440
Coaldale	863	-31	-35	31	19	4700	17	85	390
Cochrane	1159	-32	-34	28	18	5400	17	75	500
Cold Lake	540	-36	-38	28	20	6100	15	81	430
Coleman	1320	-31	-34	28	18	5300	15	76	550
Coronation	790	-31	-33	30	19	5800	20	92	400
Cowiey	1175	-31	-34	29	18	5100	15	81	525
Crossfield	1113	-32	-34	28	18	5500	17	105	485
Daysland	708	-36	-39	28	19	5700	21	85	455
Devon	709	-37	-40	27	19	5600	20	90	490
Didsbury	1037	-37	-40 -36	28	18	5600	17	100	490 480
Drayton Valley	869	-35 -35	-36 -37	26 27	19	5700	20	85	525
Drayton valley Drumheller	685	-35 -31	-37 -33	27 29	18		20	86	375
						5300			
Eckville	930	-34	-37	27	19	5700 5400	17	105	540 460
Edmonton	645	-32	-34	28	19	5400	23	97	460 570
Edson	920	-34	-37	28	18	5900	18	81	570
Elk Point	598	-38	-40	28	20	6200	21	75	440
Embarras Portage	220	-41	-44	27	19	7100	10	86	390
Fairview	670	-38	-40	27	18	6050	15	86	450

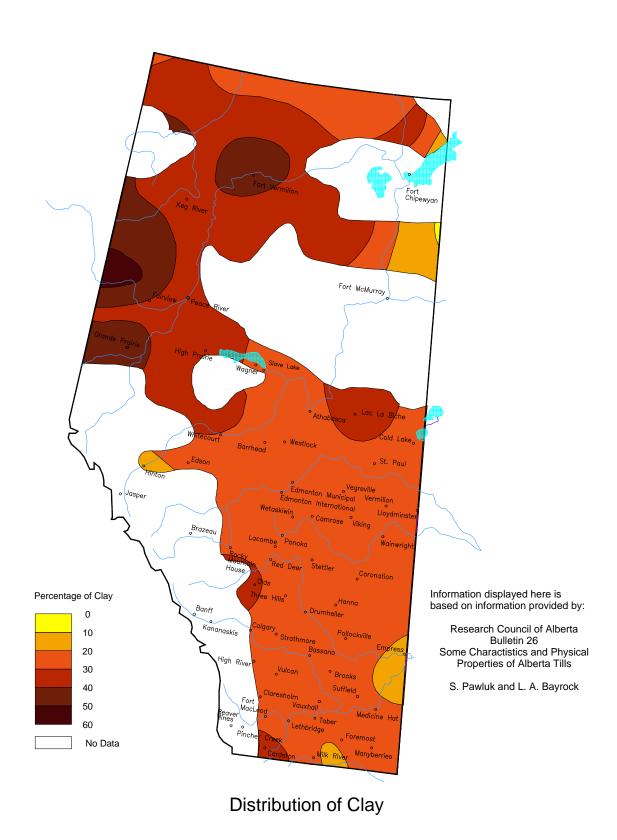
		gn Data by Des	•	perature	•	D	45	One	
	Flanskian			r		Degree	15	Day	A T-4
Site Name	Elevation,	Janua	r		2.5%	-Days	Min.	Rain,	Ann. Tot
	m	2.5% °C	1%° C	Dry °C	Wet °C	Below 18°C	Rain, mm	1/50, mm	Ppn., mm
Falher	587	-40	-42	27	18	5900	15	55	420
Foremost	889	-32	-36	32	20	4800	14	70	360
Fort Chipewayan	221	-43	-46	26	19	7400	12	70	381
Fort MacLeod	945	-31	-33	31	18	4600	16	97	425
Fort McMurray	255	-39	-41	28	19	6550	13	92	460
Fort Saskatchewan	610	-32	-35	28	19	5700	20	86	425
Fort Vermilion	270	-41	-43	28	18	6900	13	65	380
Fox Creek	808	-36	-40	27	19	5900	17	90	550
Gibbons	643	-37	-40	27	19	5800	19	85	485
Gleichen	903	-32	-34	28	18	5300	17	90	360
Grand Centre	541	-36	-39	28	20	6100	21	75	435
Grande Cache	1220	-35	-38	27	15	5700	14	70	605
Grande Prairie	650	-36	-39	27	18	6000	23	86	450
Granum	991	-33	-36	30	18	4800	17	95	440
Grimshaw	603	-40	-42	27	18	6350	14	80	390
Habay	335	-41	-43	28	18	7150	13	70	425
Hanna	785	-33	-36	29	20	5700	19	90	390
Hardisty	615	-33	-35	30	19	5900	20	76	425
High Level	320	-46	-47	26	18	7200	11	75	420
High Prairie	595	-38	-40	25	19	6000	15	75	470
High River	1040	-31	-33	28	17	5300	18	103	425
Hinton	990	-34	-38	27	17	5700	13	81	500
Innisfail	945	-34	-38	28	19	5700	18	95	480
Irvine	763	-32	-36	32	20	4900	17	75	360
Jasper	1060	-32	-35	28	18	5500	10	76	400
Keg River	420	-40	-42	28	18	6800	13	65	450
Killam	680	-35	-38	29	20	5700	21	90	445
Kitscoty	670	-35	-38	29	20	6150	22	80	430
Lac la Biche	560	-35	-38	28	19	6150	15	86	475
Lacombe	855	-33	-35	29	18	5700	23	92	450
Lake Louise	1600	-33	-34	27	14	6700	11	55	580
Lamont	653	-37	-40	27	19	5800	19	90	460
Leduc	730	-35	-38	27	19	5600	20	90	485
Lethbridge	910	-30	-33	31	18	4650	20	97	390
Lloydminster	645	-35	-38	29	20	6100	18	70	430
Magrath	983	-31	-35	31	19	4800	17	80	430
Manning	465	-39	-41	27	18	6700	13	81	390
Mayerthorpe	712	-36	-40	27	19	5950	15	90	555
McLennan	625	-40	-42	27	18	5900	15	65	425
Medicine Hat	705	-31	-34	33	19	4750	23	92	325
Milk River	1059	-31	-35	31	19	4800	16	70	375
Millet	755	-35	-38	27	19	5600	21	95	475
Morinville	700	-37	-40	27	19	5700	19	90	480
Morrin	832	-34	-38	28	19	5500	19	75	390
Mundare	678	-37	-40	27	19	6100	20	90	450
Nanton	1024	-32	-34	28	18	5000	17	95	440

A.3.A. Alberta Cli	imate Desig	n Data by	Town (continue	ed)				
		De	esign Te	mperatui	e	Degree	15	One Day	Ann.
0'' 1	Elevation	Janu	arv	July	2.5%	-Days	Min.	Rain,	Tot.
Site Name	, m	2.5%	l	Dry	Wet	Below	Rain,	1/50,	Ppn.,
		°C	1%°C	°C	°C	18°C	mm	mm	mm
Okotoks	1051	-32	-34	28	18	5300	17	95	470
Olds	1041	-33	-36	28	18	5600	17	95	485
Oyen	770	-33	-36	29	20	5600	19	75	330
Peace River	330	-37	-40	27	18	6350	15	65	390
Penhold	871	-34	-38	28	19	5750	18	95	470
Picture Butte	905	-31	-35	31	19	4700	17	85	400
Pincher Creek	1130	-32	-34	29	18	5000	18	108	575
Ponoka	807	-34	-37	27	19	5600	21	80	480
Provost	668	-33	-36	29	20	5900	21	80	415
Rainbow Lake	534	-46	-47	26	18	7200	16	75	450
Ranfurly	670	-34	-37	29	19	5950	18	92	420
Raymond	960	-31	-35	31	19	4750	17	75	420
Red Deer	855	-32	-35	29	18	5750	23	97	475
Redcliff	745	-32	-36	32	20	4800	17	85	325
Redwater	625	-37	-40	27	19	5900	19	80	470
Rimbey	930	-34	-37	27	19	5700	20	100	505
Rocky	985	-31	22	28	18	5700	20	86	EEO
Mountain House	985	-31	-33	28	18	5700	20	86	550
Ryley	693	-35	-38	27	19	5800	21	90	465
Sangudo	680	-36	-40	27	19	5900	17	95	555
Sedgewick	663	-35	-38	29	20	5700	21	95	440
Sexsmith	724	-38	-41	27	18	6000	18	85	445
Sherwood Park	729	-37	-40	27	19	5500	20	90	480
Slave Lake	590	-36	-39	27	19	6000	15	81	500
Smoky Lake	623	-39	-42	27	20	6000	19	75	480
Spirit River	640	-38	-41	27	18	6200	18	75	440
Spruce Grove	709	-37	-40	27	19	5600	19	90	500
Stavely	1044	-33	-36	30	18	4800	17	95	440
Stettler	820	-32	-34	30	19	5700	20	97	450
Stony Plain	710	-32	-35	28	19	5500	23	97	540
Strathmore	973	-32	-34	28	18	5300	17	80	430
St. Albert	689	-37	-40	27	19	5600	20	95	480
St. Paul	646	-37	-40	28	20	6100	21	75	440
Suffield	755	-32	-34	33	19	4900	20	86	325
Sundre	1093	-34	-37	27	19	5700	15	95	530
Swan Hills	1113	-36	-40	27	19	6100	15	95	500
Sylvan Lake	945	-34	-37	27	19	5700	18	95 03	545
Taber	815	-31	-33	31	19	4800	20	92	370
Thorhild	649	-37	-40	27	19	6000	17	75 80	480
Three Hills	896	-34	-38 40	28	19 10	5450	19	80 05	400 465
Tofield	700	-37	-40	27	19 10	5800 5450	21	95 75	465 405
Trochu	872 1215	-34	-38	28	19	5450	18	75 07	405
Turner Valley	1215	-31	-33	28	17	5600	20	97 90	600 450
Two Hills	603 700	-38 -37	-40 40	28	20	6000	21	80 86	450 490
Valleyview			-40 25	27	18	5900	18	86 95	
Vauxhall Vegreville	779 635	-31 -34	-35 -36	31 29	19 19	4850 6100	17 18	85 86	335 410
Vegreville Vermilion	580	-34 -35	-36 -38	29 29	20	6150	18	86	410
v CITIIIION	560	-33	-30	29	20	0130	10	00	410

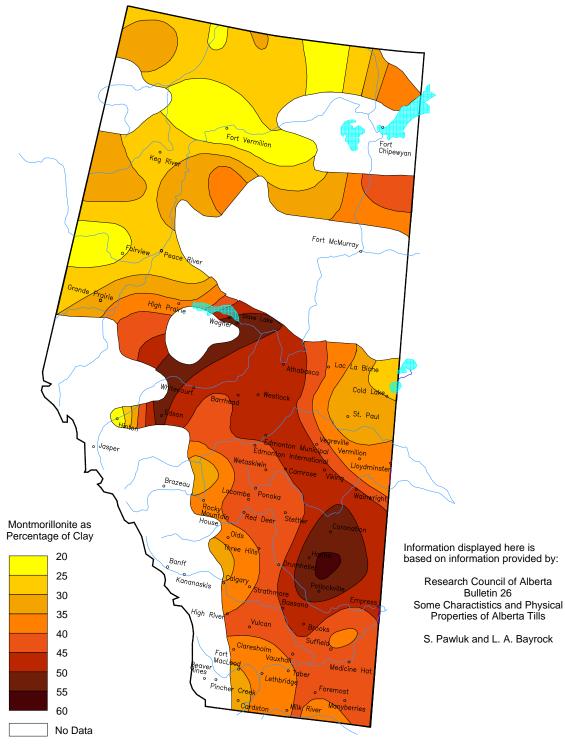
Alberta Private Sewage Systems Standard of Practice

A.3.A. Alberta	A.3.A. Alberta Climate Design Data by Town (continued)									
		Design Temperature				Degree-	15	One		
Site Name	Elevation,	Janu	ary	July 2.5%		Days	Min.	Day	Ann. Tot.	
Site Name	m	2.5% °C	1%°C	Dry °C	Wet °C	Below 18°C	Rain, mm	Rain, 1/50, mm	o, Ppn., mm	
Viking	691	-38	-40	28	20	5750	21	65	445	
Vulcan	1049	-31	-34	30	18	5000	17	90	410	
Wagner	585	-36	-39	27	19	6000	15	76	500	
Wainwright	675	-33	-36	29	19	6000	20	81	425	
Warner	1021	-31	-35	31	19	4750	16	75	375	
Wembley	724	-38	-41	27	18	5900	18	85	470	
Westlock	648	-37	-40	27	19	5900	17	75	490	
Wetaskiwin	760	-33	-35	29	19	5800	23	86	500	
WhiteCourt	690	-35	-38	27	18	6000	20	97	550	
Wimborne	975	-31	-34	29	18	5650	23	92	450	

A.3.B. Soil Clay Content Map



A.3.C. Soil Montmorillonite Content Map



Distribution of Montmorillonite

A.4. Treatment Field Design Data

A.4.A. Disposal Field Loading Rates per Day and Sizes

Table	A.4.A.	2 Bed	rooms	3 Bed	Irooms	4 Bed	rooms	5 Bec	Irooms	6 Bedi	rooms
		Square Metres	Sq. ft.	Square Metres	Sq. ft.	Square Metres	Square ft.	Square Metres	Sq. ft.	Square Metres	Sq. ft.
Loading rate, L/m2	Loading rate, Imp. gal./sq.ft.	2 BR = 340x2x2	2 bedrooms= 75x2x2	3 BR = 340x1.5x3	3 bedrooms= 75x1.5x3	4 BR = 340x1.5x4	4 bedrooms= 75x1.5x4	5 BR = 340x1.5 x5	5 bedrooms= 75x1.5x5	6 BR = 340x1.5 x6	6 bedrooms= 75x1.5x6
per	day	1360 L	300 gal	1530 L	337.5 gal	2040 L	450 gal	2550 L	562.5 gal	3060 L	675 gal
4.89	0.10	277.93	3000.00	312.67	3375.00	416.90	4500.00	521.12	5625.00	625.34	6750.00
5.38	0.11	252.66	2727.27	284.25	3068.18	379.00	4090.91	473.74	5113.64	568.49	6136.36
5.87	0.12	231.61	2500.00	260.56	2812.50	347.41	3750.00	434.27	4687.50	521.12	5625.00
6.36	0.13	213.79	2307.69	240.52	2596.15	320.69	3461.54	400.86	4326.92	481.03	5192.31
6.85	0.14	198.52	2142.86	223.34	2410.71	297.78	3214.29	372.23	4017.86	446.67	4821.43
7.34	0.15	185.29	2000.00	208.45	2250.00	277.93	3000.00	347.41	3750.00	416.90	4500.00
7.83	0.16	173.71	1875.00	195.42	2109.38	260.56	2812.50	325.70	3515.63	390.84	4218.75
8.32	0.17	163.49	1764.71	183.92	1985.29	245.23	2647.06	306.54	3308.82	367.85	3970.59
8.81	0.18	154.41	1666.67	173.71	1875.00	231.61	2500.00	289.51	3125.00	347.41	3750.00
9.30	0.19	146.28	1578.95	164.56	1776.32	219.42	2368.42	274.27	2960.53	329.13	3552.63
9.79	0.20	138.97	1500.00	156.34	1687.50	208.45	2250.00	260.56	2812.50	312.67	3375.00
10.28	0.21	132.35	1428.57	148.89	1607.14	198.52	2142.86	248.15	2678.57	297.78	3214.29
10.77	0.22	126.33	1363.64	142.12	1534.09	189.50	2045.45	236.87	2556.82	284.25	3068.18
11.25	0.23	120.84	1304.35	135.94	1467.39	181.26	1956.52	226.57	2445.65	271.89	2934.78
11.74	0.24	115.80	1250.00	130.28	1406.25	173.71	1875.00	217.13	2343.75	260.56	2812.50
12.23	0.25	111.17	1200.00	125.07	1350.00	166.76	1800.00	208.45	2250.00	250.14	2700.00
12.72	0.26	106.90	1153.85	120.26	1298.08	160.34	1730.77	200.43	2163.46	240.52	2596.15
13.21	0.27	102.94	1111.11	115.80	1250.00	154.41	1666.67	193.01	2083.33	231.61	2500.00
13.70	0.28	99.26	1071.43	111.67	1205.36	148.89	1607.14	186.11	2008.93	223.34	2410.71
14.19	0.29	95.84	1034.48	107.82	1163.79	143.76	1551.72	179.70	1939.66	215.64	2327.59
14.68	0.3	92.64	1000.00	104.22	1125.00	138.97	1500.00	173.71	1875.00	208.45	2250.00
15.17	0.31	89.65	967.74	100.86	1088.71	134.48	1451.61	168.10	1814.52	201.72	2177.42
15.66	0.32	86.85	937.50	97.71	1054.69	130.28	1406.25	162.85	1757.81	195.42	2109.38
16.15	0.33	84.22	909.09	94.75	1022.73	126.33	1363.64	157.91	1704.55	189.50	2045.45
16.64	0.34	81.74	882.35	91.96	992.65	122.62	1323.53	153.27	1654.41	183.92	1985.29
17.13	0.35	79.41	857.14	89.33	964.29	119.11	1285.71	148.89	1607.14	178.67	1928.57
17.62	0.36	77.20	833.33	86.85	937.50	115.80	1250.00	144.76	1562.50	173.71	1875.00
18.11	0.37	75.12	810.81	84.51	912.16	112.67	1216.22	140.84	1520.27	169.01	1824.32
18.59	0.38	73.14	789.47	82.28	888.16	109.71	1184.21	137.14	1480.26	164.56	1776.32
19.08	0.39	71.26	769.23	80.17	865.38	106.90	1153.85	133.62	1442.31	160.34	1730.77
19.57	0.40	69.48	750.00	78.17	843.75	104.22	1125.00	130.28	1406.25	156.34	1687.50
20.06	0.41	67.79	731.71	76.26	823.17	101.68	1097.56	127.10	1371.95	152.52	1646.34
20.55	0.42	66.17	714.29	74.45	803.57	99.26	1071.43	124.08	1339.29	148.89	1607.14
21.04	0.43	64.63	697.67	72.71	784.88	96.95	1046.51	121.19	1308.14	145.43	1569.77
21.53	0.44	63.17	681.82	71.06	767.05	94.75	1022.73	118.44	1278.41	142.12	1534.09
22.02	0.45	61.76	666.67	69.48	750.00	92.64	1000.00	115.80	1250.00	138.97	1500.00

	A.4.A.										
Со	nt'd	2 Bed	rooms	3 Bec	Irooms	4 Bed	rooms	5 Bed	rooms	6 Bed	rooms
		Square Metres	Sq. ft.	Square Metres	Sq. ft.	Square Metres	Square ft.	Square Metres	Sq. ft.	Square Metres	Sq. ft.
Loading rate L/m2	Loading rate, Imp. gal./sq.ft.	2 BR = 340x2x2	2 bedrooms= 75x2x2	3 BR = 340x1.5x3	3 Bedrooms = 75x1.5x3	4 BR = 340x1.5x4	4 bedrooms= 75x1.5x4	5 BR = 340x1.5 x5	5 bedrooms= 75x1.5x5	6 BR = 340x1.5 x6	6 bedrooms= 75x1.5x6
per	day	1360 L	300 gal	1530 L	337.5 gal	2040 L	450 gal	2550 L	562.5 gal	3060 L	675 gal
22.51	0.46	60.42	652.17	67.97	733.70	90.63	978.26	113.29	1222.83	135.94	1467.39
23.00	0.47	59.13	638.30	66.53	718.09	88.70	957.45	110.88	1196.81	133.05	1436.17
23.49	0.48	57.90	625.00	65.14	703.13	86.85	937.50	108.57	1171.88	130.28	1406.25
23.98	0.49	56.72	612.24	63.81	688.78	85.08	918.37	106.35	1147.96	127.62	1377.55
24.47	0.50	55.59	600.00	62.53	675.00	83.38	900.00	104.22	1125.00	125.07	1350.00
24.96	0.51	54.50	588.24	61.31	661.76	81.74	882.35	102.18	1102.94	122.62	1323.53
25.45	0.52	53.45	576.92	60.13	649.04	80.17	865.38	100.22	1081.73	120.26	1298.08
25.93	0.53	52.44	566.04	58.99	636.79	78.66	849.06	98.32	1061.32	117.99	1273.58
26.42	0.54	51.47	555.56	57.90	625.00	77.20	833.33	96.50	1041.67	115.80	1250.00
26.91	0.55	50.53	545.45	56.85	613.64	75.80	818.18	94.75	1022.73	113.70	1227.27
27.40	0.56	49.63	535.71	55.83	602.68	74.45	803.57	93.06	1004.46	111.67	1205.36
27.89	0.57	48.76	526.32	54.85	592.11	73.14	789.47	91.42	986.84	109.71	1184.21
28.38	0.58	47.92	517.24	53.91	581.90	71.88	775.86	89.85	969.83	107.82	1163.79
28.87	0.59	47.11	508.47	53.00	572.03	70.66	762.71	88.33	953.39	105.99	1144.07
29.36	0.60	46.32	500.00	52.11	562.50	69.48	750.00	86.85	937.50	104.22	1125.00
29.85	0.61	45.56	491.80	51.26	553.28	68.34	737.70	85.43	922.13	102.52	1106.56
30.34	0.62	44.83	483.87	50.43	544.35	67.24	725.81	84.05	907.26	100.86	1088.71
30.83	0.63	44.12	476.19	49.63	535.71	66.17	714.29	82.72	892.86	99.26	1071.43
31.32	0.64	43.43	468.75	48.85	527.34	65.14	703.13	81.42	878.91	97.71	1054.69
31.81	0.65	42.76	461.54	48.10	519.23	64.14	692.31	80.17	865.38	96.21	1038.46
32.30	0.66	42.11	454.55	47.37	511.36	63.17	681.82	78.96	852.27	94.75	1022.73

A.5. Acceptable Piping Materials Table

A.5.A. Piping Materials

Type of Piping	Standard Reference	Gravity Sewage or Effluent Piping	Pressure Effluent Line	Weeping Lateral Piping	Pressure Effluent Distribution Lateral Pipe
Polyethylene water pipe and tubing	CAN3-B137.1	N	Р	N	N
Series 160 sizes with compression fittings					
Series 75, 100 and 125					
Poly vinyl chloride (PVC) water pipe	CAN3-B137.3	Р	Р	Р	Р
Schedule 40, Schedule 80					
Chlorinated poly vinyl chloride (CPVC) water pipe	CAN3-B137.6	N	N	N	Р
Plastic Sewer Pipe perforated Plastic Sewer Pipe non perforated	CAN/CSA-B182.1	N P	N N	P N	N N
Corrugated Polyethylene perforated non-perforated	CGSB 41-GP-31	N P	N N	P N	N N
Acrylonitnle- butadiene-styrene (ABS) <i>DWV pipe</i>	CAN/CSA-B181.1	Р	N	N	N
Poly (vinyl chloride) (PVC) <i>DWV pipe</i>	CAN/CSA-B181.2	Р	N	N	N
Type PSM PVC sewer pipe > 35 SDR	CAN/CSA-B182.2	P	N	N	N
Profile poly (vinyl chloride) (PVC) sewer pipe PS 320 kPa	CAN/CSA-B182.6	Р	N	N	N
Profile polyethylene sewer pipe PS 320 kPa	CAN/CSA-182.6	Р	N	N	N
Cast iron soil pipe	CAN3-B70	Р	N	N	N

P = Permitted

N = Not Permitted

A.6. Septic Tank Sludge and Scum Accumulation Rates for Other Than Residential

A.6.A. Septic Tank Sludge and Scum Accumulation Rates

A.6.A. Septic Ta	nk Sludge and Scun	n Accumulation Rates	6
Premises	Fixtures	Sludge/scu	um rate
		Number of Persons	Rate: litres/person/year
Note: Calculate each use a	and add to obtain total capacity		
Note: The term average or highest number in any 12-r	highest daily number over an month period	"x" day period means the	
RECREATIONAL VEHICL Permanent Occupation	E PARKS wc/urinal basin bath/shower laundry kitchen sink	Total number of sites x 3.5	80
Casual Occupation	wc/urinal basin bath/shower laundry kitchen sink	Average number of sites occupied per year x 3.5	48
CHILD DAY CARE CENTI	wc/urinal basin bath/shower laundry kitchen sink	Total number of children and staff	48
CHURCHES, PUBLIC HA	LLS etc. wc/urinal basin kitchen sink (coffee service area only)	12 month highest daily average number over 7- day period	25 for up to 4 days use/ week 40 when over 4 days use/week
Addition:	where kitchen area provided for catering		Add 10 to either of above

Premises	Fixtures	Sludge/s	cum rate
		Number of Persons	Rate: litres/person/year
CLUBS			
Membership entry only. Members/guests & staff using facilities	wc/urinal basin bath/shower kitchen sink (coffee service area only)	Average daily number over 7-day period	35
Licensed area Bar trade only	wc/urinal basin bar sink glass washer	Average daily number over 7-day period	5
Licensed bar & restaurant/meals area	wc/urinal basin kitchen sink dishwasher	Average daily number over 7-day period	10
COFFEE / TEA SHOPS / KIOS	KS		
e.g. light refreshments and prepared food, cakes etc.	wc/urinal basin kitchen sink	Average daily number over 7-day period	30
CONSTRUCTION CAMPS - TE	MPORARY		
	wc/urinal basin shower laundry kitchen sink dishwasher	Total number of persons using facilities	80
HOLIDAY CAMPS			
e.g. scout, youth and church centres with casual occupation	wc/urinal hand basin shower kitchen sink	Total number of beds (single equivalent)	48

Premises	Fixtures	Sludge/scum rate				
		Number of Persons	Rate: litres/person/year			
HOSPITALS AND NURSING	HOMES					
HUSPITALS AND NURSING	HOMES					
Accommodation and resident staff	wc/urinal basin bath/shower laundry kitchen sink dishwasher	Total number of beds plus resident staff	80			
Non-resident staff	wc/urinal basin kitchen sink (coffee service area only)	Number of employees per shift x number of shifts	25			
HOTELS / MOTELS / LIVE IN	CONFERENCE CENTRES					
Accommodation	wc/urinal basin bath/shower kitchen sink laundry	Total number of beds (single equivalents)	48			
Permanent residents, staff etc.	wc/urinal basin bath/shower kitchen sink laundry	Total number of live in staff	80			
Bar trade	wc/urinal basin bar sink glass washer	Average daily number attending in 7-day period	5			
Dining room lounge area non-resident use	wc/urinal basin kitchen sink dishwasher	Average daily number of diners per 7-day period	10			
Non-resident staff	wc/urinal basin kitchen sink (tea service area only)	Number of employees per shift x number of shifts	25			

Premises	Fixtures	Sludge/scu	um rate
		Number of Persons	Rate: litres/person/yea
MEDICAL CONSULTING RO	OMS		
e.g. doctors, dentists, etc. Staff	wc/urinal basin kitchen sink (coffee service area only)	Number of persons using system per shift x number of shifts	40
Consulting rooms		Per consulting room	80
PUBLIC SWIMMING POOLS			
include kiosk e.g. take away food	wc/urinal basin shower kitchen sink (coffee service area only)	Average daily number over 7-day period	20
PUBLIC TOILETS			
	wc/urinal basin	Average daily number over 7-day period	20
Addition:	where shower provided	as above	5
RESTAURANTS			
No liquor license	wc/urinal basin kitchen sink dishwasher	Average daily number over 7-day period plus staff	35
With liquor license	wc/urinal basin kitchen sink dishwasher glass washer	Average daily number over 7-day period plus staff	35

Premises	Fixtures	Sludge/scum rate				
		Number of Persons	Rate: litres/person/year			
REST HOMES, BOARDING						
Accommodation and resident staff	wc/urinal basin bath/shower laundry kitchen sink	Total number of beds plus resident staff (single equivalents)	80			
Non-resident staff	wc/urinal basin kitchen sink (coffee service area only)	Number of employees per shift x number of shifts	25			
ROAD-HOUSES / SERVICE Staff	STATIONS wc/urinal basin kitchen sink (coffee service area only)	Number of employees per shift x number of shifts	25			
Public toilets	wc/urinal basin	Average daily number over 7-day period	20			
	with shower	as above	5			
Restaurant take away and sit down meals	wc/urinal basin kitchen sink dishwasher	Average daily number over 7-day period	10			

Premises	Fixtures	Sludge/scum rate		
		Number of Persons	Rate: litres/person/yea	
SCHOOLS				
Including kiosk facilities e.g. take away food	wc/urinal basin kitchen sink	Total number of students plus staff	25	
Where canteen facilities provided e.g. plated hot and cold meals	kitchen sink dishwasher	as above	10	
SEMINAR/CONFERENCE RO	OMS			
No meals	wc/urinal basin kitchen sink (coffee service area only)	Total seating capacity plus staff	25	
Meals No liquor license	wc/urinal basin kitchen sink dishwasher glass washer	Total seating capacity plus staff	35	
Meals with liquor license	wc/urinal basin kitchen sink dishwasher glass washer	Total seating capacity plus staff	35	
	with shower	as above	5	
Restaurant take away and sit down meals	wc/urinal basin kitchen sink dishwasher	Average daily number over 7-day period	10	

Premises	Fixtures	Sludge/scum rate		
		Number of Persons	Rate: litres/person/year	
SHOPPING CENTRES				
Staff	wc/urinal basin kitchen sink (coffee service area only)	Number of employees per shift x number of shifts	25	
Public	wc/urinal basin	average daily number over 7-day period	20	
Shop Facilities	double bowl sink basin	per shop	20	
Supermarket	double bowl sink basin cleaners sink	per supermarket	40	
SPORTS CENTRES				
e.g. health and fitness clubs, squash courts indoor hockey, basketball	wc/urinal basin shower kitchen sink (coffee service area only)	average daily number over 7-day period plus staff	25	
STAFF ABLUTIONS, WORK	(PLACE INSTALLATIONS			
e.g. factories commercial office	wc/urinal basin kitchen sink (coffee service area only)	number of employees per shift x number of shifts	25	
Where canteen facilities provided for kiosk meals, e.g. pies, pastries, sandwiches	kitchen sink			
Where plated meals provided e.g. hot/cold meals prepared on site	kitchen sink dishwasher	as above	10	
WINE TASTING				
	wc/urinal basin kitchen sink glass washer	average daily number over 7-day period	5	

A.7. Conversion Factors

- 1 pound = 0.45359 kilograms
- 1 inch = 2.540 centimetres
- 1 foot = 0.3048 metres
- 1 yard = 0.9144 metres
- 1 yard = 36.00 inches
- 1 mile = 1.609 kilometres
- 1 square inch = 6.452 square centimetres
- 1 square foot = 0.093 square metres
- 1 square yard = 0.836 square metres
- 1 acre = 0.405 hectares
- 1 acre = 43560 sq. ft. or 208.7x 208.7 ft.
- 1 square mile = 259 hectares
- 1 square mile = 2.59 square kilometres
- 1 cubic inch = 16.387 cubic centimetres
- 1 cubic foot = 28.317 cubic centimetres
- 1 cubic foot = 6.23 Imperial gal.
- 1 cubic foot = 28.3 litres
- 1 cubic yard = 0.765 cubic metres
- 1 cubic yard = 168 lmp gal.
- 1 cubic yard = 765 litres
- 1 Imperial gal. = 4.546 litres
- 1 Imperial gal. = 277.42 cubic inches
- 1 Imperial gal. of water = 10 lbs.
- 1 U.S. gal. = 3.785 litres
- 1 U.S. gal. = 231 cubic inches
- 1 Imperial gal. per sq. ft. = 49 litres per sq. metre
- 1 Imperial gal. = 1.20 U.S. gal.
- 1 U.S. gal. = 0.83 Imperial gal.
- 1 foot pressure head = 304.8 mm pressure head
- 1 foot pressure head = 0.434 psi
- 1 psi = 2.301 ft. pressure head
- 1 psi = 6.894757 kPa

- 1 kilogram = 2.2046 pounds
- 1 centimetre = 0.3937 inches
- 1 metre = 3.281 ft.
- 1 metre = 1.094 yards
- 1 metre = 39.37 inches
- 1 kilometre = 0.6214 miles
- 1 square centimetre = 0.155 sq. inches
- 1 square metre = 10.765 square ft.
- 1 square metre = 1.196 square yards
- 1 hectare = 2.471 acres
- 1 hectare = 10,000 square metres
- 1 square kilometre = 0.386 square miles
- 1 cubic centimetre = 0.06102 cubic inches
- 1 cubic decimeter = 0.0353 cubic ft.
- 1 litre = 0.0353 cubic ft.
- 1 cubic metre = 1.308 cubic yards
- 1 cubic metre = 35.3 cubic ft.
- 1 cubic metre = 220 Imperial gal.
- 1 cubic metre = 1000 litres
- 1 litre = 0.220 Imperial gal.
- 1 litre = 0.264 U.S. gal.
- 1 kPa = 0.145037 psi
- 1,000 mm pressure head = 9.807 kPa
- 1 kPa = 102 mm pressure head
- 1 kPa = 0.335 ft. pressure head
- 1 litre per sq. metre = 0.020 Imperial gal. per sq. ft.
- 1 Litre per sq. metre = 1 mm depth of effluent applied
- 1 Imperial gal. per sq. foot = 1.92 inches depth of effluent applied



